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TEST OF A SUPERSONIC AXIAL COMPRESSOR STAGE INCORPORATING SPLITTER VANES IN THE ROTOR

A. J. Wennerstrom, et al

Aerospace Research Laboratories Wright-Patterson Air Force Base, Ohio

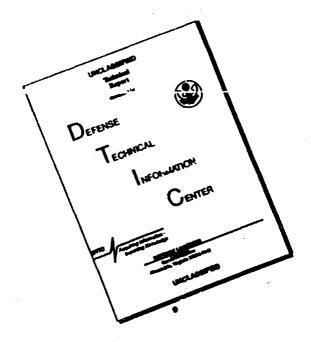
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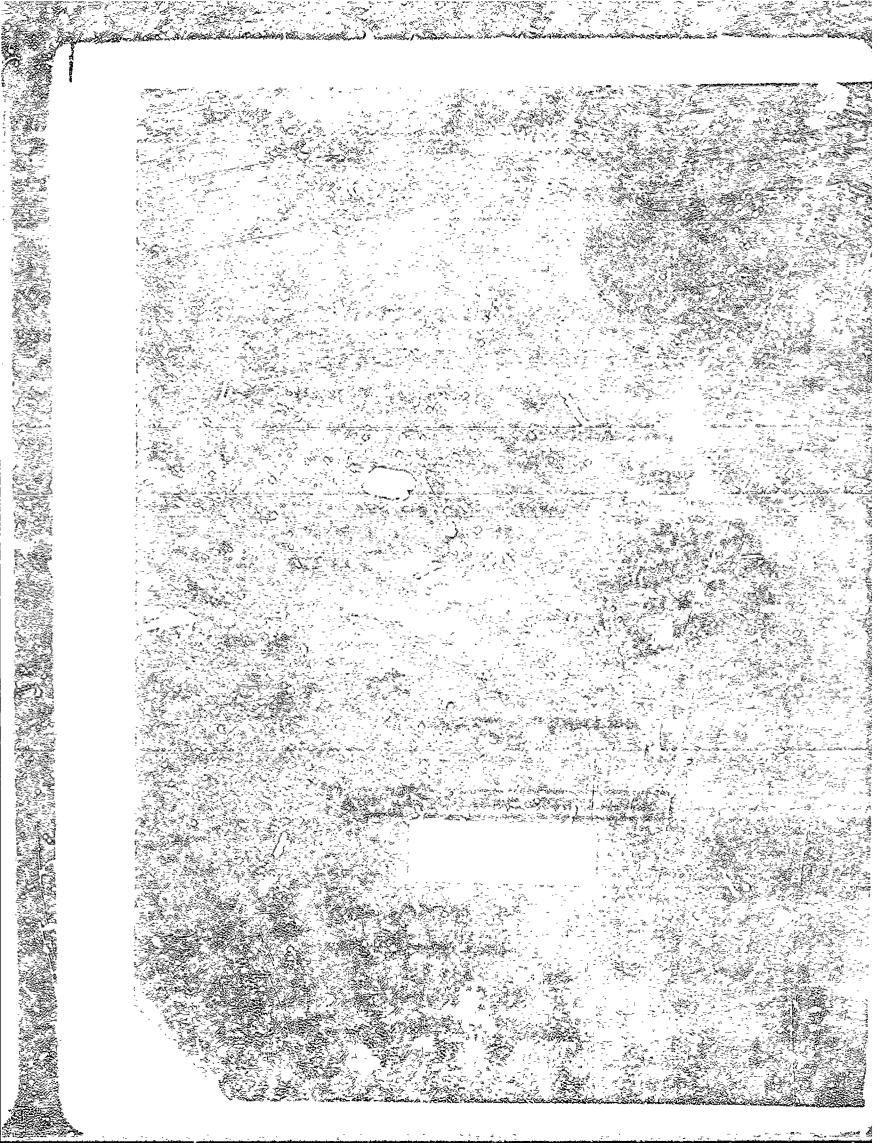


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Complete experimental results are presented from tests of an axialcompressor stage designed for a tip speed of 1600 ft/sec, a stage total pressure ratio of 3.06, and an inlet hub/tip radius ratio of 0.75. The rotor had been redesigned to incorporate a splitter vane between each pair of principal airfoils. At design speed, the compressor passed 88 percent of design flow, achieved a stage total pressure ratio of 2.77, and achieved isentropic efficiencies of 0.846 for the rotor and 0.674 for the stage. This represented a major improvement over the Dreceding configuration tested without roton solitter

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PREFACE

William A. Buzzell of the Fluid Mechanics Research Laboratory, Aerospace Research Laboratories (AFSC), Writht-Patternon Air Rorce Base, Onio and Mr. Robert D. DeRose of Systems Research Laboratories, Inc., Dayton, Ohio. The work herin reported was accomplished between December 1972 and December 1974.

The report presents results from a portion of the effort of the Flids Machinery Research Group supervised by Dr. Arthur J. Wennerstrom and conducted under Work Unit 09 of Project 7065, "Aerospace Simulation Techniques Research," under the over-all direction of Mr. Elmer G. Johnson, Director.

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SECTION I

INTRODUCTION

This report presents the results of an experimental evaluation of the single stage, supersonic axial compressor described in Reference 1 and modified according to Reference 2. This compressor was designed for an over-all stage total pressure ratio of 3.06 to 1 at an isentropic efficiency of 81.5 percent. Design tip speed was 1600 ft/sec at standard conditions, and the inlet hub/tip radius ratio was 0.75. There were no inlet guide vanes. The modification described in Reference 2 consisted of redesign of the rotor to incorporate a "splitter vane" between each of the principal rotor airfoils. The splitter vane consisted of an airfoil located circumferentially mid-way in the downstream half of each rotor blade passage and extending full span.

The compressor tested was designed for diffusion levels beyond the range of past experience in both rotor and stator. This choice was deliberate in order to provide a suitable test bed for the evaluation of boundary layer control devices applicable to a compressor and to obtain data at values of Diffusion Factor above 0.5. The performance of the original design, reported in Reference 3, was extenely poor. The results reported herein, obtained after the addition of splitter vanes, represent a major improvement in both rotor and stage performance. The rotor performed relatively close to, although somewhat below, design goals. Stage performance was still significantly short of design objectives. No boundary layer control devices were installed for this test.

The second section of this report describes the test facility flow path, the compressor test vehicle, and the complete instrumentation system. Section III describes the procedures used in taking data and subsequently in reducing the data. The results of the test are presented in Section IV. Section V, the last section, summarizes the conclusions drawn from the data. Appendix A presents detailed aerodynamic results, including computing stations within blade rows, for the data point on each speed line corresponding to peak stage efficiency. The rest of the Appendices provide sufficient data such that any reader wishing to process any data point not fully presented here, or wishing to process any data point differently, can, with the aid of References 6 and 1, completely reprocess the data or adapt the raw data to his own data reduction scheme.

SECTION II

APPARATUS

FACILITY FLOW PATH

The test facility used is of the open-loop variety. It is schematically shown in Pigure 1. Air enters the facility through a filter designed to remove five micron particles with a 99.5 percent efficiency. The air then passes through a 30-inch duct to a Dall Flow Tube located about six pipe diameters downstream. About two pipe diameters further domstream, the air is turned 90 degrees with the aid of turning vanes and then passes through a perforated plate designed to reduce inlet pressure approximately three psi at 24-lb/sec flow at standard atmospheric conditions. Following this, the air passes through a tube bundle and subsequently enters a 48-inch diameter settling chamber. The settling chamber contains a perforated conical flow spreader and two screens patterned after the model investigation reported in Reference 4. From the settling chamber, air enters the compressor through a direct-coupled believeth. Air leaving the compressor is deflected radially outsignd to a peripheral thristtle. The throttle consists of one stationary and one rotating cylindrical ring, each with 16 circumferentially distributed matching holes. Throttling takes place at a diameter of approximately 47 inches. Downstream of the throttle. the flow enters a collector, from which it is passed through a 24-inch duct to a silencer, and back to the atmosphere. A fast-acting paper type valve, bypassing the throttle valve, is also available to relieve surge conditions. A cutaway drawing of the complete test facility is shown in Pigure 2.

2. COMPRESSOR TEST VEHICLE

A cross section of the research compressor is shown in Figure 3. The design employs a contilevered rotor supported by four 0.5-inch thick bearing support struts with leading edges located about two stator chord lengths downstreem of the stator trailing edge plane. The rotor tip diameter at the leading edge is nominally 18 inches. Oil seals are controlled gap carbon seals with an air burrier. Ho oil leakage into the flow path has ever been experienced. Cold rotor radial tip clearance with the rotor at rest is 0.037 to 0.039 inch. Hot clearence at design speed is predicted to be approximately 0.020 inch or about 0.6 percent of the mean rotor chord. The rotor shaft is mounted on ball bearings. Radial runout does not exceed 0.0005 inch. The bulletnose and inlet hit flow path are supported by six bi-convex struts in the inlet. The flow area contraction ratio between the trailing edge plane of the struts and the leading edge plane of the rotor is 2.72 to 1. Surface finish on all surfaces adjacent to the flow upstream of the bearing support struts is 32 microinches or better. An abradable costing has been employed in the casing adjacent to the roter tip. However, no rubs have been experienced, even in stall. The rotor is of integral construction, the blades and disc being mechined from a single forging

of 6Al-4V titanium. The stator blades are individually inserted but are muchined integrally with platforms at hub and tip. The gap between adjacent platforms lies in the range of 0 to 0.002 inch. A photograph of the rotor is shown in Figure 4.

3. COMPRESSOR INSTRUMENTATION

Aerodynamic instrumentation in the compressor consists of measuring points in stator leading edges for total pressure and temperature, rakes downstream of the stators for total pressure and temperature, a large number of static pressure taps distributed on the inner and outer flow path and on the surface of one pair of stator blades, and dynamic wall pressure measurements made over the rotor tip. Measurements of inlet total pressure and temperature, mass flow, relative humidity, and rotor speed are accomplished outside of the compressor and are discussed in paragraph 4 of Section II. The Supersonic Compressor research vehicle has a total of 133 sensors measuring aerodynamic parameters at various points throughout the stage. Refer to Figure 3 and Table 1 for specific locations. Some of the static pressures are sensed at more than one point and are manifolded to become, in each case, a single measurement. Figure 5 shows the vehicle instrumentation bulkhead.

a. Temperature Measurements

(1) Location

A total of thirty-nine Chromel-Alumel thermocouples are used to sense temperature. Four are mounted in the planum, ten are mounted in the vane leading edges, and twenty-five are located in the five discharge plane rakes. The vane leading edge and the rake mounted thermocouples are of the slot vented probe type (Figures 6, 9a., and 10). A detailed analysis of the features of the slot vented design, along with recovery factor characteristics, may be found in Reference 5. The rakes were designed with the sensors dividing the discharge annulus into equal radial increments while circumferential spacing is on divisions equal to 2.2 times the distance between vane trailing edges. In Figure 3, the discharge plane drawing is in error. The temperature rake shown at 200° 31' chould be located at 211° 33'.

The ten stator leading edge thermoccuple probes are mounted on four varies with two varies having two thermoccuples and two varies having three thermoccuples. As with the discharge rakes, these probes are also spaced to divide radially the stator annulus into five equal increments; however, in this case with two sensors per radius.

(2) Calibration

All thermocouples were fabricated from individually insulated, single rolls of Chromel and Alumel wire. Samples were taken periodically along the rolls as the thermocouples were made for vehicle installation. These sample thermocouples were calibrated against a model 162 platinum resistance bulb primary standard manufactured by

Rosemount Engineering Company. A constant temperature oil bath, made by Lauda Division of Brinkman Instruments, are was used as the heat medium. The bath was set at four different temperatures within the range of interest. The results, indicated in Table 2, show a worst case error of plus or minus 0.5°P at the highest temperature.

With thermocouple calibrated as indicated, the entire electronic system employed to record temperature data was examined. The results are shown in Table 3. Taking the worst case error, at the highest temperature, for both the thermocouples and readout system yields a maximum error of plus or minus 0.9°F. The more realistic RSS error goes from 0.23°F at 150 degrees to 0.65°F at 350 degrees. Finally, when recovery factor variation is added, the RSS error at 350°F becomes plus or minus 1.0°F. Figure 7 depicts the equipment used in the calibrations.

h. Pressure Measurements

(1) Location

Thirty-five static (PS) and thirty-five total (PT) pressures are measured in the vehicle flowpath. Twenty-five of the static taps are distributed at various points on the compressor flowpath liners. In particular, ten of these are located over the rotor blade tip, starting at 0.25 inch axially forward of the leading edge and following at 0.25 inch axial intervals extending downstream. A further ten statics are located approximately mid-chord radially on two vanes with seven suction side taps on one vane and three pressure side taps on the other.

The ten vane mounted total pressure probes are of the Kiel stagnation tube design (Figure 8) and are mounted with two sensors on each of two vanes and three on each of two other vanes. All are radially located to divide the annulus into five equal parts, with two measurements per radius. The other twenty-five are impact tubes mounted as five radial rakes of five sensors each, dividing the discharge annulus into equal increments which are circumferentially spaced in a menner similar to that of the temperatue rakes. An impact pressure rake is shown in Figure 9.b.

Located for use in conjunction with the static taps placed over the rotor blade tips are eight Kistler Model Number 603A pressure transducers and a Bentley Model 316 proximity detector. Because of problems observed at high speed with the Kistler dynamic pressure data, no further mention will be made of this sytem.

(2) Calibration

Four Statham strain gage type transducers are used to convert the various pressures into electrical signals for processing through readout and recording. One transducer is located in each of four, forty-eight port Scanivalve sequential pressure switching devices. The

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pressures to be campled are connected to oid numbered ports while moderate vacuum is applied to all even (Roughir,) ports to minimize hysteresis effects.

Three calibration pressures are sensed by all four Scanivalves on every scan. These are barometric, 15 PSIG and 30 PSIG. The 15 and 30 PSIG standards are supplied by Ametek Model PK-30 self-regulating, primary deadweight type, pressure standards referred to atmosphere. The computer software used for data reduction corrects these two gauge values against variation in local barometric pressure and creates a new transducer calibration curve for every scan. Two absolute calibration pressures have been added to this system for use in future tests, and the barometric calibration pressure has been eliminated.

c. Readout Electronics

Data are collected and recorded through use of a Hewlett Packard 2012B Data Acquisition System (DAS). This system is comprised of a 2011 guarded prossbar scanner, 2547A coupler, 2402A integrating digital voltmeter, 5050B digital recorder, and a Kennedy 1506 incremental tape recorder.

As previously stated, pressure measurements are routed through four Scanivalve units using Stathan transducers for conversion into electronic signals. A "Scanivalve" offers the advantage of using the same transducer to measure many pressures and lends itself to on-line calibration as described above. An interface unit was built to program the Scanivalves, along with other parameters, into the HP DAS in a manner which minimizes scanning time without compromising transducer settling time. Instead of sampling the same port on all valves sequentially before stepping to the next port, the digital interface causes each valve to move through its next roughing port to its next data point immediately after being interrogated. Each transducer then has an opportunity to settle out at its next test pressure while two others are sequentially interrogated. This sequence is repeated until all ports are sampled. Approximately six seconds lapse for the entire procedure.

Thermocouple outputs are routed through a Kaye Instruments' Model K170 electronic ice point reference into the interface unit and then to the HP DAS.

4. TEST FACILITY INSTRUMENTATION

a. Rotor Speed

A Pentley Model 306 transducer senses six prooves machined into the gearbox/rotor driveshaft coupling. The output is fed into a Model 3115 proximitor for signal conditioning. The proximitor signal is a train of pulses having a repetition rate corresponding to rotor RPM/10. This

repetition rate is directly recorded by the HP DAS. A Bently Model 5030 digital tachometer provides a visual indication of rotor speed accurate to ten RPM. The Tachometer also includes an adjustable speed limiting switch as a safety feature.

t. Mass Flow

Inlet pressure is metered through a product series 122 Dall tube venturi manufactured by B.I.F. Industries with a 12.687-inch throat. Metering accuracy has been calibrated to plus or minus one-half percent by the manufacturer. Static pressure taps are located both in the throat and in the inlet cavity.

c. Inlet (Plenum) Total Pressure and Temperature

Compressor inlet total pressure is assumed equal to plenum static pressure just downstream of the last screen. Four static taps are manifolded into one pressure and recorded on two separate Scanivalves. The Maximum error associated with this assumption is 0.06 percent. Temperature is sensed by four bare junction thermocouples located in the same axial plane as the pressure taps, and supported on two crossed cables.

d. Analog Compressor Mapping

An on-line plot of stage pressure ratio vs pseudo mass flow was effected through use of a Mosely Model 2FRA X-Y plotter. Teledyne pressure transducers were used to sense stage inlet PO1, stage exit PO3 from a mid-radius stagnation tube and hub P1 (measured 0.25 inch upstream of the rotor). Operational amplifiers were used to ratio exit PO3 to inlet PO1 and also to ratio hub P1 to inlet PO1. Stage pressure ratio was used to excite the Y-axis while 1 - (P1/PO1) was sent to the X-axis. The approximate compressor map so obtained was used to select a reasonable distribution of throttle settings at which to record detailed data.

e. Relative Humidity

A Foxboro Dewcel Model 2711TG-K222 was mounted in the inlet stack to monitor humidity. This device continuously measures the moisture content of the air by sensing the temperature at which the partial pressure of its water vapor is equal to the water vapor pressure of a saturated salt solution. The humidity information is acquired by the DAS as a thermocouple reading on every test run and subsequently treated in the Phase I data reduction program.

SECTION III

TEST PROCEDURE AND DATA REDUCTION

1. TEST PROCEDURE

Test data were taken in order of increasing speed, with each speed-line being entirely probed before any data at higher speed were acquired. The on-line analog x-y plot capability discussed in paragraph 4.d. of Section II was used to select the test points, since on-line data reduction was not available.

For each speedline, test data were first acquired at a partially-closed exhaust throttle settling, after which the compressor was gradually throttled to include stall. After recovery, data were taken at several points as the throttle was opened from near-stall to wide-open. Stall was indicated by two sources: the dynamic pressurers across the rotor tip, which were displayed on oscilloscopes on the test operator's console, and a microphone in the plenum. Sudden oscillations of the above-mentioned x-y plotter were further indicators that stall had occurred.

Data were acquired at the rate of about one speedline per hour. On dates when elevated speed lines were investigated, a single test point at each of several lower speeds was taken to assure data integrity by comparison to previously acquired data at these lower speeds.

Prior to each test, an atmospheric pressure reading was obtained from a mercury barometer at the test site. The rig was initially brought up to speed and then monitored for about ten minutes, when it was assumed equilibrium had been reached. A five-minute dwell at each throttle setting was observed prior to data acquisition. Two data scans were acquired per test point on each speedline.

A 12-character test identification number was manually assigned to each test point and acquired by the DAS as the first item of information during data acquisition at that point character 1: last digit of year; characters 2-3: numerical month; characters 4-5: numerical day of month; characters 6-7: test point number on that particular date; characters 8-10: numerical throttle setting; characters 11-12: last two digits of the nominal percent-speed (e.g., 85% = 85; 100% = 00)). Where two scans were taken at a particular test point automaticall each scan bears the same test identification number.

Finally, a listing of all raw experimental data which were acquired during testing of this stage is provided in Appendix D, and all computer input data used for Phases I and II of the data reduction are provided in Appendix B.

2. DATA REDUCTION - PHASE I

Phase I reduction of the test data was accomplished by using a slightly modified version of the computer program described in Reference 6. The modifications are subsequently described in Reference 3.

In Reference 6, Equation (11) is in error and should be expressed as follows:

$$W = C1 \cdot \frac{CQ \cdot Y \cdot d^2 \cdot F}{\sqrt{1 - \beta^4}} \int_{h(\gamma_a + \gamma_v)}$$

No change, however, is required to the actual computer coding of the original program.

3. DATA REDUCTION - PHASE II

Phase II reduction of the test data was accomplished by using the computer program described in Reference 7.

To aid in the calculation procedure of the within blade analysis, a CALCOMP plotting routine labeled DEVPLOT was developed to allow better visualization of the deviation angles at each rotor computing station and hub, mid, and tip streamlines. The DEVPLOT input values used are the final deviation angles determined during a within blade calculation. The values are given as a function of normalized axial distance. A complete listing of this program is given in Appendix C1.

In addition to the DEVPLOT routine, a second CALCOMP plotting routine was utilized to plot the stator mid-span surface static pressure distribution for each within blade analysis. This program is labeled STAPLOT and uses the experimental readings of the seven suction surface static taps and the three pressure surface static taps (located on the mid-span of the instrumented stator blades) as input values. Extrapolated static pressure values for the stator leading and trailing edges are also input to the plotting routine. These values are based on the radial location of the first and last suction surface static taps and the leading and trailing edge calculated values of static pressure determined by the within blade analysis. A complete listing of this program is given in Appendix C2.

SECTION IV

RESULTS

1. OVER-ALL PERFORMANCE

The mass-averaged performance of the rotor and of the complete compressor stage is tabulated in Table 4 and plotted in Figure 12. The performance shown is a major improvement over the original configuration tested (without rotor splitter vanes) and reported in Reference 3. At 100 percent design corrected speed, corrected flow was approximately 12 percent low, rotor efficiency was 5 points low, stage efficiency was 14 points low, rotor total pressure ratio peaked at 3.47 versus a design value of 3.35, and stage total pressure ratio peaked at 2.77 versus 3.06, respectively. The compressor was throttled to stall at each corrected speed shown on the map. The data point nearest stall was taken at a throttle opening approximately 0.5 percent further open than the setting which precipitated stall. This change in throttle area is equivalent to about 0.9 percent of the annulus area at the rotor inlet.

2. BLADE-ELEMENT PERFORMANCE (ACROSS BLADE)

The radial distributions of relative inlet Mach number, incidence angle, loss coefficient, deviation angle, and diffusion factor for both rotor and stator are presented in Figures 13 through 82, using Tables 5-11, for each data point shown on the compressor map. One set of these five radial distributions is presented for each blade row at each corrected speed. In each of these sets, the distributions for all throttle settings are superimposed on each respective plot. As described earlier in Section III, this data was reduced using the full radial equilibrium equation with the equations of momentum, continuity, etc. satisfied at each computing station for each streamline. This data, also used for the compressor map, was reduced with computing stations only at blade-row edges and in free spaces; there were no computing stations internal to blade rows.

3. BLADE-ELEMENT PERFORMANCE (WITHIN BLADE)

The data point nearest maximum stage efficiency for each operating speed was selected for more detailed analysis. The more detailed analysis involved the introduction of four additional computing stations within the rotor. The data reduction was then accomplished in the same manner as before, with blockages and deviation angles internal to the rotor adjusted so that the calculated and measured static pressures along the casing adjacent to the rotor tip were as nearly coincident as possible. The results of these analyses include plots of the radial

distribution of the same five parameters for rotor and stator described in the preceding paragraph (Figures 102 through 191), plots of the experimental (rotor only) and calculated axial distribution of static pressure at hub, mean, and case (Figures 192 through 201), corresponding plots of the distribution of deviation angle within the rotor blade row (Figures 202 through 211), plots of the surface distributions of static pressure for a mid-span section of the stator (Figures 212 through 221), and a complete herodynamic description at each computing station - streamline intersection (Appendix A).

ROTOR TIP DYNAMIC PRESSUE'S MEASUREMENTS

The dynamic distribution of static pressure over the rotor tips was observed during operation to assess qualitatively flow stability during the test. In general, the flow appeared much more stable at the higher speeds than was the case with the previous compressor configuration reported in Reference 3. Also, as design speed was approached, the dynamic pressure signal measured 0.25 inch upstream of the rotor because very weak, indicating that the passage shock had probably been swallowed. A few bursts of these data were recorded on wide-band FM magnetic tape. However, no further processing of these data was attempted since at no time during the course of these tests were all elements of the dynamic pressure recording system working sat's factorily simultaneously.

SECTION V

CONCLUSIONS

The major conclusion drawn from the reported tests was that splitter vanes added to the axial compressor rotor accomplished their intended purpose of controlling rotor deviation angles at off-design, high incidence operating conditions with a satisfactory level of total pressure losses. Furthermore, operation of the compressor was now close enough to its design point that it appeared feasible to embark upon the series of boundary-layer-control modifications originally envisioned to assess their potential usefulness in this type of environment.

The dramatic decrease achieved in deviation angle is best seen by referring to Figures 222 and 223. The first of these figures presents deviation angle at the rotor trailing edge mid-radius location versus rotor incidence at mid-radius on the leading edge for the original rotor as presented in Reference 3 and also for the new rotor. Whereas a definite trend was apparent for the original rotor, all data points for the new rotor fall in a cluster, exhibiting no apparent sensitivity to incidence angle. The single data point shown for each corrected speed corresponds to operation at peak stage efficiency for each respective speed. The second of these figures compares the design radial distribution of deviation angle with distributions measured at design speed for the first and second rotor configur-Whereas deviation angles measured with the first rotor remained well above design values all along the span, deviation angles recorded for the second rotor remained substantially lower than design values over most of the span. Only locally near the tip was deviation observed to rise rapidly above the design level. This might be due to boundary layer separation on the outer casing. It might also be due to rotor boundary layer and wake fluid, rotating at near blade speed, being centrifuged outward and collecting at the outer casing.

In order to assess the loss characteristics of the rotor, it was necessary to divide the measured total losses into diffusion losses and shock losses. Reference 8 presents the results of a cascade test of a blade section corresponding to streamsurface No. 10 in the design calculations of Reference 1, with splitter vanes added. At design-point operating conditions, static pressure along the suction surface of the principal airfoils was seen to be nearly constant at the undisturbed freestream value up to the shock impingement point indicating that neither precompression nor expansion has occurred upstream of the passage shock wave. Consequently, since the compressor stage passed only about 88 percent of design flow, the suction surface Mach number just upstream of the shock wave was assumed

to be increased above the free stream relative value by an amount equal to a Prandtl-Meyer expansion from the relative free stream Mach number through an angle equal to the difference betweem actual operating incidence and design incidence. was then presumed equal to the total pressure loss through a normal shock having an upstream Mach number equal to the average of the relative free stream and section surface Mach numbers on any streamsurface. Interpolating between streamsurfaces, these computations were performed for blade sections at 10, 50 and 90 percent span. Shock loss was subtracted from the total loss measured at the same location, and the result was plotted in the form of Total Pressure Loss Parameter versus Diffusion Factor in Figure 224. Blade solidity was presumed equal to the sum of principal blade chord plus splitter vane chord divided by the mean circumferential spacing between principal blade sections. Shown in this same figure are curves derived from Reference 9 and the extrapolation made for design purposes and presented in Reference 1. The interesting conclusion drawn from this figure is that at Diffusion Factors below 0.6, where there is extensive data, the blade section including splitter vanes performs exactly as would be expected, upon taking the increaed solidity into account. However, at Diffusion Factors substantially above 0.6, the blade section with splitter vanes continues to perform satisfactorily and with losses lower than expected.

Consequently, the application of splitter vanes to axial compressor blade rows has potential for configurations combining relatively low aspect ratio with high aerodynamic loading. should be suitable for stationary as well as rotating blade They may also be suitable for fully subsonic blade sections as well as supersonic sections for which the concept was demonstrated. Although the rotor performance reported herein was good, the data of Reference 8 indicate that the splitter vane design was not optimum. The simple approach used for this splitter vane design, which consisted of duplicating the camber line of the principal airfoils and locating the splitter vane in mid-channel, resulted in very poor pressure distributions around the splitter vane, including re-expansion to supersonic Mach numbers according to Reference 8. It appears that a splitter vane carefully designed in the cascade plane might produce much lower losses than reported herein.

TABLE I
INSTRUMENTATION LIST

SENSOR T/C T/C T/C	AXTAL 6.181	7.800	CIRCINGERENTIAL	REMARKS
T/C T/C	6.181			~ · · · · · · · · · · · · · · · · · · ·
T/C			36*48	Disch Rake Element
				Hamidity
TIC				(Not In Use)
			45°	Plenum
T/C			135°	Plenum
T/C			225*	Planus
				Pleran
				Leeding Edge
			يساخل النادات وبرجوي والمنبال والمناجع بمانات المناجع والمناجع والمناجع والمناجع والمناجع والمناجع والمناجع والمناجع	Landina: Páge
				Leading Idae
				Leeding Rine
				Lending Base
				Leading Rine
				Leading Rice
				Leading Rine
				Leading Rice
				Disch. Rake Rieses Disch. Rake Rieses
				Dische Rake Riesen
				Mach. Pake Rieser
				Disch, Bake Riesen
			والمراب والمستون الأكارات والكالية المراجع والمراجع والمراجع والمراجع والمراجع والمراجع والمراجع والمراجع	Disch. Pake Bless
				Mach. Rake Rieser
				Mach. Rake Ricon
T/C				Dische Rake Blessen
T/C	6.181		243°581	Disch, Bake Blance
T/C	6.181	8.120	4°281	Disch. Pake History
T/C	6.181	8.120	36*48*	Disch. Bake Rlange
T/C	6.181	8.120	69* 7*	Disch, Pake Blance
1/C	6.181	8.120	211 33'	Mach, Pake Blance
T/C	6.181	8.120		Disch. Rake Blance
	6.181	7.960		Disch. Rake . 'small
		7.960	36°43'	Disch. Rake Rieses
				Disch. Rake Elemen
			211 33'	Disch. Rake Blanes
			243*58*	Disch. Pake Blesser
T/C	6.181	7.800	4'28'	Disch. Rake Elemen
				Disch. Rake Elemen
				Disch. Rake Kleng
T/C	6.181	7.800	243'58'	Misch. Rake Blance
				1
				<u> </u>
	1/C 1/C 1/C 1/C	T/C LE T/C G.181 T/C 6.181	T/C LE 8.371 T/C LE 8.371 T/C LE 8.251 T/C LE 8.251 T/C LE 8.121 T/C LE 8.121 T/C LE 8.121 T/C LE 8.001 T/C LE 8.001 T/C LE 7.871 T/C LE 7.871 T/C LE 7.871 T/C 6.181 8.440 T/C 6.181 8.440 T/C 6.181 8.440 T/C 6.181 8.440 T/C 6.181 8.280 T/C 6.181 8.20 T/C 6.181 8.20 T/C 6.181 8.120 T/C 6.181 8.120 T/C 6.181 7.960	T/C LE 8.371

TABLE I (continued)

ITEM	TYPE		LOC	ation	REMARKS
NUMBER	SENSOR	AXIAL	RADIAL	CIRCUMFERENTIAL	RIMAKAS
101	Atmos				Barometric Pressur
103	PS				Venturi Throat
105	PS				Venturi Cavity
107	PT				Plenum
109	PS	-0.25	ID	315*	Casing (Same as 751)
111	PS	-0.25	OD	315°	Casing
113	PS	0.00	OD	306°	Casino
115	PS	0.25	OD	294*	Casing
117	PS	0.50	OD	180°	Craing
119	75	0.75	00	190°	Vasing
121	PS	1.00	OD	310°	Casing
123	PS	1.25	OD	170°	Casing
125	PS	1.50	OD	290*	Casing
127	PS	1.75	00	301	Casing
129	PS	2.00	œ	160*	Casing
131	PS	3.227	8.163	Vane 16	Section Side Vame
133	PS	3.393	8.175	Vane 16	Suction Side Vane
135	PS	3.361	8.184	Vane 16	Suction Side Vane
137	PS	3.837	8.190	Vane 16	Suction Side Vame
139	PS	4.115	8.191	Vane 16	Suction Side Vane
141	Ref.			7,200	Not Used
143	Ref.			· · · · · · · · · · · · · · · · · · ·	Atmos.
145	Ref.			· · · · · · · · · · · · · · · · · · ·	15 PSIG Reference
147	Ref.				30 PSIG Reference
14/	Wer.	 			30 TOIG RELECTION
201	Atmos	 			Barometric Pressure
203	PS	· · · · · ·			Same as 103
205	PS				Same as 105
207	PT				Same as 107 and 752
209	PS	4.281	8.192	Vane 16	Suction Side Vame
211	PS	4.559	8.194	Vane 16	Suction Side Vane
	PS				
213		-2.00	ID)		Two Manifolded Tape
215	PS	-2,00	II)	225 & 315	Two Manifolded Tape
217	PS	-2,00	88	45° & 135°	Two lamifolded Tape
219	PS	-2.00	00	225° & 315°	Two Manifolded Tabe
221	PS	2.25	တ	Vanes 18.22.	Pour Manif. Taps
	nc			40 & 44	
223	PS	2.25	ID	113.5°.156.5°	Four Manif. Tabe
<u></u>	 			290.5°&334.5°	
225	PS	6.181	00	60°	Casing
227	PS	6.181		120°	Casipq
229	PS	6.181		252*	Casing
231	PS	6,181		300°	Casing
253	PS	6.181		\$Q*	Casino
235	PS	6.181		120*	Casing
237	PS	6.181		252*	Casing
239	PS	6,181	ID	300°	Casing

TABLE I (continued)

241 243 245	SENSOR Ref.	AXIAL		37.8	
243	Ref.		KAULAL	CIRCLES TRUCKS	RIMARKS
					for lines
245	Ref.				Atmos.
<u></u>	Ref.		-		15 PSIG Reformes
247	Ref.				90 PSIG Reference
301					for lead
303					Not lines
305	P S	3.393	8.175	Vane 17	Free. Side of Valle
307	PS	3.837	8,189	Vane 17	Pres. Side of these
309	PS	4,281	8,191	Vege 17	Tree Star of Man
331	PI	LE	8.371	Vene 20	Leading More
333	PT	LE	8.371	Years 45	Landin Mar
315	77	LE	8.251	Trace M	
317	PI	LE	8,251	thee 47	
319	PŢ	LE	8,121	Space 20	Legisland - Mark
201	PT	LE	0.0	thee 40	
323	PT	LE	8,001	Vane 18	Lagding Man
325	PT	LE	8.001	Vane 47	Leading Bine
327	PT	LE	7.871	Vane 20	seding bigs
329	PT	LE	7.871	Vene 40	Leeding Bige
331	PT	6.181	7,800	20'47'	Mach. Rake Manual
333	PT	6.181	7.80C	52*37*	Disch. Rake Klement
335	PT	6.181	7.800	195*29*	Disch. Rolte Element
337	PT	6,181	7.800	227°49'	Mach. Rate Blooms
339	PT	6.181	7.800	260° 81	Disch, Rake Elegant
341	Ref.				let lised
343	Ref.				Atmos.
345	Ref.				15 PSIG Reference
347	Ref.				30 PSIG Reference
401	PT	6.181	7.960	20*47*	Disch. Rake Element
403	PT	6.181	7.760	52*57*	Mach. Rake Mement
405	PT	6.181	7.960	195'29'	Misch. Nake Misment
407	PT	6.181	7.960	227 49	Mach. Rake Blemant
409	PT	6.181	7.960	260* 8*	Disch. Rake Riement
411	PT	6.181	8.120	20 47	Mach. Rake Element
413	PT	6.181	8.120	52*71*	Disch. Rake Element
415	þŵ	6,181	8.120	195*29'	Disch. Rake Flencht
417	PT	6.181	8.120	227*491	Disch. Rake Menent
419	PT	6.181	8.120	260° 81	Disch. Rake Element
421	PT	6.181	8.280	20 47	Disch. Rake Blement
423	PT	6.181	8.280	52*57*	Disch. Rake Element
425	PT	6.181	8,280	195*29*	Disch. Raise Desert
427	PT	6.181	8.280	227*49*	Disch. Rake Element
429	PΫ́	6.181	8,280	260° 8'	Disch. Rake Elevent
431	PT	6.181	8.440	20°47'	Disch. Rake Alement
433	PT	6.181	8.440	52*571	Disch. Rake Element

TABLE I (concluded)

ITEM	TYPE	ROCATION			
MINER	SAMOOR	JATEA.	PARKAL	CTACHERERETAL	REMARKS
435	PX	6.181	8.440	195*29*	Disch. Rake Element
437	77	6.181	8.440	227*491	Disch. Rake Klevent
439	71	6.181	8.440	260 8	Disch, Rake Element
441	Ref.		1		Not Used
443	Ref.	†	t		Atmos.
445	Ref.	 			15 PSIG Reference
447	Ref	 	}		90 PSIG Reference
		1		<u> </u>	
700	XPI	-0.25	CO	67*16*	Finsh MrD. Kistler
701	201	0.00	oo	75"28"	Plush Mrb. Kistler
702	XPI	0.25	00	60*	Flush MED. Kistler
703	27	0.30	100	68"49"	Plack MD. Kistler
704	X23	0.75	oo	53°53'	The MED. Kielle
705	NPT.	1.00	00	63°16°	First Mr. Kistler
706		1.25	GD .	49° 8'	Plack MID. Matter
707	181 181	1.50	CO	59*23*	Minch Made Carline
708		102	100	37.43	
709		 	 		
710	Pros.	1.25	00	39°	
720	FEGG	1.023	100	37	Bentley Tran duper
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<u> </u>	<u> </u>	1	<u> </u>	<u> </u>	

TABLE II CALIBRATION OF SAMPLE THERMOCOUPLES

BATH °C	SET PT	AVG. OF 9 SAMPLES	MAX. SPREAD
65	148.1	148.4	0.1
100	211.4	210.9	0.1
150	300.8	301.4	0.4
175	346.5	346.4	0.5

A Gil Bath Set Pt.

TABLE III CALIBRATION OF TEMPERATURE READOUT ELECTRONICS

SET PT. Avg+ °F	PRINTER OUTPUT Avg* °F	MAX. SPREAD ± °F
148.2	148.3	0.2
210.7	210.7	0.2
301.7	301.7	0.3
345.4	345.5	0.4

Average of two calibrated T/C's. Average of eight channels.

B Mueller bridge readout converted to temperature.

TABLE IV
MASS AVERAGED COMPRESSOR PERFORMANCE

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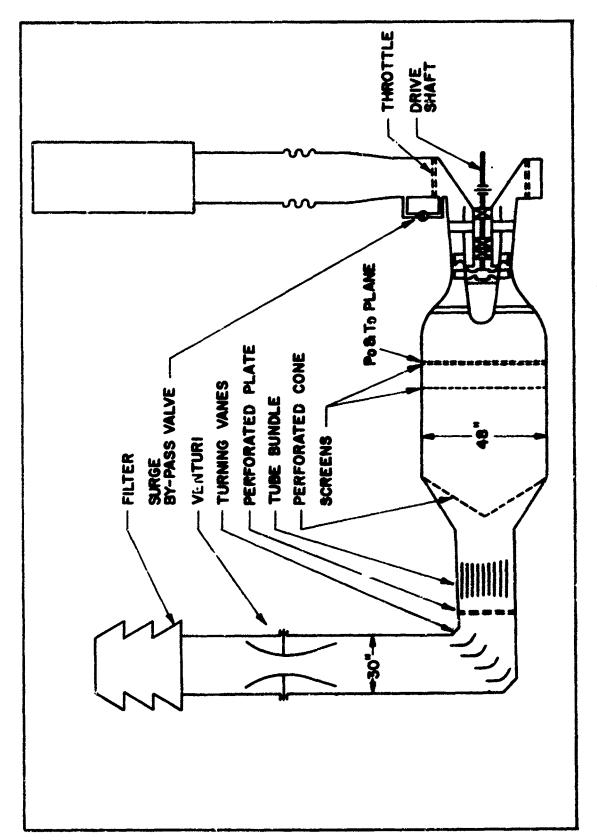
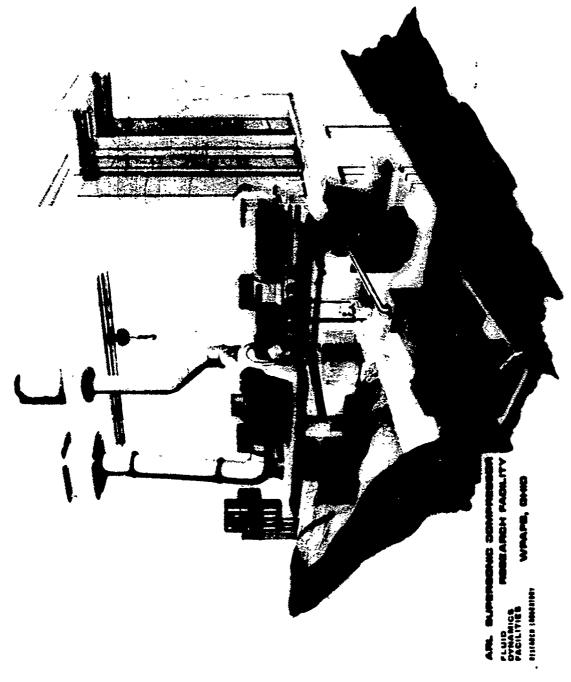


FIGURE 1. COMPRESSOR FACILITY FLOW PATH



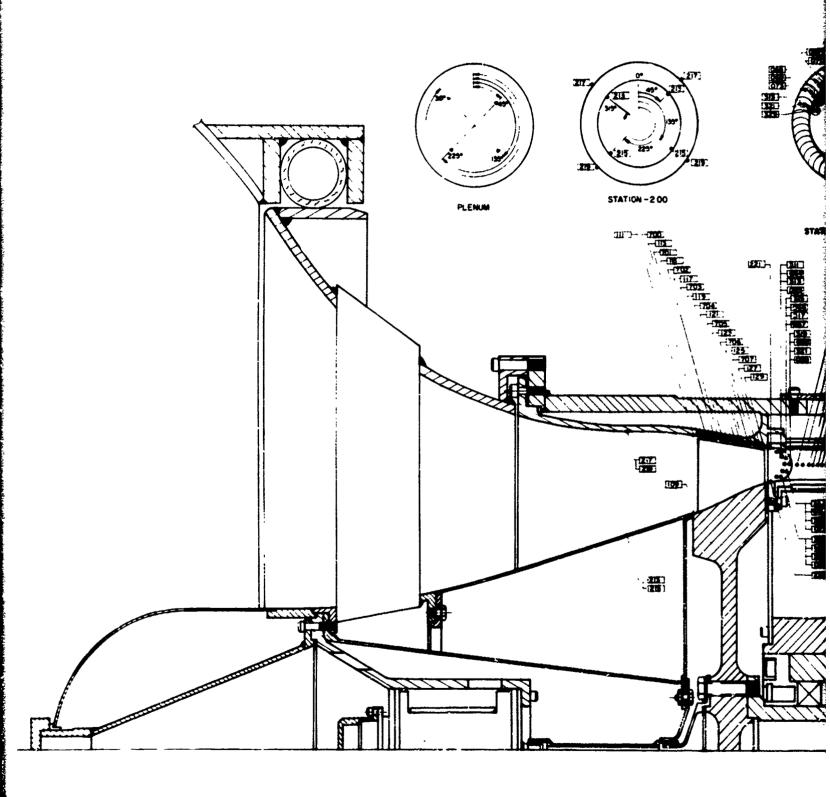
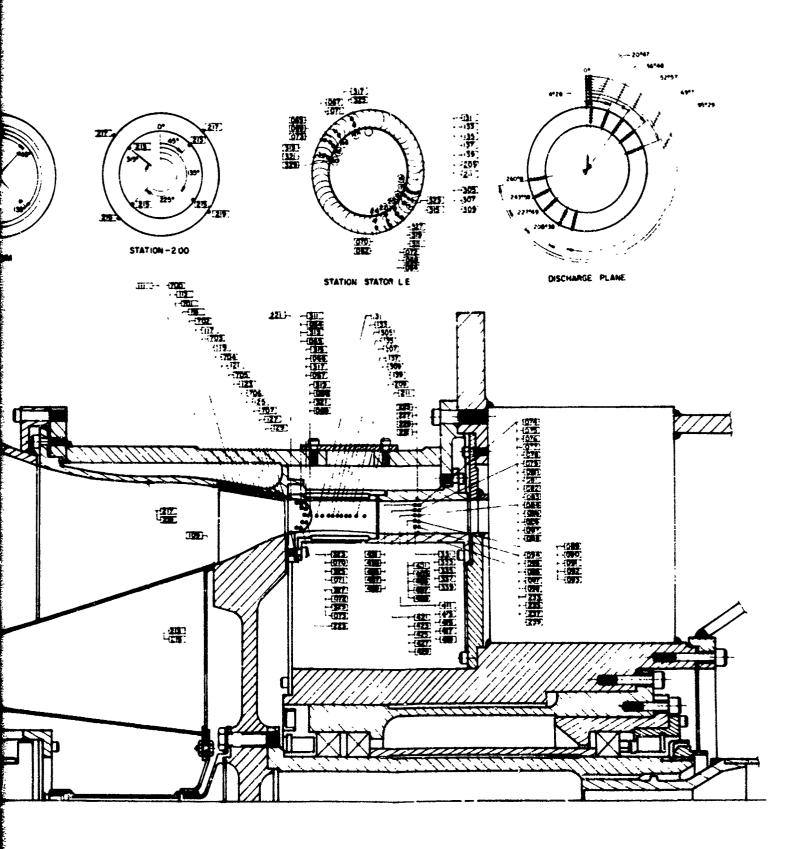


FIGURE 3. COMPRESSOR CROSS SECTION WITH INSTRUMENT/ LOCATIONS



3. COMPRESSOR CROSS SECTION WITH INSTRUMENTATION LOCATIONS



FIGURE 4. ROTOR WITH SPLITTER VANES



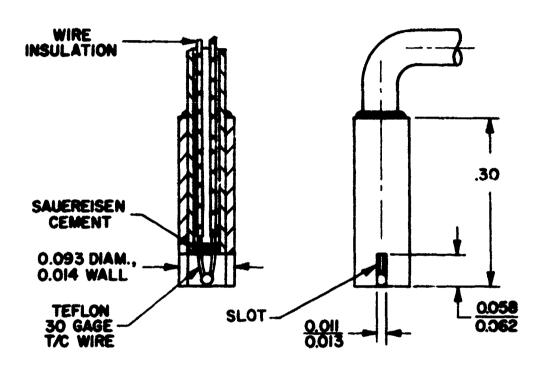


FIGURE 6. SLOT VENTED TEMPERATURE PROBE DESIGN

. 1,

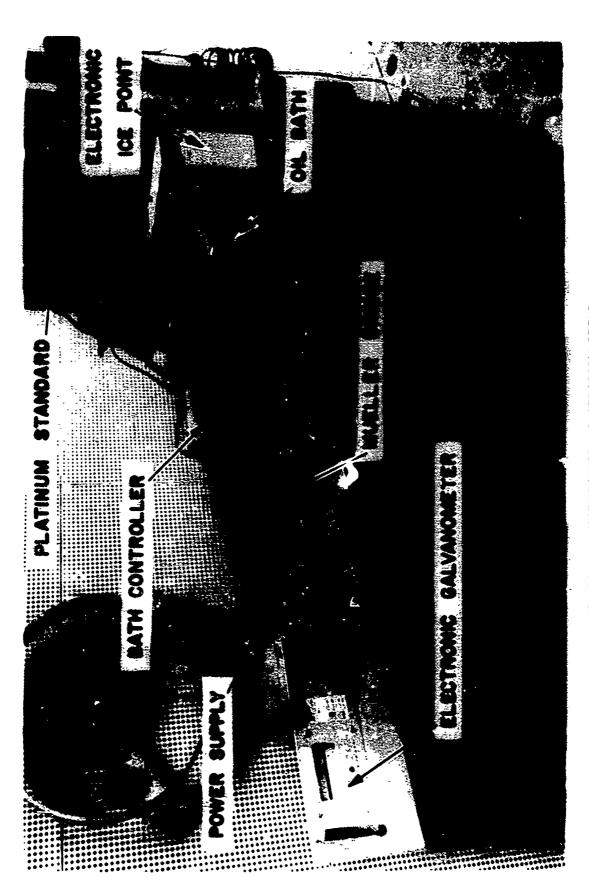


FIGURE 7. TEMPERATURE CALIBRATION SETUP

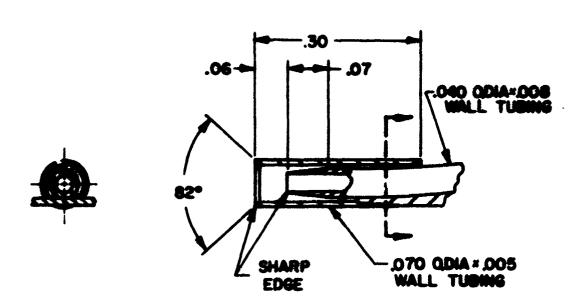


FIGURE 8. KIEL STAGNATION TUBE DESIGN

FIGURE 9. INSTRUMENTATION RAKES

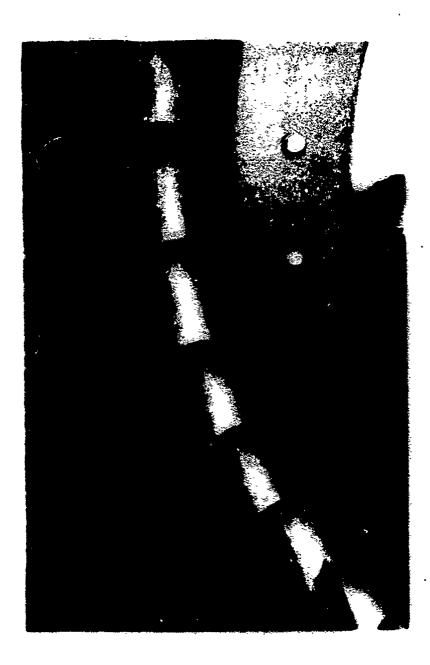


FIGURE 10. VANE-HOLANTED INSTRUMENTATION

THE PARTY OF PROPERTY OF PROPE

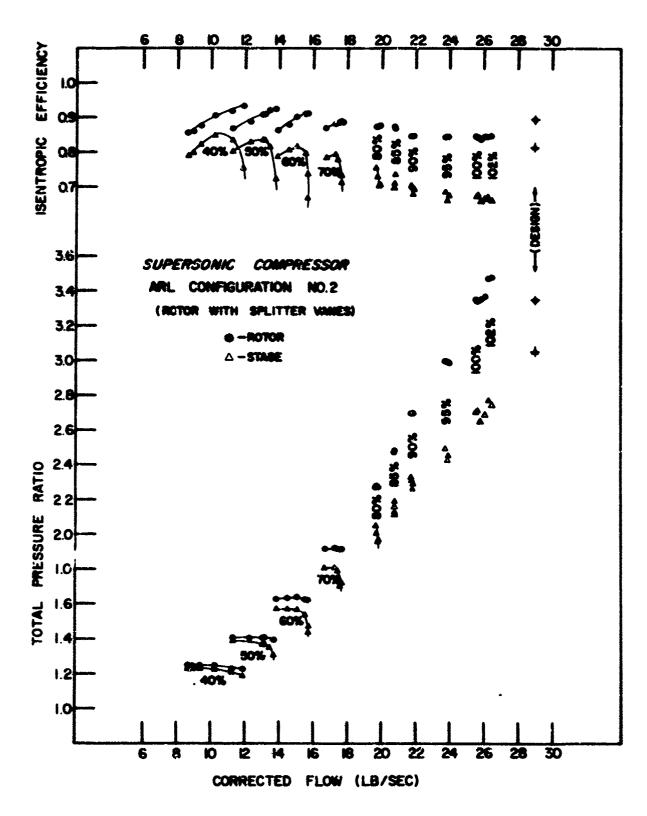
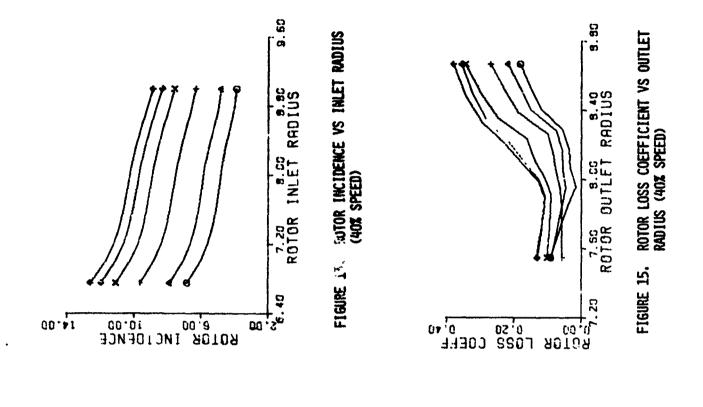


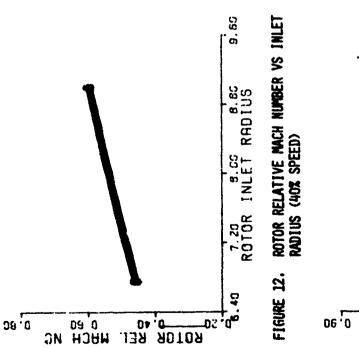
FIGURE 11. COMPRESSOR PERFORMANCE MAP

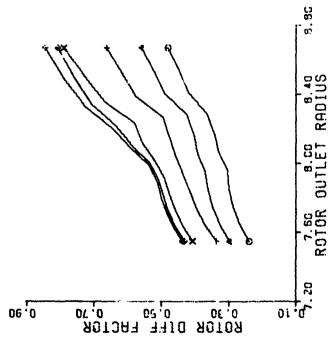
TABLE V

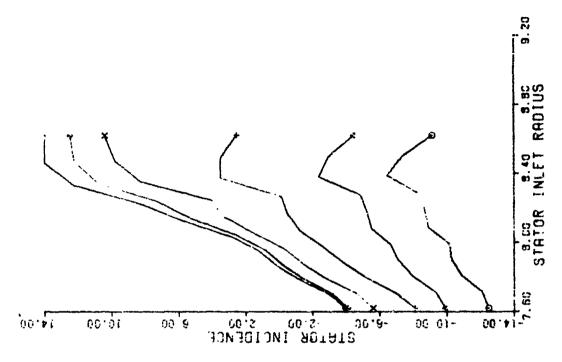
IDENTIFICATION OF SYMPLS FOR 401-SPEED ACROSS-MANE FIGURES

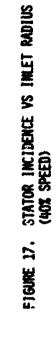
TEST IDENTIFICATION	SYMMOL
212050109840	۵
212050213440	▼
212050315040	+
212050415940	×
212050516240	\$
212050616440	4











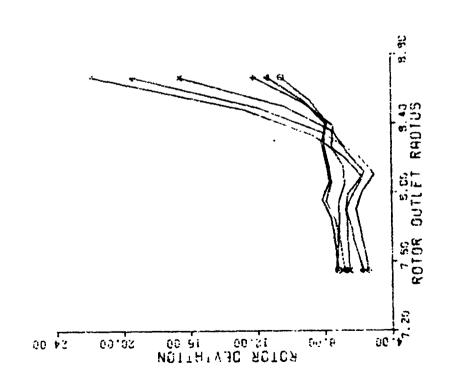
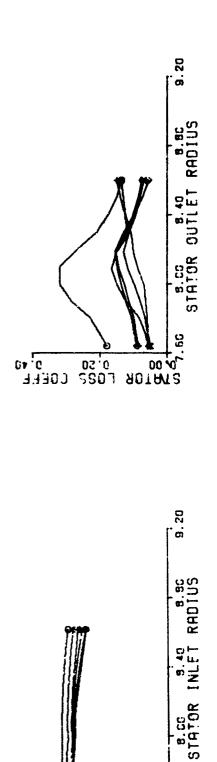


FIGURE 16. ROTOR DEVIATION VS OUTLET RADIUS (40% SPEED)



STATOR MACH NG 0-60 0.40 0.40 0.50

大きないないからないのでもある ヤーン

FIGURE 19. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (40% SPEED)

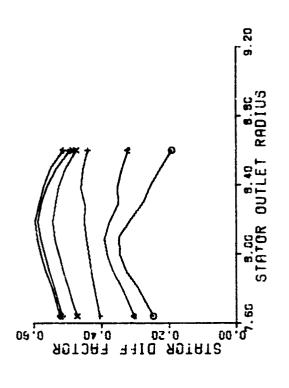


FIGURE 20. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (40% SPEED)

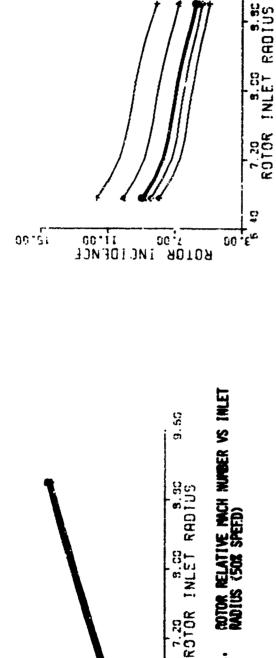
STATOR MACH NUMBER VS INLET RADIUS (40% SPEED)

FIGURE 18.

TABLE VI

IDENTIFICATION OF SYMBOLS FOR 504-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
212050615050	©
21205081575C	Ÿ
212050916250	+
212051015050	×
212051114250	φ
212051212250	4

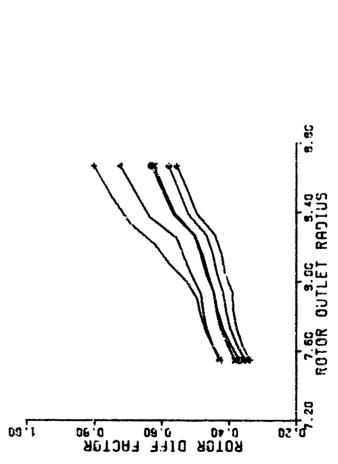


ROTOR RE! MACH

06 0 0N 9. 03

ROTOR INCIDENCE VS INLET RADIUS (SOX SPEED)

FIGURE 22.

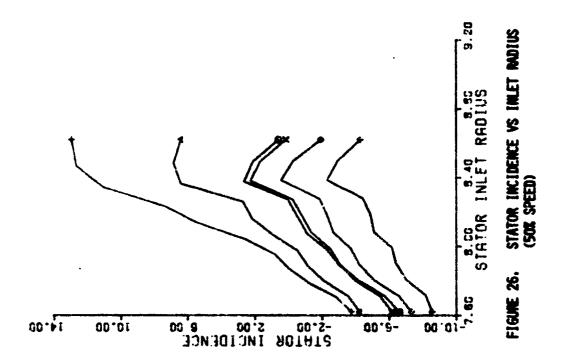


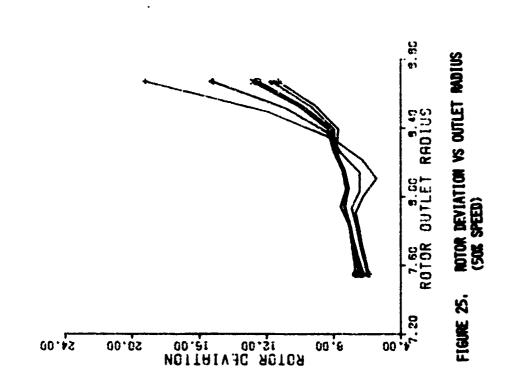
MOTOR DIFFUSION FACTOR VS OUTLET RADIUS (501 SPEED)

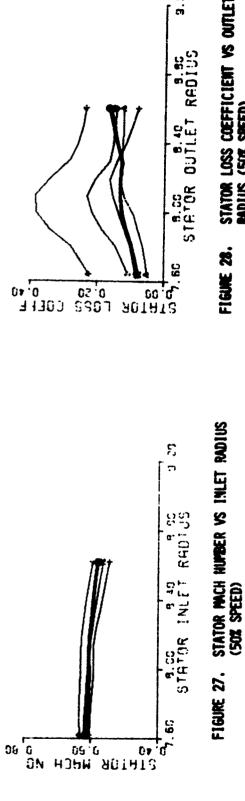
FIGURE 23.

FIGURE 24. ROTOR LOSS COEFFICIENT VS OUTLET
RADIUS (508 SPEED)

F16URE 21.









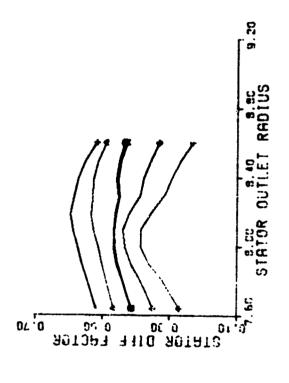
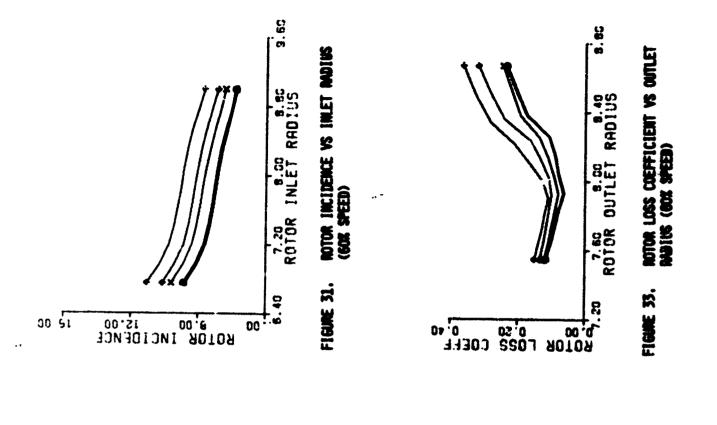


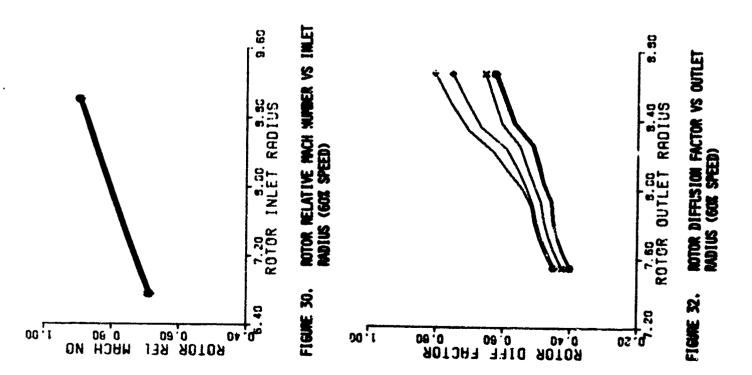
FIGURE 29. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (50% SPEED)

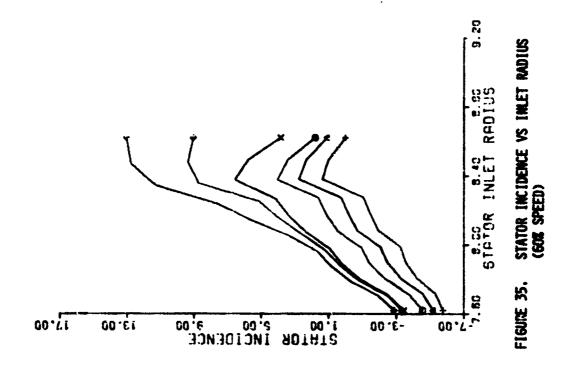
TABLE VII

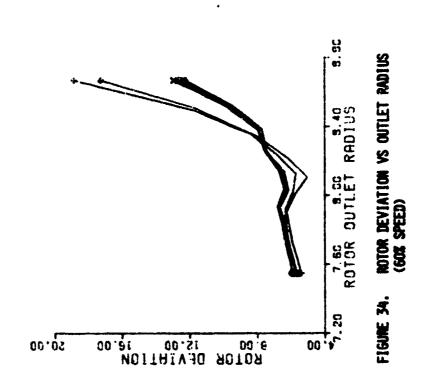
IDENTIFICATION OF SYMBOLS FOR 604-SPEED ACROSS-BLADE FIGURES

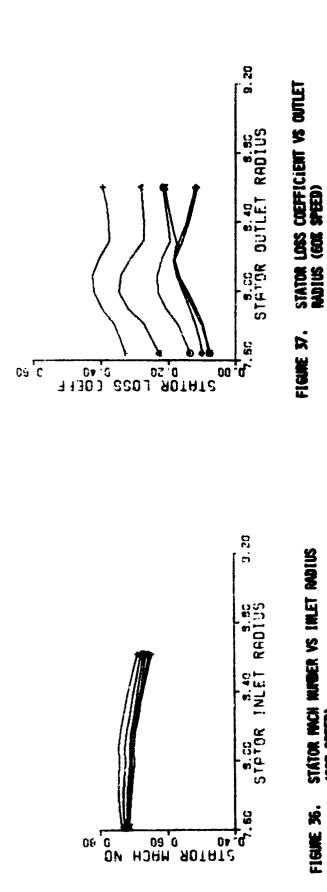
TEST ID ANTIFICATION	SMOOL
212051415060	Ø
212051514360	₩
212051612 9 60	+
212051715560	×
212051815960	•
212051916360	÷

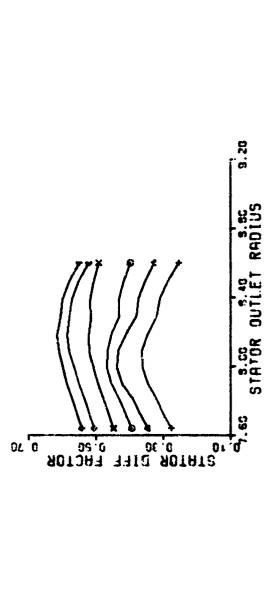












STATOR DIFFUSION FACTOR VS OUTLET RADIUS (GOR SPEED) FIGHE 35.

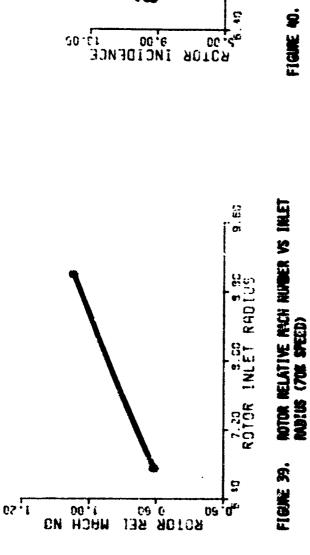
FIGHE 36.

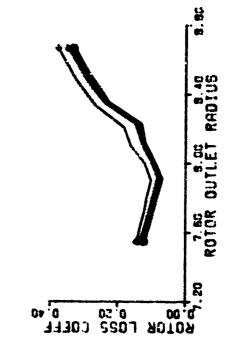
STATOR PACH MANDER VS INLET PADIUS (60% SPEED)

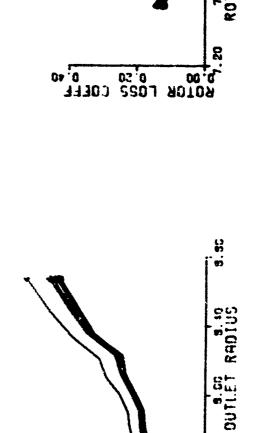
TABLE VIII

IDENTIFICATION OF SOCIALS FOR 700-SPEED ACROSS-BLAGE FIGURES

THE IDENTIFICATION	SPACE
212070215070	©
212070314770	V
212070615070	+
212076715670	×
212970615970	•
212070916170	+







ROTOR DUTILET RADIUS 5, 20 DE .C 80108 THE FACTOR 01.0 02.0 Œ

NOTOR DIFFLUION FACTOR VS OUTLET ANDILE (70% SPEED) FIGURE 41.

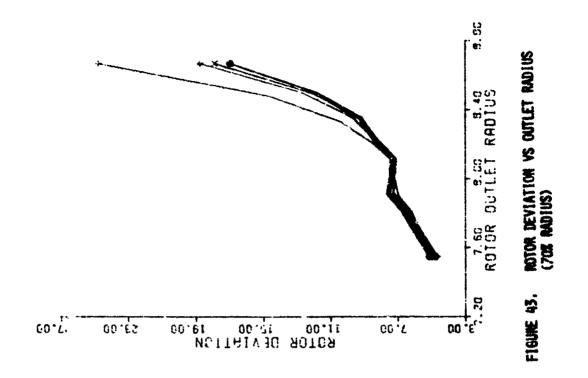
NOTOR LORS CREPTICIENT YS OUTLET NADIUS (70% SPEED)

FIGURE 12.

NOTOR INCIDENCE VS INLET NABIUS (70% SPEED)

FIGURE 40.

7.20 8.50 8.80 ROTOR INLET RROTUS



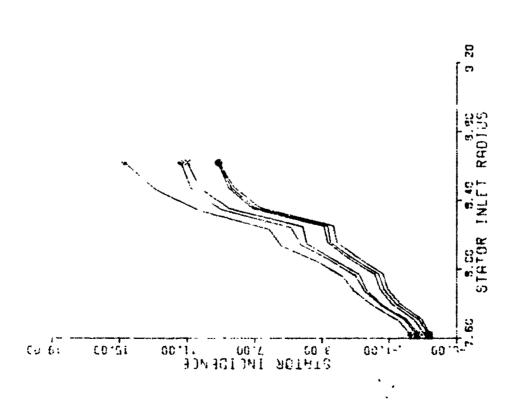


FIGURE 44. STATOR INCIDENCE VS INLET RADIUS (70% SPEED)

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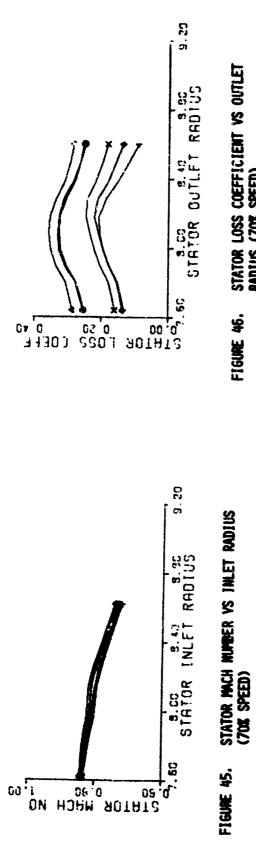
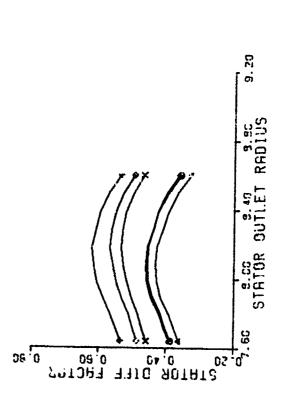




FIGURE 46.

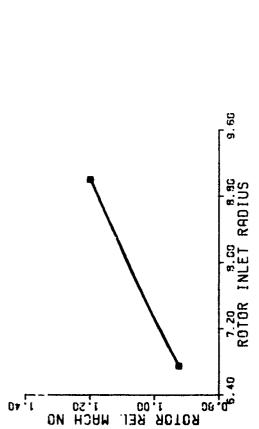


STATOR DIFFUSION FACTOR VS OUTLET RADIUS (70% SPEED) FIGURE 47

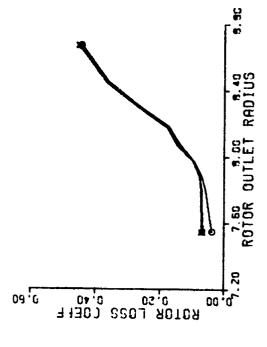
TABLE IX

IDENTIFICATION OF SYMBOLS FOR 80%-SPEED ACROSS-BLADE FIGURES

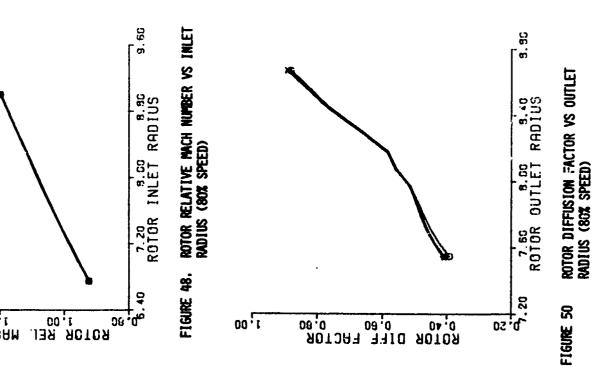
TEST IDENTIFICATION	SYMBOL
212071015080	©
212071315080	▼
212071415580	+
21207151.5980	×

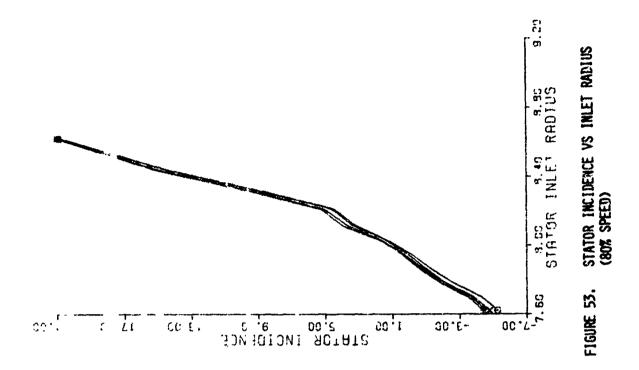


9.60 ROTOR INCIDENCE VS INLET RADIUS (80% SPEED) 7.20 8.00 8.90 ROTOR INLET RADIUS ROTOR INCIDENCE FIGURE 49



ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (80% SPEED) FIGURE 51.





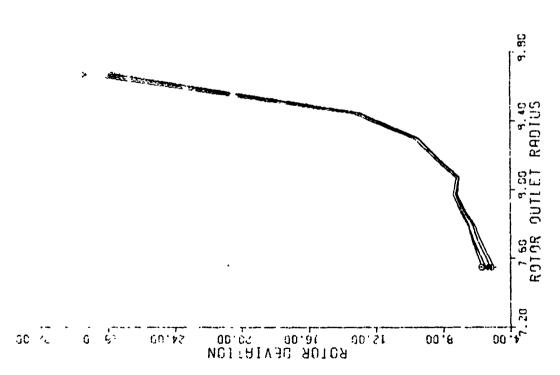
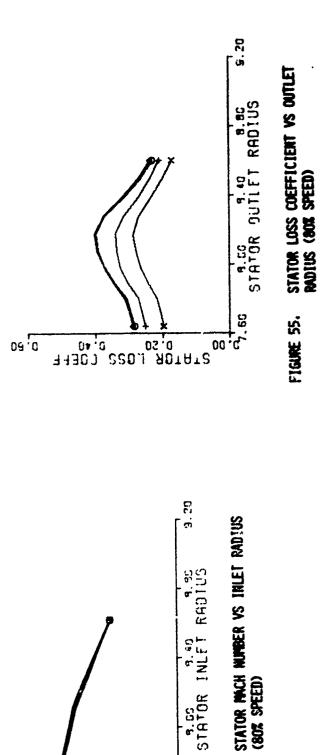
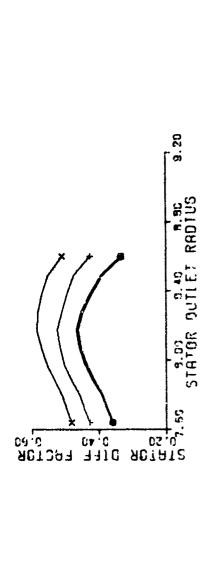


FIGURE 52. ROTOR DEVIATION VS OUTLET RADIUS (80% SPEED)



S: 110R M9CH NO



STATOR DIFFUSION FACTOR VS OUTLET RADIUS (80% SPEED) FIGURE 55.

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FIGURE ST.

FIGURE 55.

TABLE X

IDENTIFICATION OF SYMBOLS FOR 85%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
301180915685	ű.
301181015885	abla
301180615085	7
301180815385	×

FIGURE 58. NOTOR INCIDENCE VS INLET INDIUS (85% SPEED)

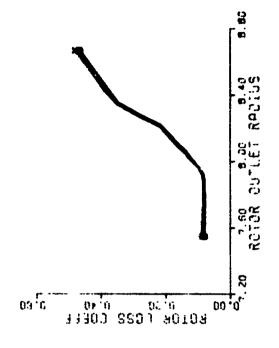
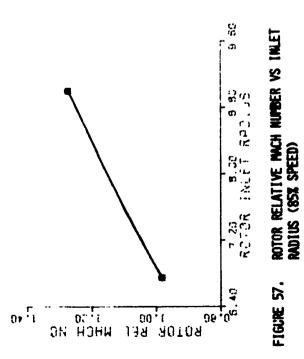
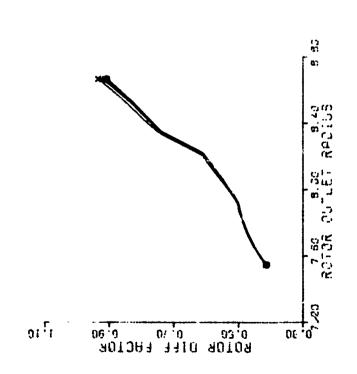
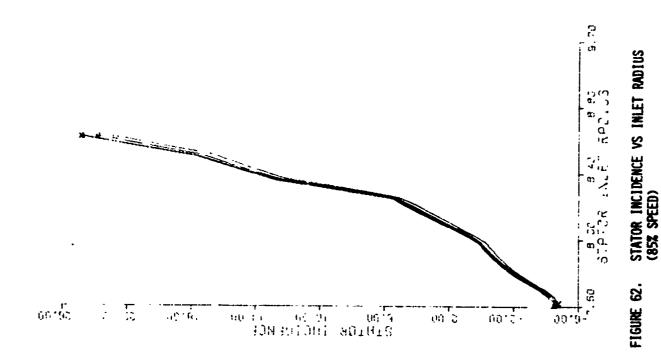
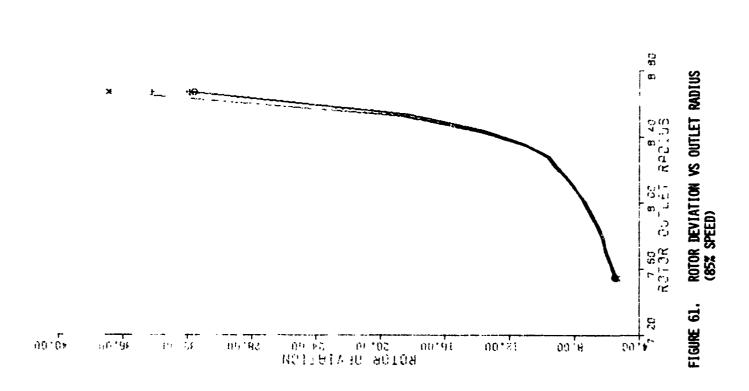


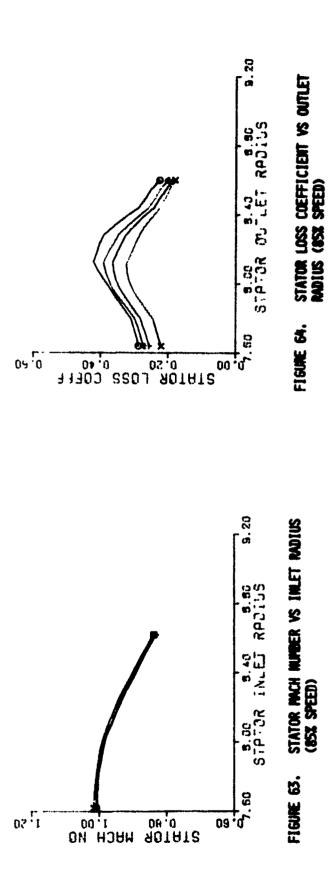
FIGURE 60. NOTOR LOSS CREFFICIENT VS OUTLET NADIUS (85% SPEED)











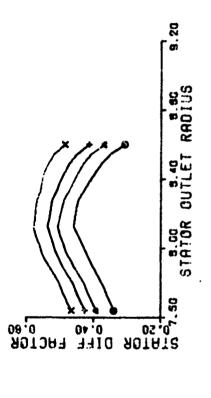


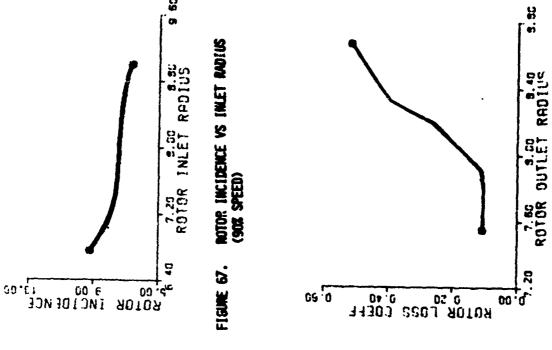
FIGURE 65. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (85% SPEED)

TABLE XI

IDENTIFICATION OF SYMBOLS FOR 901-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
301181515590	Θ
301181615790	₩
301181715 550	+
301181415290	×

9.50 ROTOR INLET RADIUS 01:1

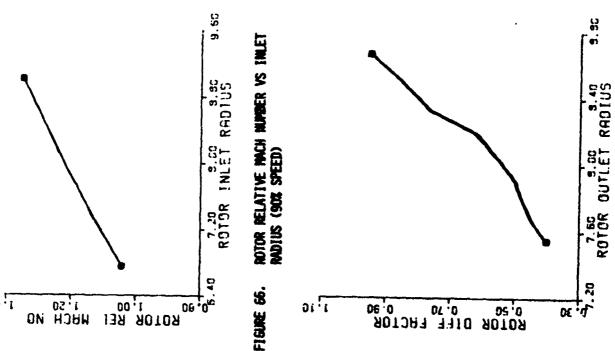


NOTOR LOGS COEFFICIENT VS OUTLET RABIUS (90% SPEED)

FIGURE 69.

NOTOR DIFFUSION FACTOR VS OUTLET MADIUS (90% SPEED)

FIGURE 68.



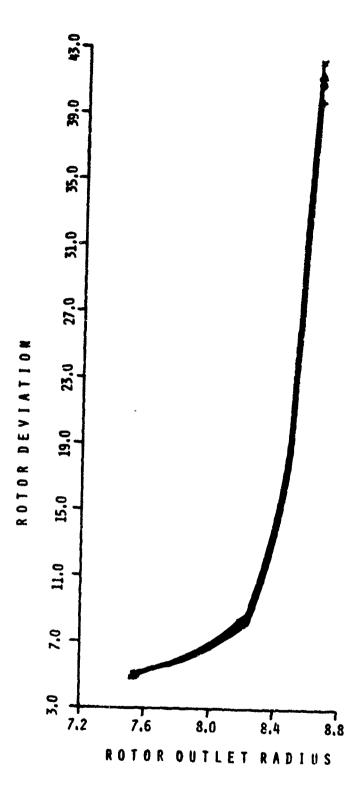


FIGURE 70. ROTOR DEVIATION VS OUTLET RADIUS (90% SPEED)

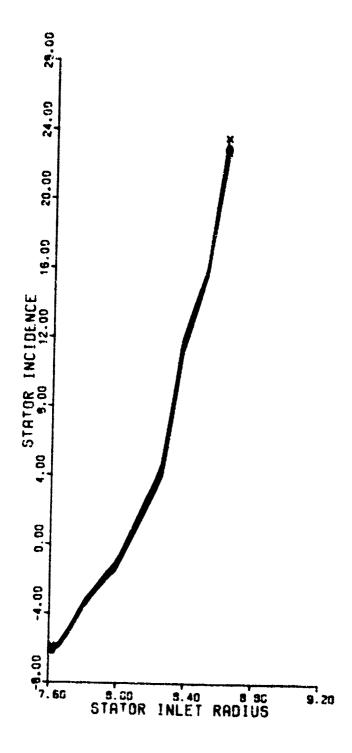
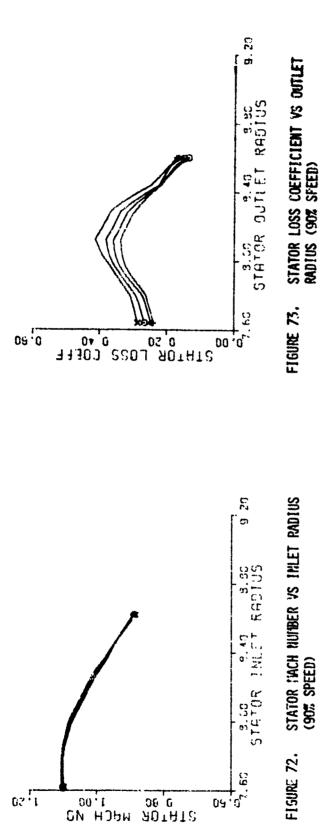


FIGURE 71. STATOR INCIDENCE VS INLET MADIUS (90% SPEED)



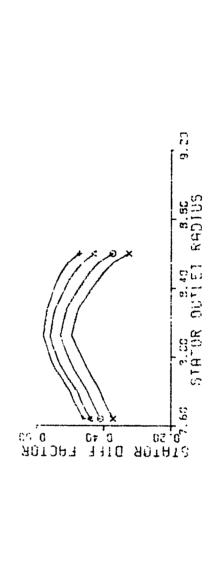


TABLE XII

IDENTIFICATION OF SYMBOLS FOR 951-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYNBOL
301230615095	O
301230415395	Ψ
301230515695	+

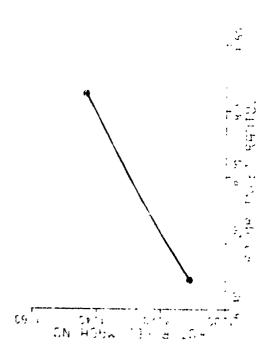


FIGURE 75, ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (95% SPEED)

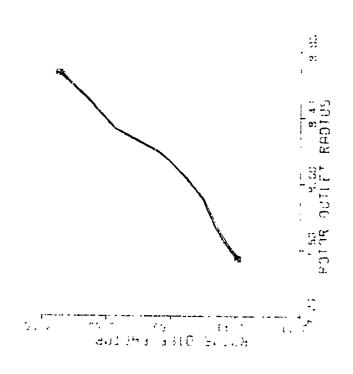


FIGURE 77. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (95% SPEED)

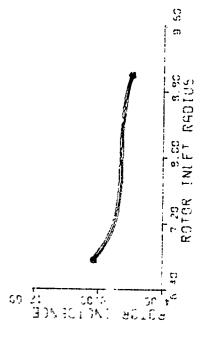


FIGURE 76. ROTOR INCIDENCE :S INLET RADIUS (95% SPEED)

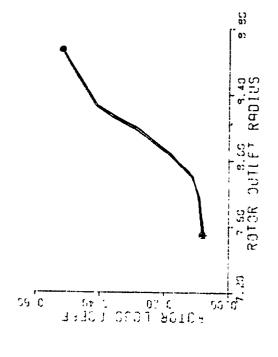


FIGURE 78. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (95% SPEED)

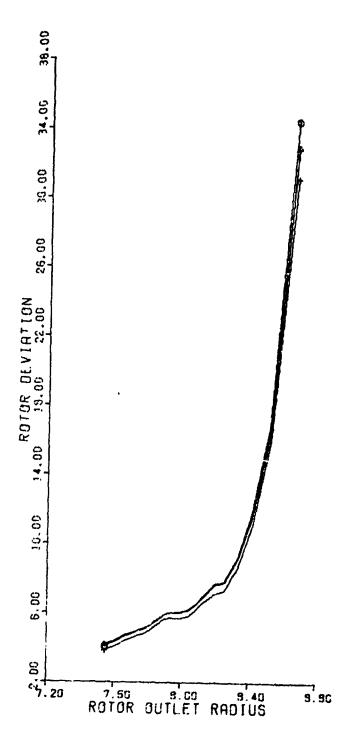


FIGURE 79, ROTOR DEVIATION VS GUTLET RADIUS (95% SPEED)

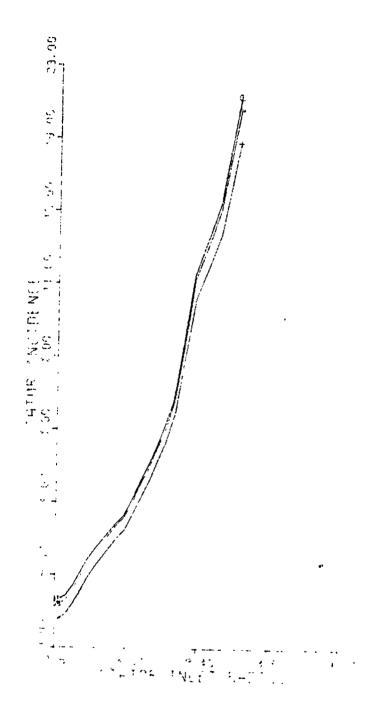


FIGURE 80. STATOR INCIDENCE VS INLET RADIUS (95% SPEED)

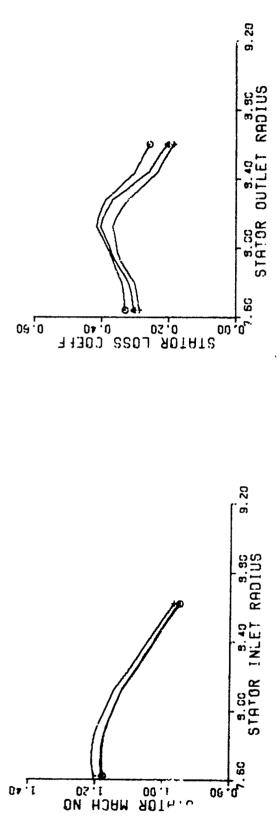


FIGURE 82. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (95% SPEED)

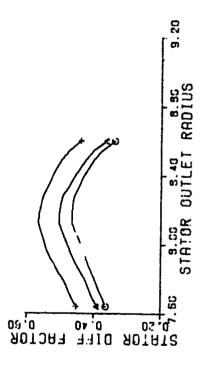


FIGURE 83. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (95% SPEED)

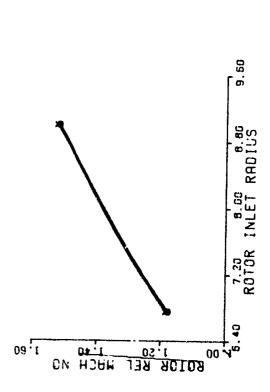
FIGURE 81.

STATOR MACH NUMBER VS INLET RADIUS (95% SPEED)

TABLE XIII

IDENTIFICATION OF SYMBOLS FOR 100%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
301231515600	Ō
301231615700	∇
301231315200	+
301231415400	×



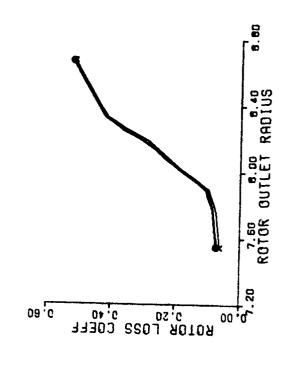
"IGURE 84. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (100% SPEED)

7.20 8.00 8.90 ROIDS

90109 00.10

8:00 15:00 INCIDENCE ROTOR INCIDENCE VS INLET RADIUS (100% SPEED)

FIGURE 85,



ROTOR DIFF FACTOR 0,80

FIGURE 87. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (100% SPEED)

FIGURE 86. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (102% SPEED)

8.80

ROTOR OUTLET RADIUS

03.0

30 [[

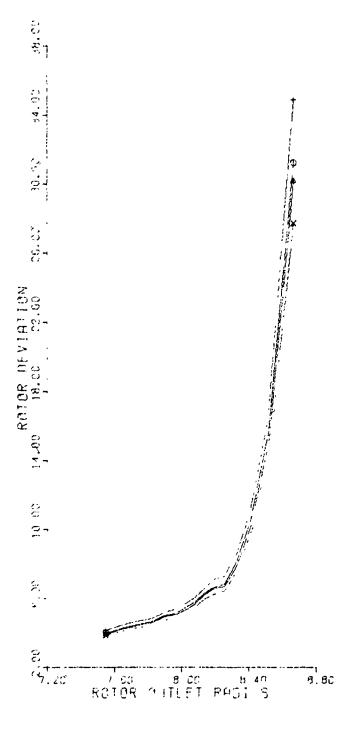


FIGURE 88. ROTOR DEVIATION VS OUTLET RADIUS (100% SPEED)

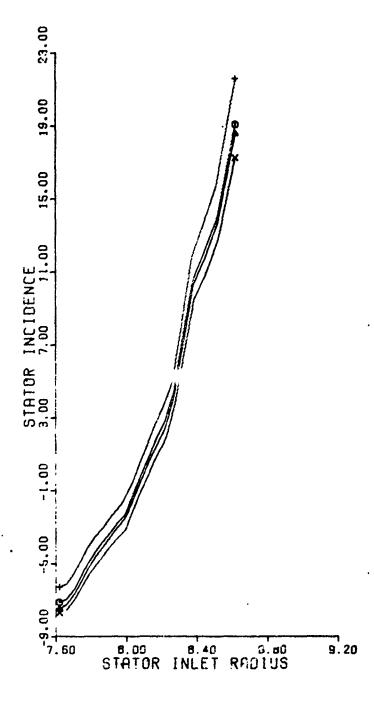
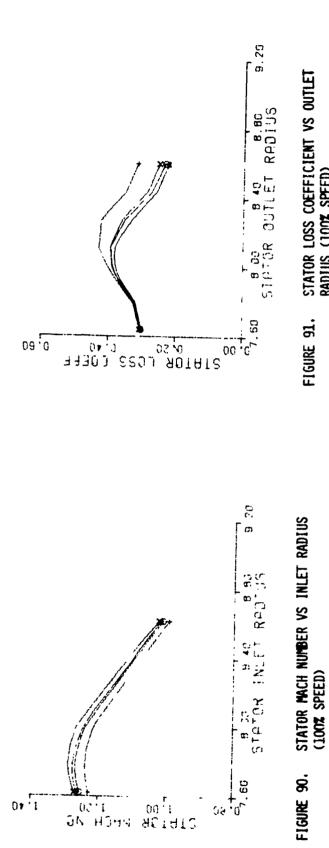
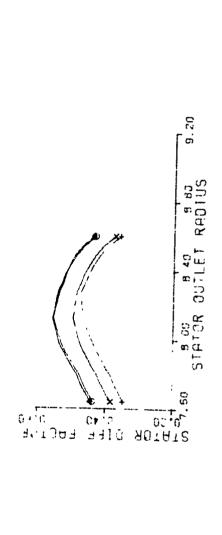


FIGURE 89. STATOR INCIDENCE VS INLET RADIUS (100% SPEED)





STATOR DIFFUSION FACTOR VS CUTLET RADIUS (100% SPEED) FIGURE 92.

STATOR LOSS COEFFICIENT VS OUTLET RADIUS (100% SPEED)

FIGURE 91.

TABLE XTV

IDENTIFICATION OF SYMBOLS FOR 1028-SPEED ACROSS-BLADE FIGURES

TEST TRENTIFICATION	SIMBUL.
301240815302	O
301240915602	₩

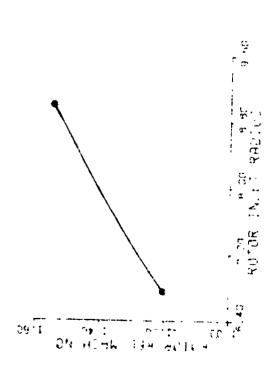


FIGURE 93. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (102% SPEED)

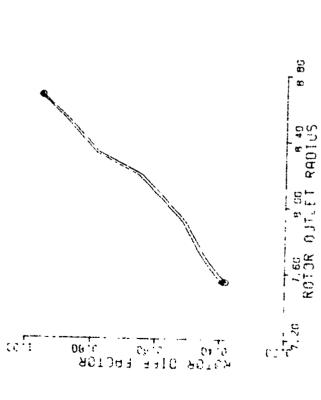


FIGURE 95, ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (102% SPEED)

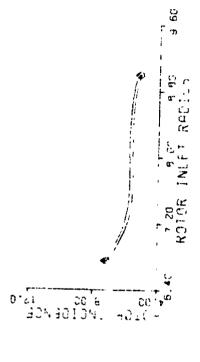


FIGURE 94. ROTOR INCIDENCE VS INLET RADIUS (102% SPEED)

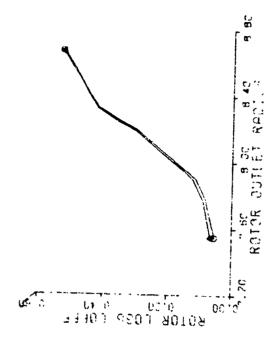


FIGURE 96. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (102% SPEED)

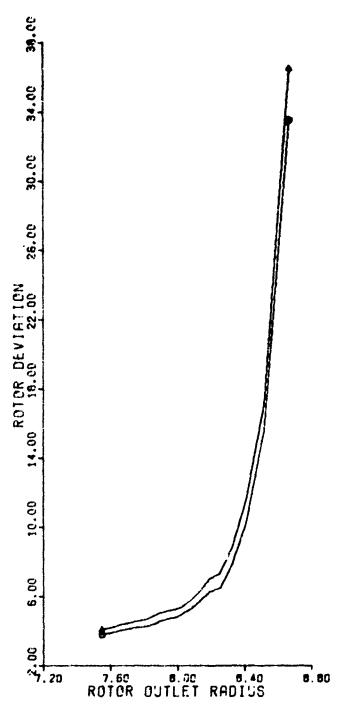


FIGURE 97. ROTOR DEVIATION VS OUTLET RADIUS (102% SPEED)

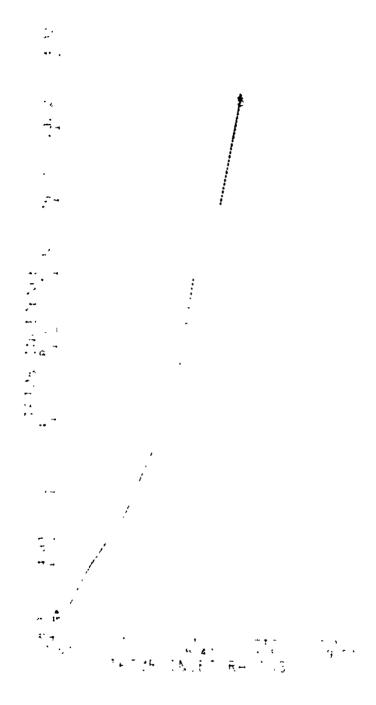
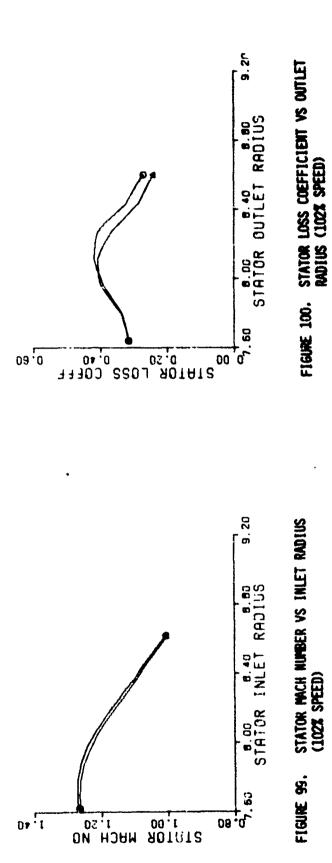


FIGURE 98. STATOR INCIDENCE VS INLET RADIUS (102% SPEED)



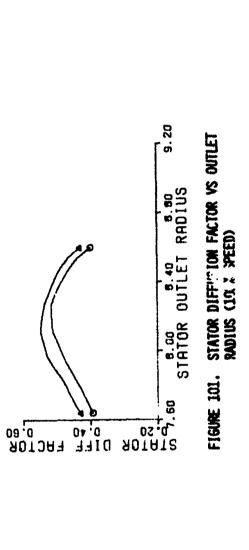


FIGURE 102. ROTOR RELATIVE MACH WUMBER VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

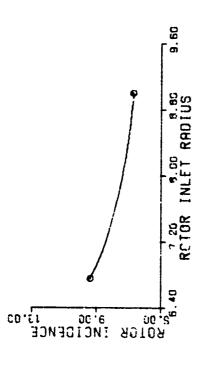


FIGURE 103. ROTOR INCIDENCE VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

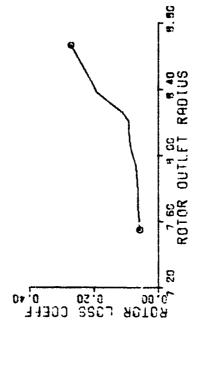


FIGURE 105. ROTOR LOSS COEFFICIENT VS OUTLET NADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

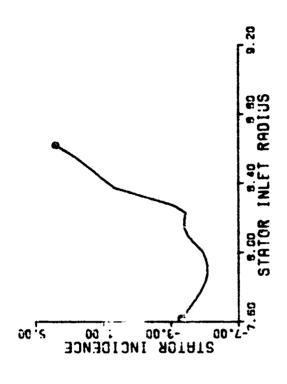
ROTOR OUTLET RADIUS

R010R DIFF

FIGURE 104. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE AMALYSIS, 40% SPEED)

08 .0

FACTOR 0: 60





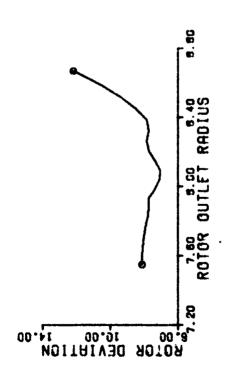
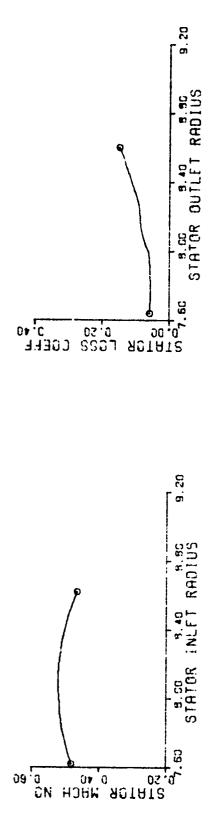


FIGURE 106. ROTOR DEVIATION VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)





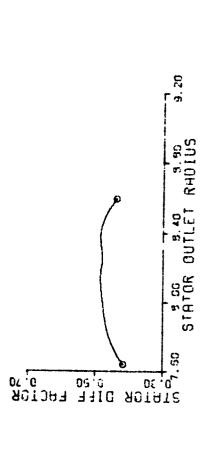


FIGURE 110. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

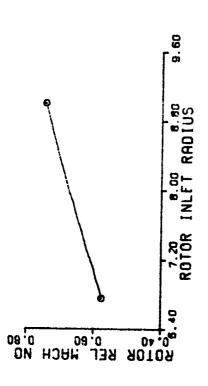
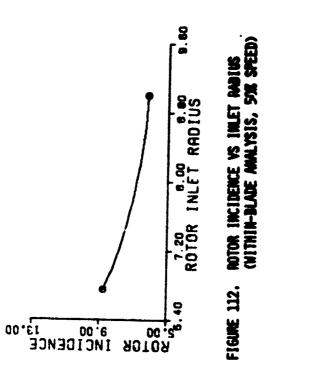


FIGURE 111. NOTOR RELATIVE MACH NUMBER VS INLET RADIUS (WITHIN BLADE ANALYSIS, 50% SPEED)



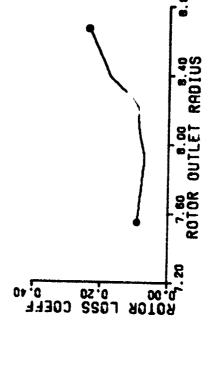


FIGURE 113. ROTOR DIFFUSION FACTOR VS OUTLET MADIUS (WITHIN-BLADE AWALYSIS, 50% SPEED)

7.60 6.00 8.40 ROTOR OUTLET RADIUS

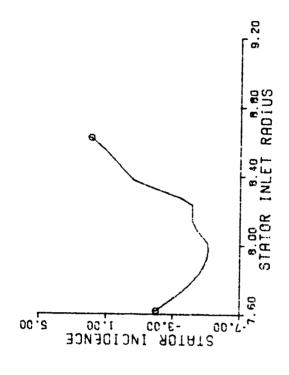
مبرہ 7.20

50

FIGURE 114. ROTOR LOSS CREFFICIENT VS OUTLET MOTUS (WITHIN-BLADE ANALYSIS, SOR SPEED)

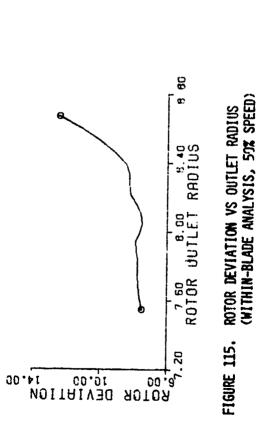
08.0

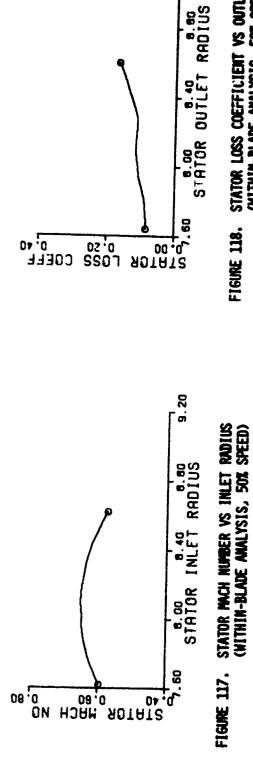
ROTOR DIFF FACTOR 0,0 0,60



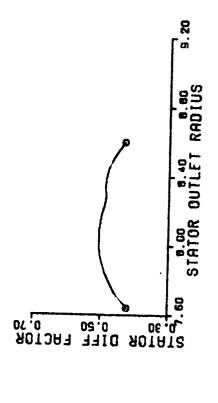
STATOR INCIDENCE VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 50% SPEED)

FIGURE 116.





STATOR LOSS COEFFICIENT VS OUTLET MADIUS (WITHIN-BLADE ANALYSIS, SOR SPEED) FIGURE 118.



STATOR DIFFUSION FACTOR VS OUTLET MAJUS (WITHIN-BLADE ANALYSIS, 50% SPEED) FIGURE 119.

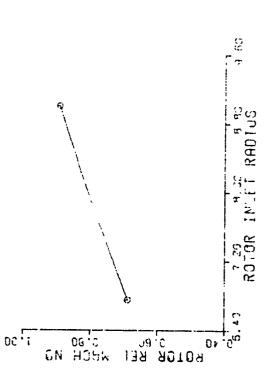


FIGURE 120. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 60% SPEED)

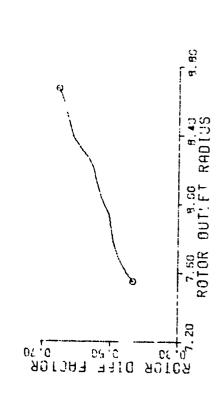


FIGURE 122. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 60% SPEED)

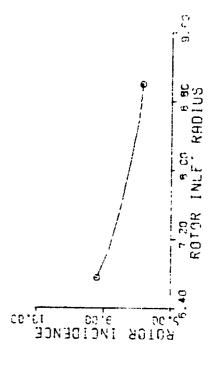


FIGURE 121. ROTOR INCIDENCE VS INLET RADIUS (WITHIN-BLADE ANALYSIS, SOZ SPEED)

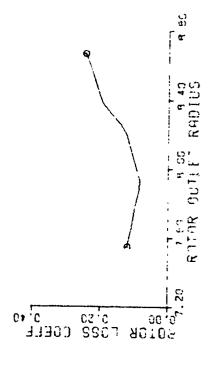
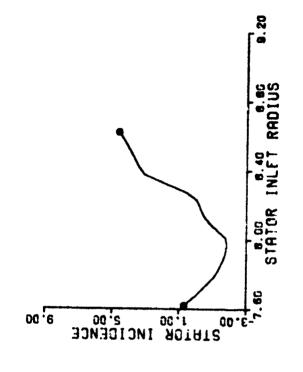
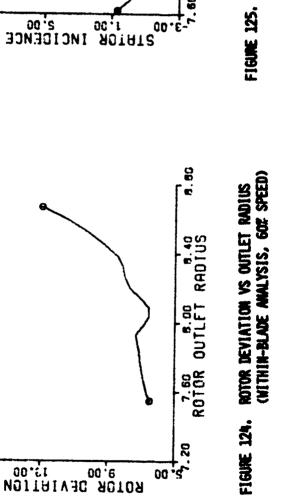


FIGURE 123. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 60% SPEED)



STATOR INCIDENCE VS INLET MOIUS (WITHIN-BLADE ANALYSIS, GOR SPEED)



82

17.00

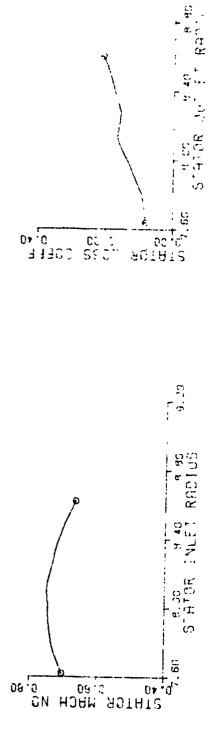


FIGURE 126. STATOR MACH NUMBER VS INLET RADIUS
(WITHIN-BLADE ANALYSIS, 602 SPEED)
FIGURE



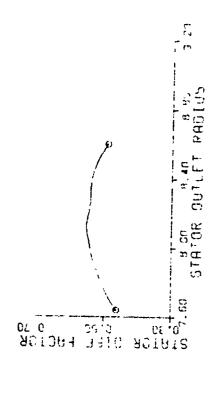


FIGURE 128. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 60% SPEED)

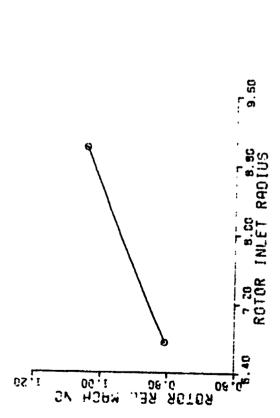


FIGURE 129. ROTOR RELATIVE MICH MUMBER VS INLET RADIUS (WITHIN-BLADE AMLYSIS, 70% SPEED)

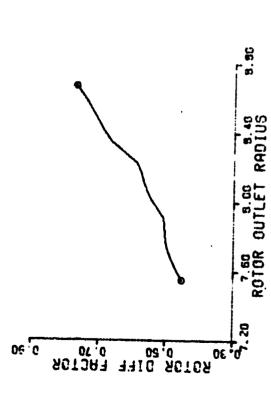


FIGURE 131. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 70% SPEED)

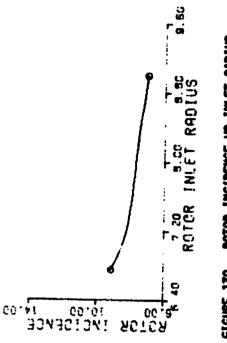


FIGURE 130. ROTOR INCIDENCE VS INLET INDIGE (WITHIN-BLADE ANALYSIS, 70% SPEED)

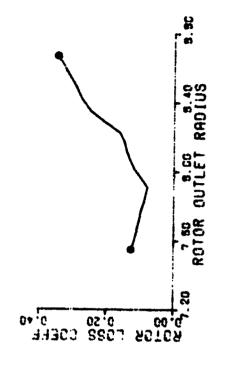
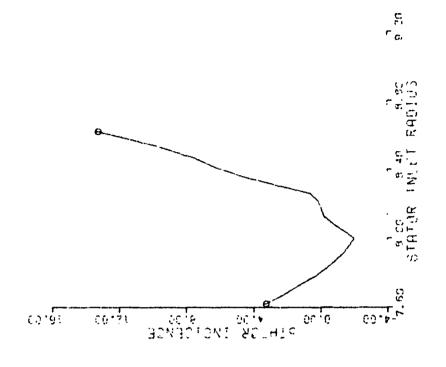


FIGURE 132. NOTOR LOSS CREFFICIENT VS OUTLET MADIUS (WITHIN-BLADE ANALYSIS, 70% SPEED)





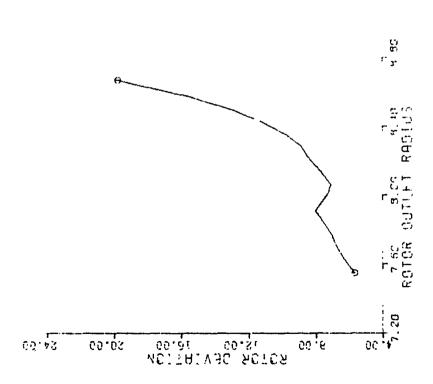


FIGURE 133. ROTOR DEVIATION VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 70% SPEED)

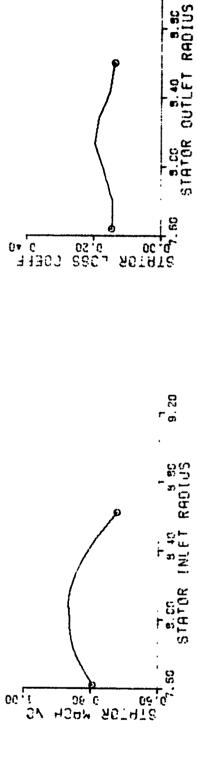


FIGURE 135. STATOR MACH NUMBER VS INLET RADIUS (MITHIN-BLADE ANALYSIS, 70% SPEED)



9.20

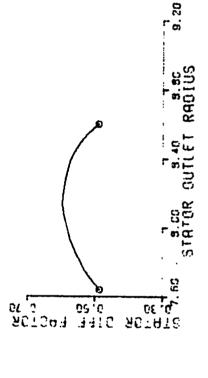


FIGURE 137. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 70% SPEED)

The best of the second desired as a second of the second of the

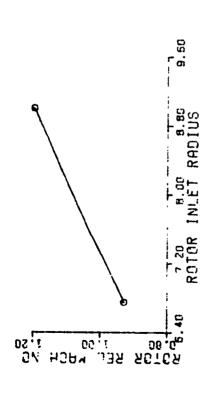


FIGURE 138, ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (HITHIN-BLADE AWALYSIS, 80% SPEED)

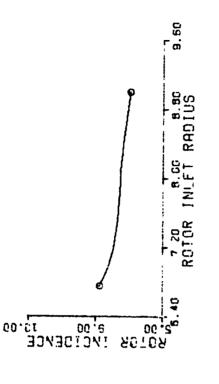
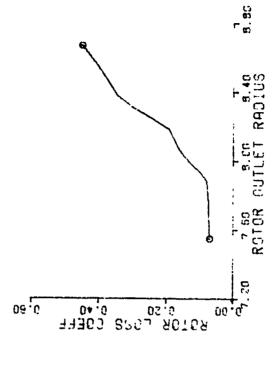


FIGURE 139. ROTOR INCIDENCE VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 80% SPEED)



TET RADIUS FIGURE 141. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (MITHIN-BLADE ANALYSIS, 80% SPEED)

FIGURE 141. ROTOR DIFFUSION FACTOR VS CUTLET RADIUS (NITHIN-BLADE ANALYSIS, 80% SPEED)

ີ. ອີ.ອີດ

> 3.00 8.40 OUTLET RADIUS

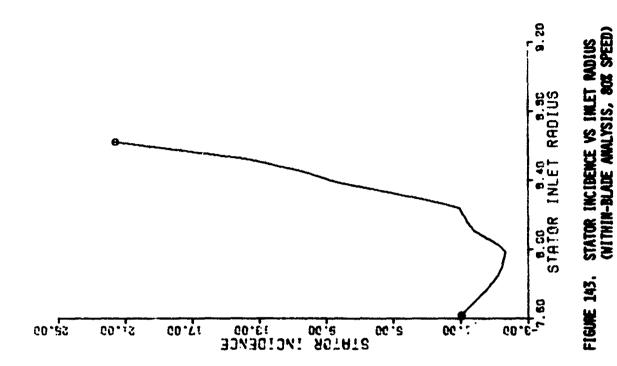
7 6C ROTOR

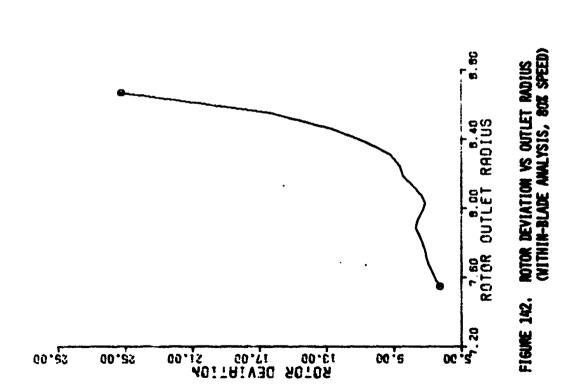
07. G

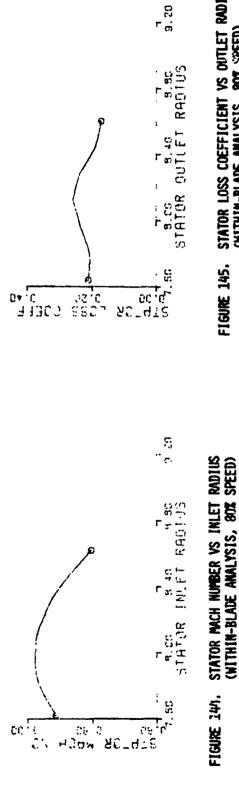
7110 R010R 02,0

05 70

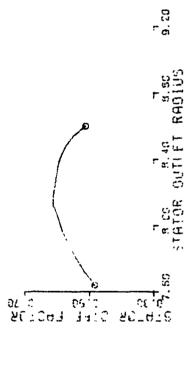
R6T3H∃ or;9







STATOR LOSS COEFFICIENT VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 80% SPEED) F16URE 145.



STATOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 80% SPEED) FIGURE 146.

12. Secretaria de la la constante de la consta

INCIDENCE

FIGURE 147. ROTOR RELATIVE MICH NUMBER VS INLET RAPIUS (MITHIN-BLADE AMALYSIS, 85% SPEED)

9.50

7.20 5.00 9.80 ROTOR INLET RADIUS

ลบาอล 00.a. 5 NOTOR INCIDENCE VS INLET NADIUS (NITHIN-BLADE ANALYSIS, 85% SPEED)

FIGURE 148.

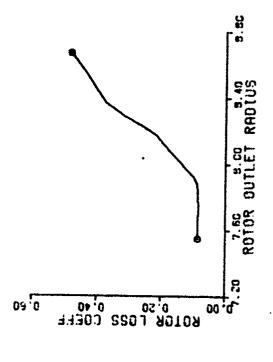


FIGURE 150. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (MITHIN-BLADE ANALYSIS, 85% SPEED)



3 3 3

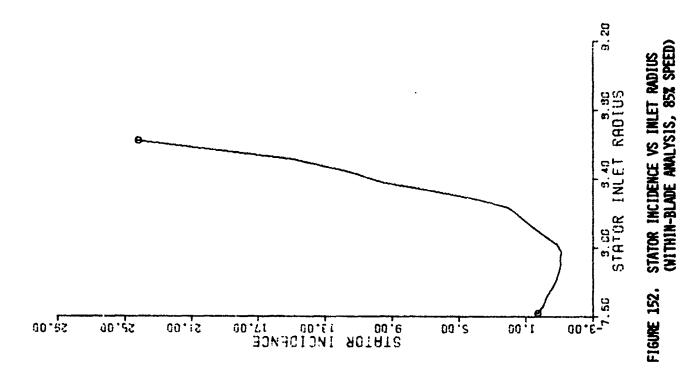
ROTOR BUTLET RADIUS

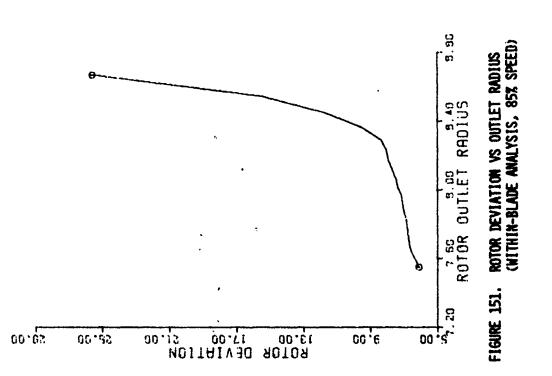
0E .Q.

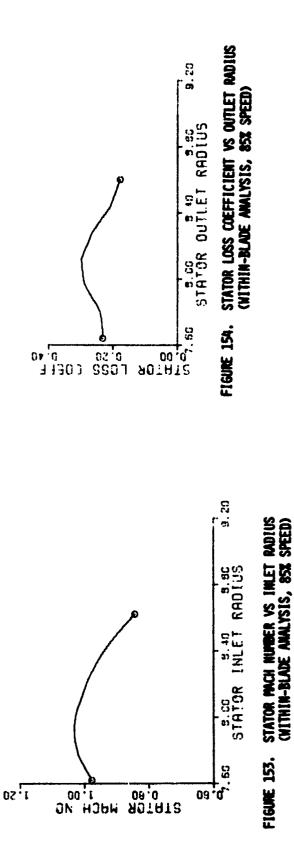
ROTOR DIFF 0,50

06 .0

FACTOR 07:0







STATOR DIFF FACTOR

07.0 02.0 06.0

STATOR DIFFUSION FACTOR VS OUTLET PADIUS (WITHIN-BLADE AMALYSIS, 85% SPEED) FIGURE 155.

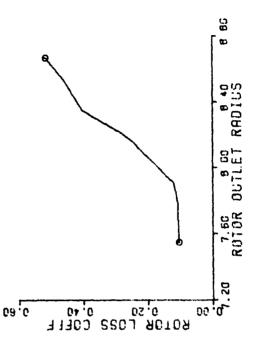
STRICA CUILET RADIUS

ROTOR REL MACH NO 1.20 8.43 7.20 8.00 8.0108 1.NLET RADIUS

FIGURE 157. ROTOR INCIDENCE VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 90% SPEED)

9.60

7,20 8.00 8.80 R0105 R0105



8813R-01FF EACTGR 0,50 67,0 62,0

FIGURE 159. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 90% SPEED)

معام معامدتمة همتا بسماعت مرام ميدونيكو والموضوع ومعاضوه مسمي ومعاق ومعاضية معاهمة ومعاقعة فالمفاقعة والمقافعة والمعافة والمعافقة والمعافقة والمعافة والمعافة والمعافقة وا



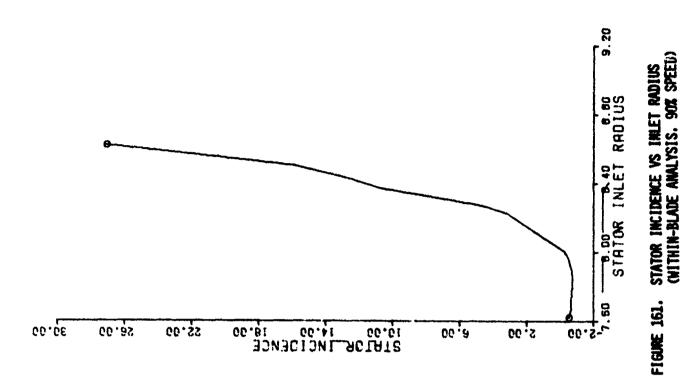
ROTOR OUTLET RADIUS

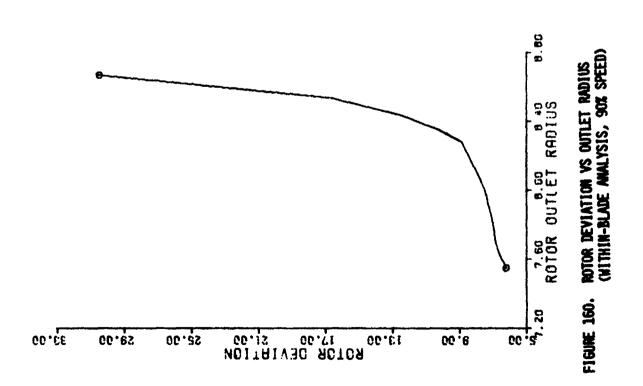
0E.Q.

1710

ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 90% SPEED)

FIGURE 156.





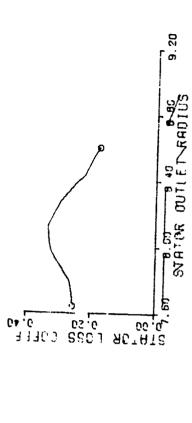


FIGURE 163. STATCR LOSS COEFFICIENT VS OUTLET RADIUS (MITHIN-BLADE ANALYSIS, 90% SPEED)

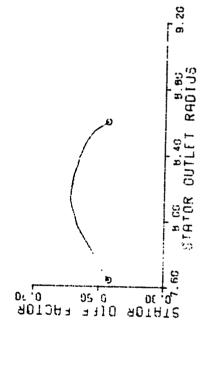


FIGURE 164. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 90% SPEED)

FIGURE 162.

STATOR MACH NUMBER VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 90% SPEED)

SAMTON INLET RADIUS

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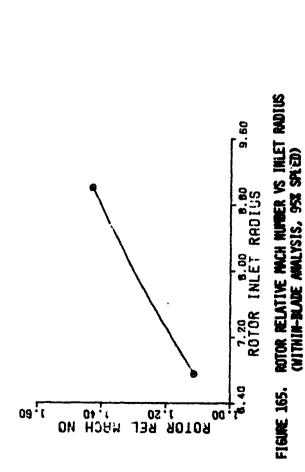
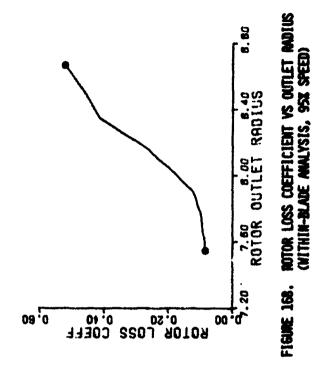


FIGURE 166. NOTOR INCIDENCE VS INCET RADIUS

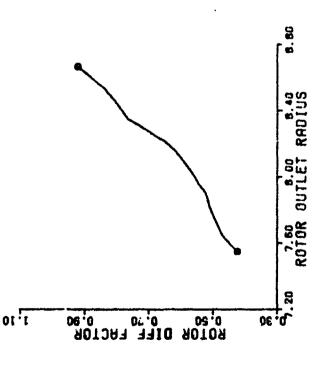
(WITHIN-BLADE AMALYSIS, 953 SPEED)

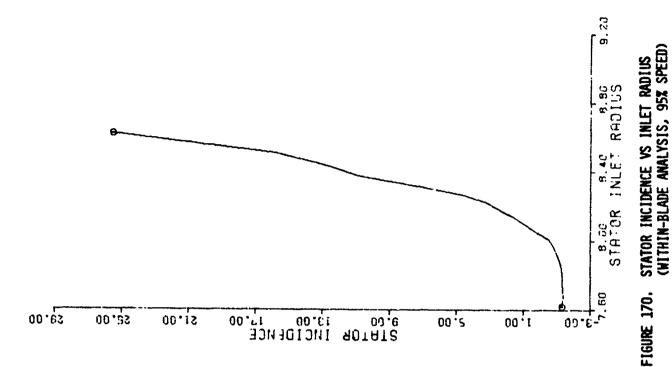


ROTOR DIFFUSION FACTOR VS OUTLET RADIUS

(MITHIN-BLADE AMALYSIS, 95% SPEED)

FIGURE 167.





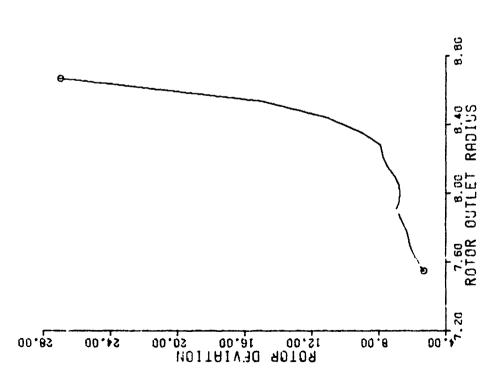


FIGURE 169. ROTOR DEVIATION VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 95% SPEED)

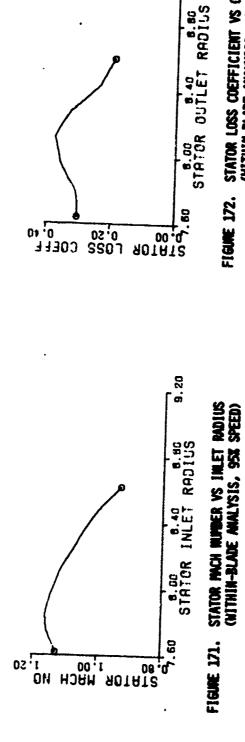


FIGURE 172. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 951 SPEED)

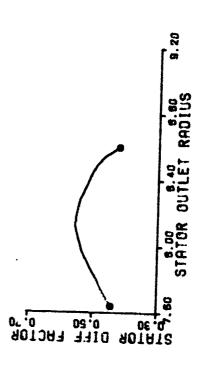


FIGURE 173. STATOR DIFFUSION FACTOR VS OUTLET PADIUS (WITHIN-MADE MALYSIS, 95% SPEED)

ROTOR INCIDENCE

FIGURE 175. ROTOR INCIDENCE VS INLET RADIUS

ROTOR INCIDENCE VS INLET RADIUS

WITHIN-BLADE AMALYSIS, 1003 SPEED)

ROTOR LOSS 6.40

ROTOR 2.00

ROTOR 3.00

ROTOR 3

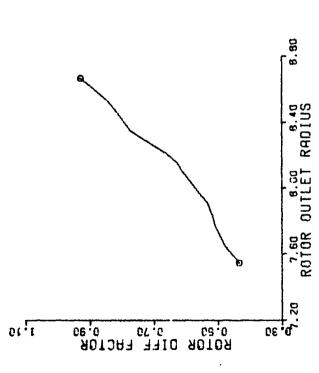


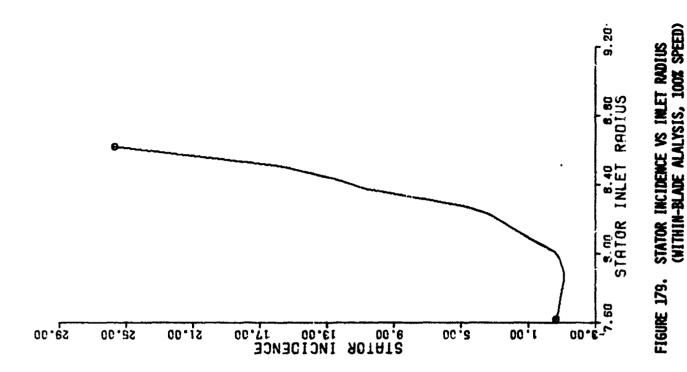
FIGURE 176. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 100% SPEED)

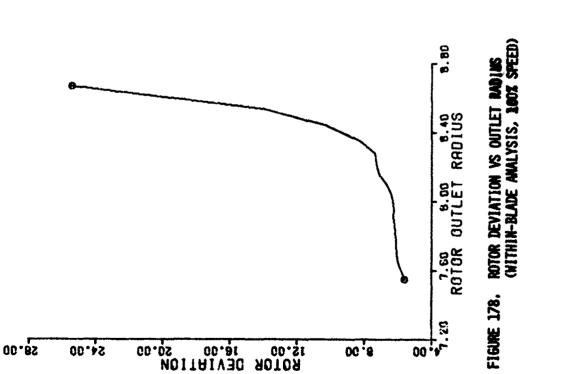
ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 100% SPEED)

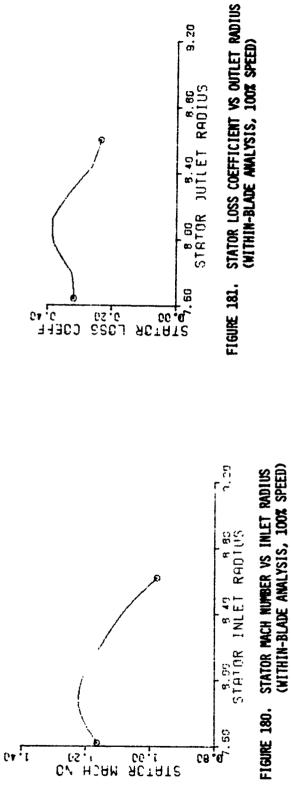
F16URE 177.

ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 100% SPEED)

F160RE 174.







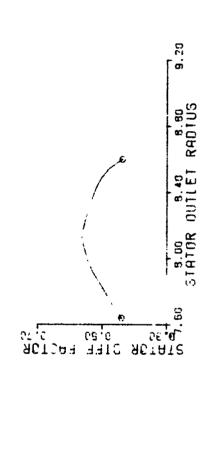


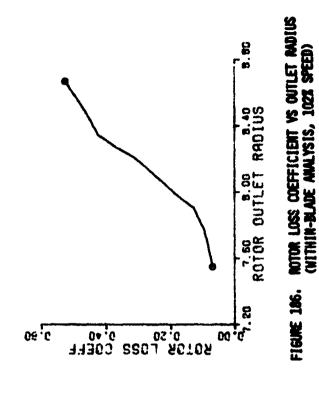
FIGURE 182. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 100% SPEED)

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ROTOR DIFF FACTOR 0,50

ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 102% SPEED) FIGURE 185.

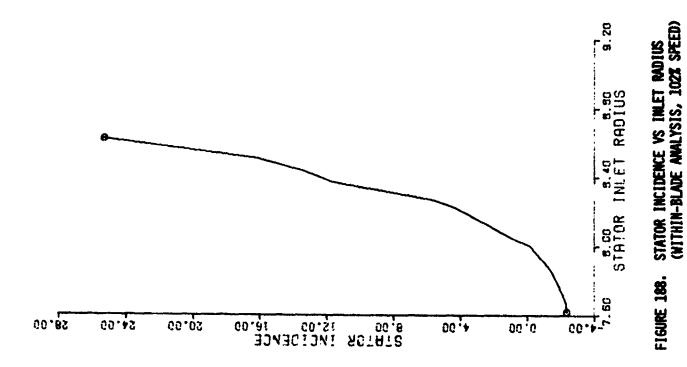
ROTOR OUTLET RADIUS

00.0°

FIGURE 183.

01 1

NOTOR RELATIVE PACH NUMBER VS INLET PADIUS (WITHIR-BLADE ANALYSIS, 102% SPEED)



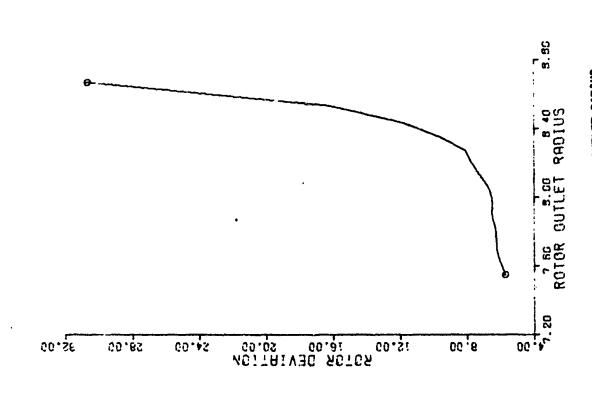
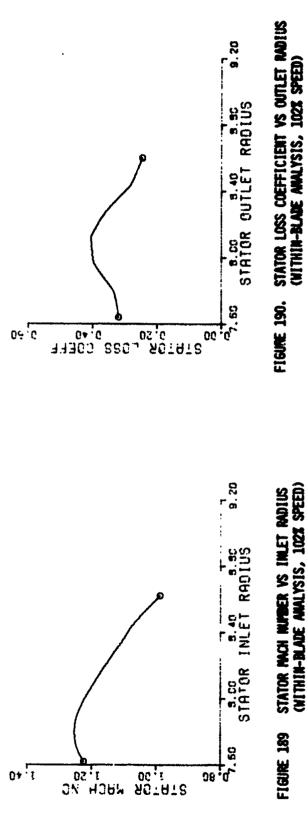


FIGURE 187. ROTOR DEVIATION VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 102% SPEED)



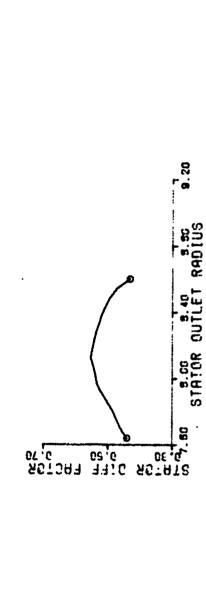


FIGURE 191. STATOR DIFFUSION FACTOR VS OUTLET PADIUS (WITHIN-BLADE ANALYSIS, 102% SPEED)

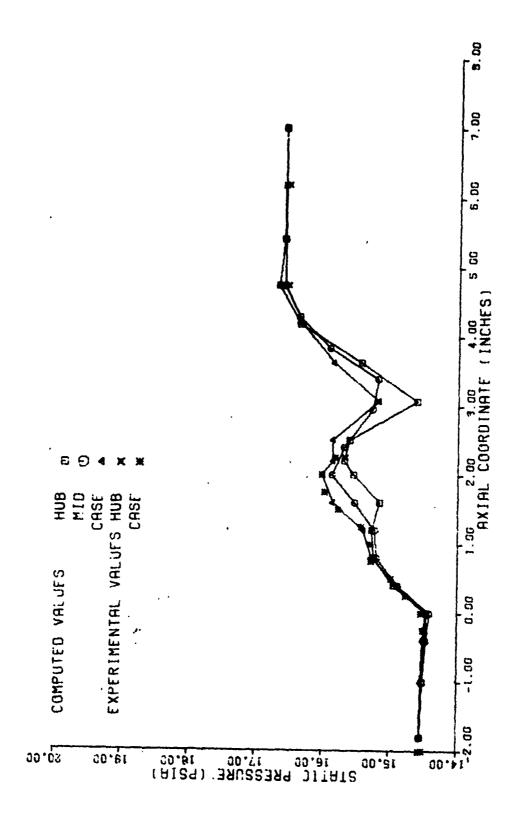


FIGURE 192, AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 40% SPEED)

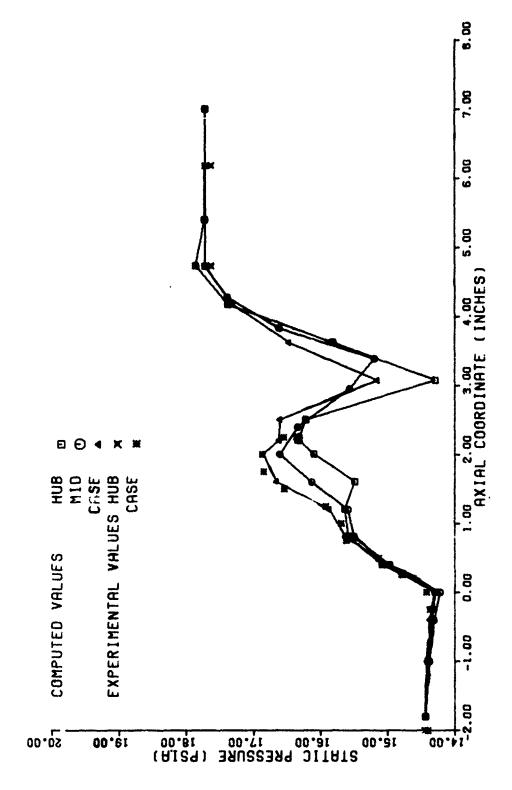


FIGURE 193, AXIAL STATIC PRESSURE DISTRIBUTION (MITHIN-BLADE ANALYSIS, 50% SPEED)

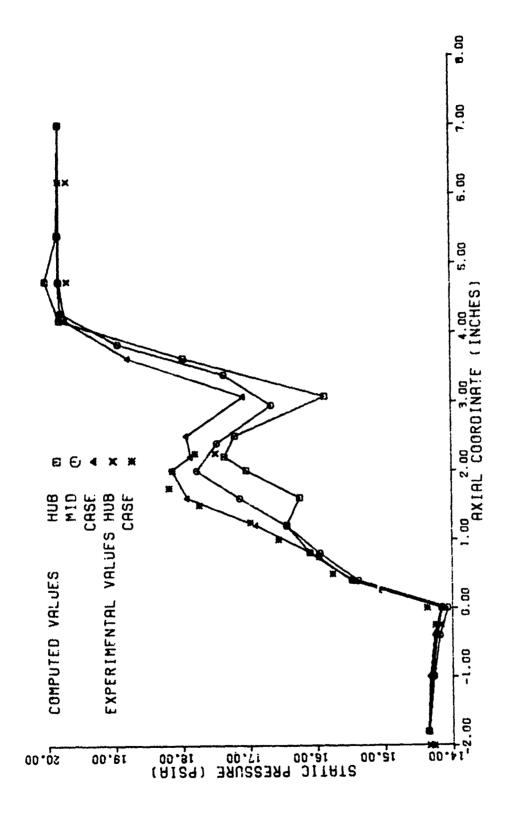


FIGURE 194, AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 60% SPEED)

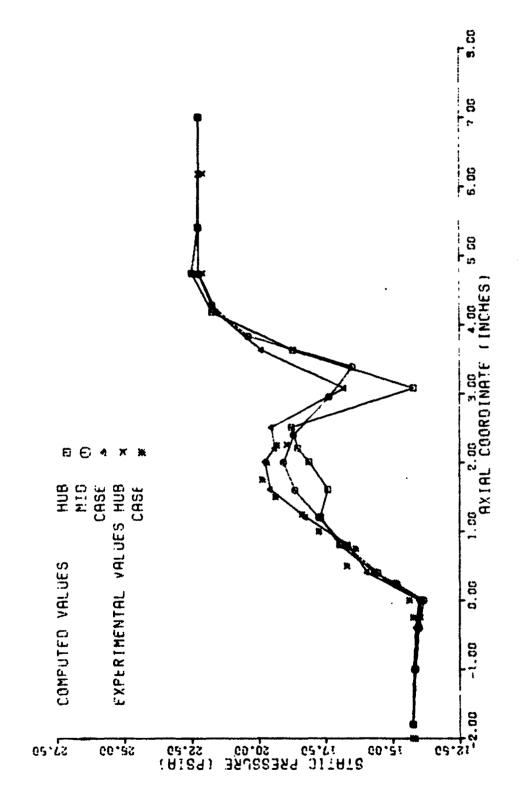


FIGURE 195. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE AMALYSIS, 70% SPEED)

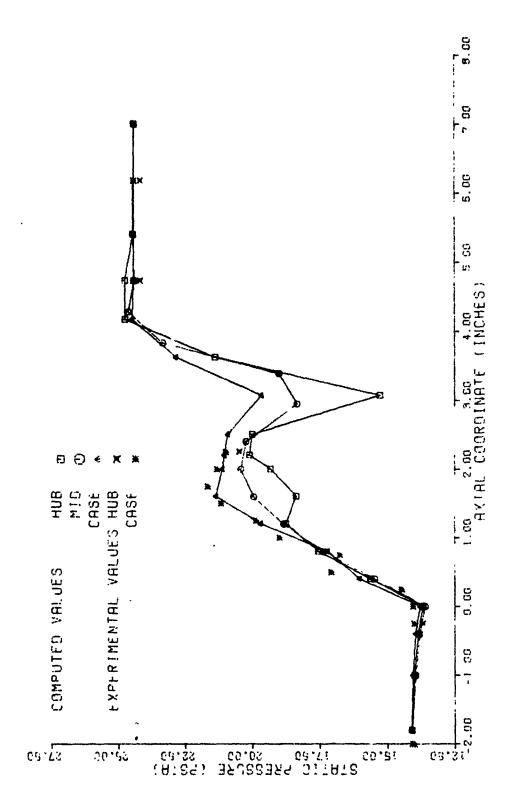


FIGURE 196. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 80% SPEED)

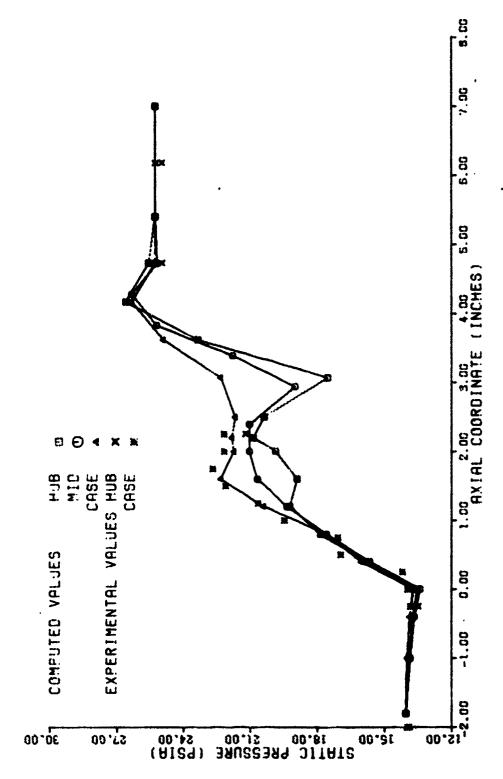


FIGURE 197. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE AMALYSIS, 85% SPEED)

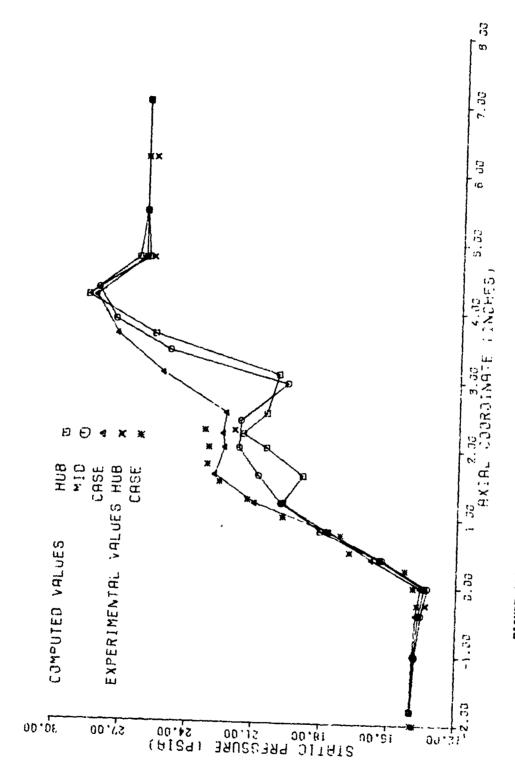


FIGURE 198. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 90% SPEED)

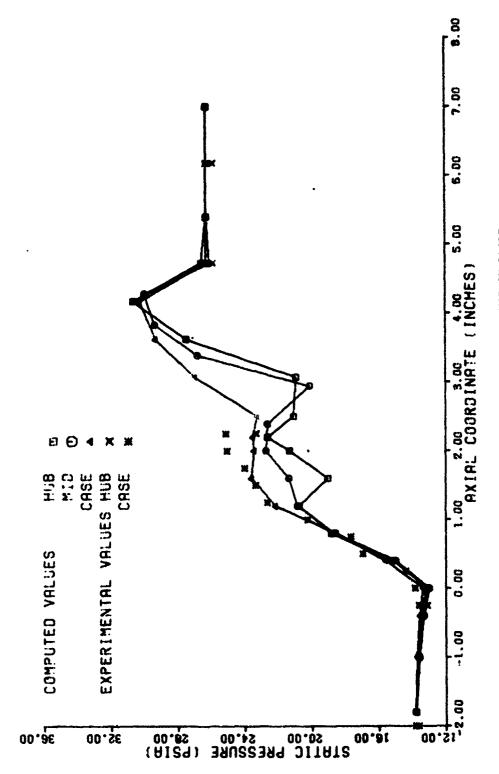


FIGURE 199. AXIAL STATIC PRESSURE DISTRIBUTION (NITHIN-BLADE AMALYSIS, 95% SPEED)

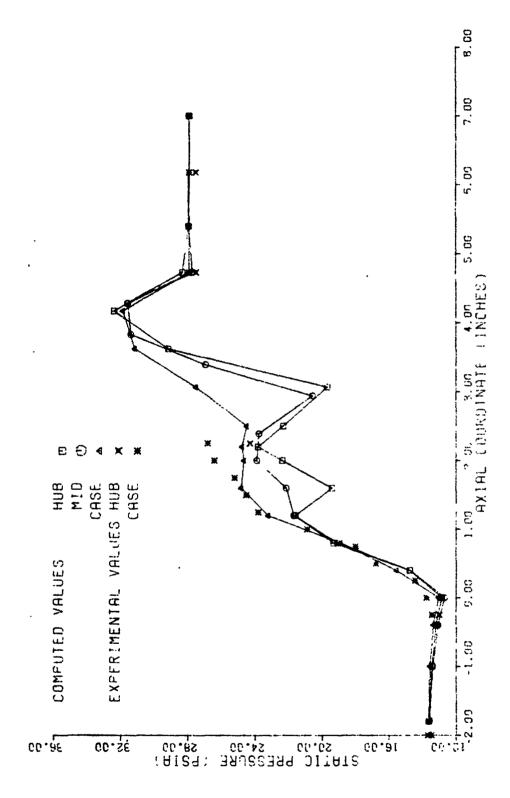


FIGURE 200. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 100% SPEED)

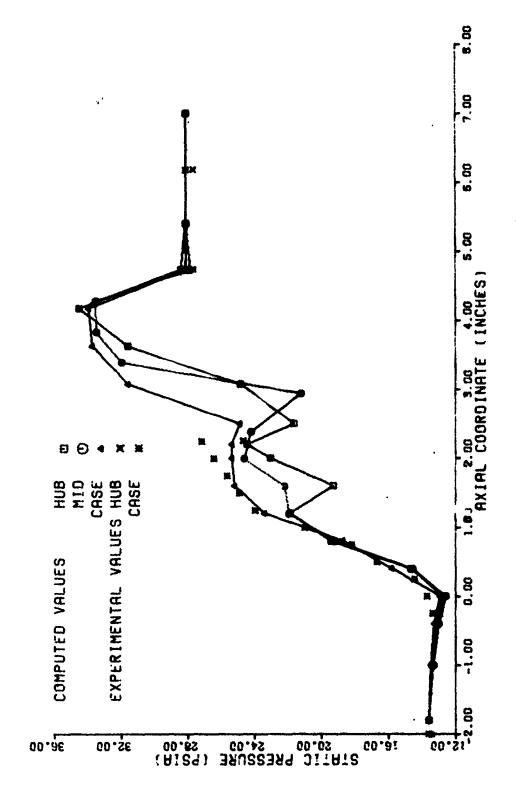


FIGURE 201. AXIAL STATIC PRESSURE DISTRIBUTION (WITHINGRADE ANALYSIS, 1028 SPEED)

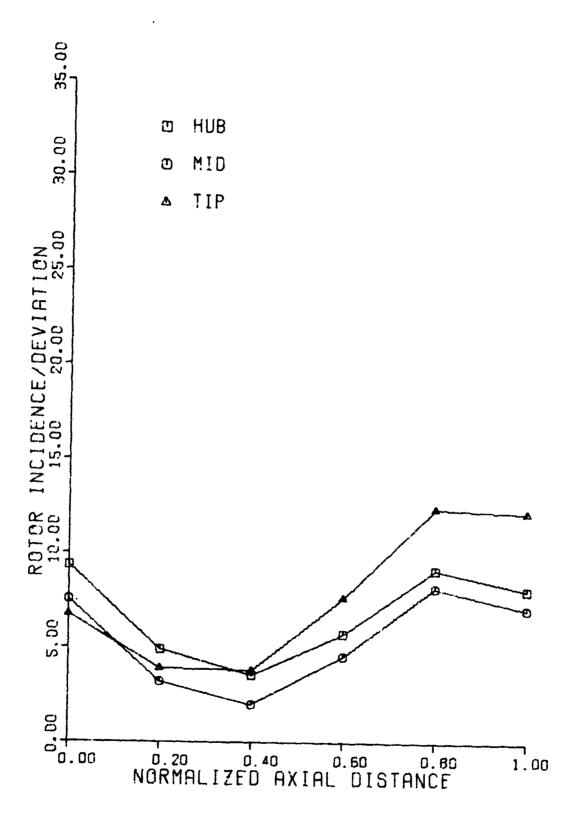


FIGURE 202. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (40% SPEED POINT)

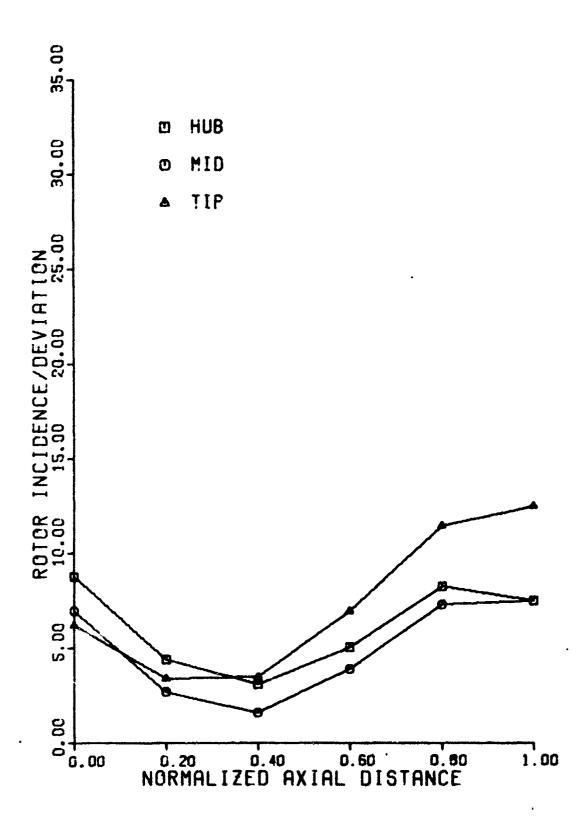


FIGURE 203. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (50% SPEED POINT)

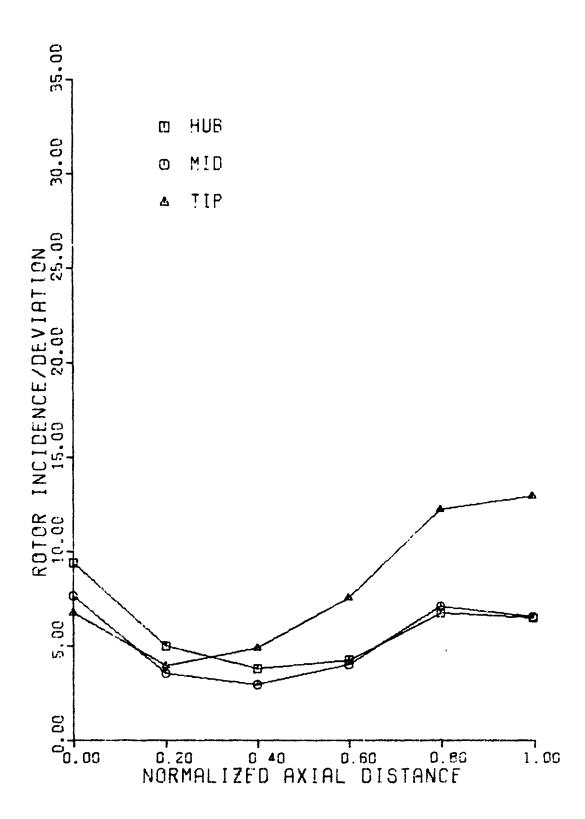


FIGURE 204. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (60% SPEED POINT)

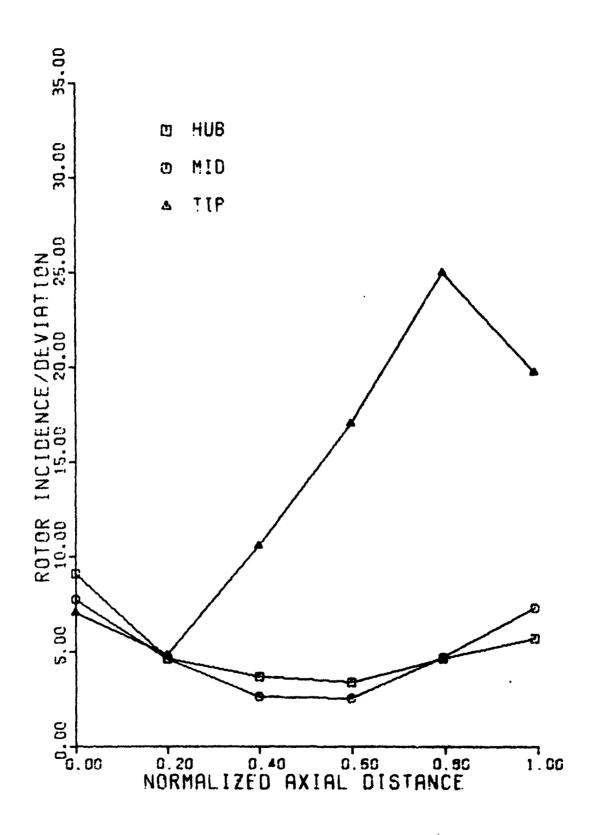


FIGURE 205. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (70% SPEED POINT)

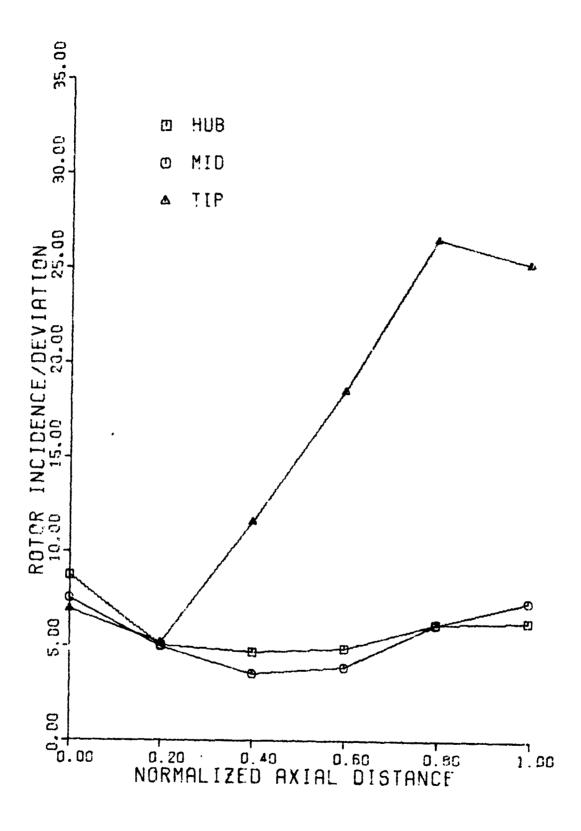


FIGURE 206. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (80% SPEED POINT)

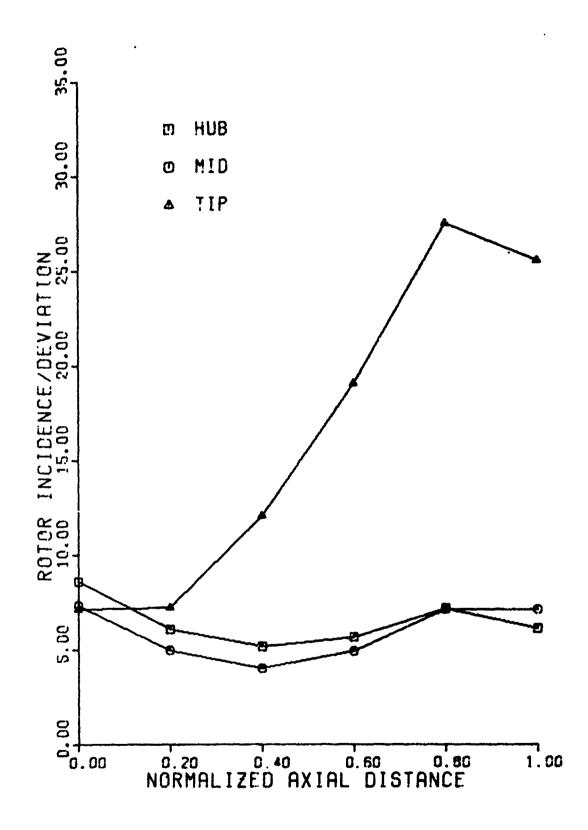


FIGURE 207. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (85% SPEED POINT)

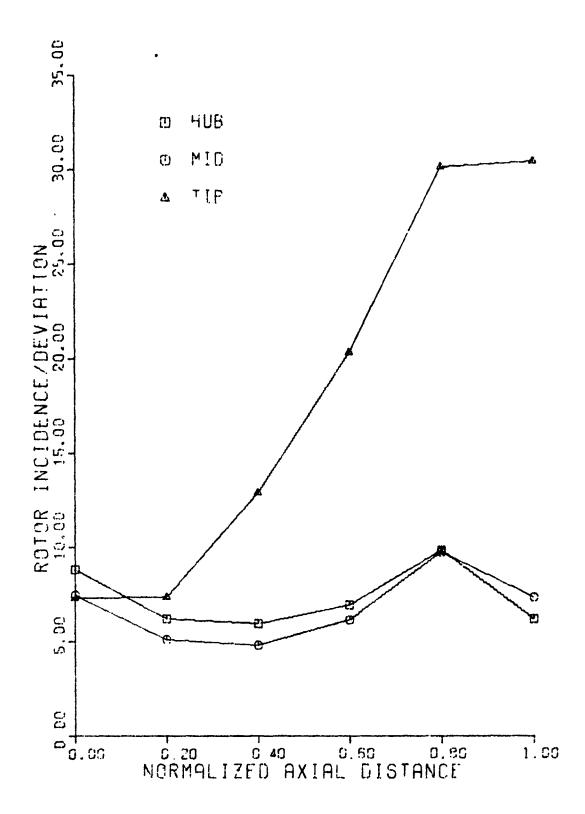


FIGURE 208. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION 90% SPEED POINT)

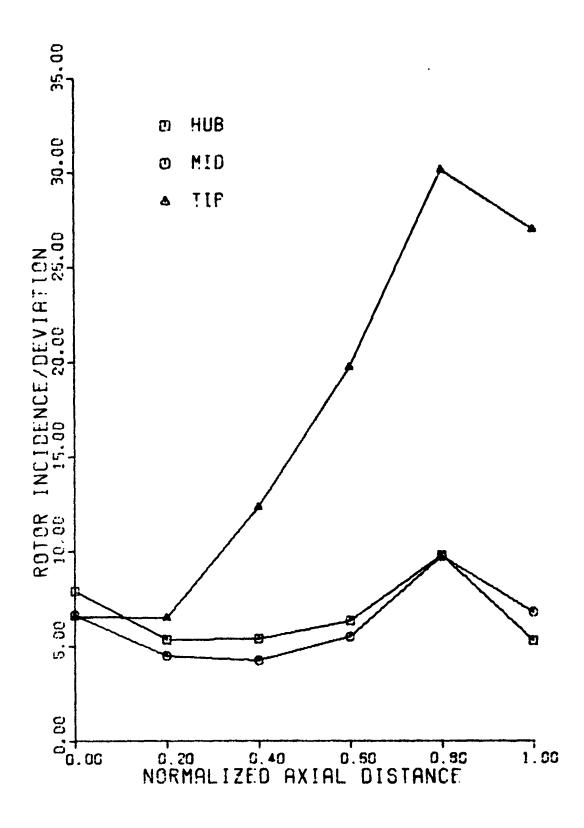


FIGURE 209. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (95% SPEED POINT)

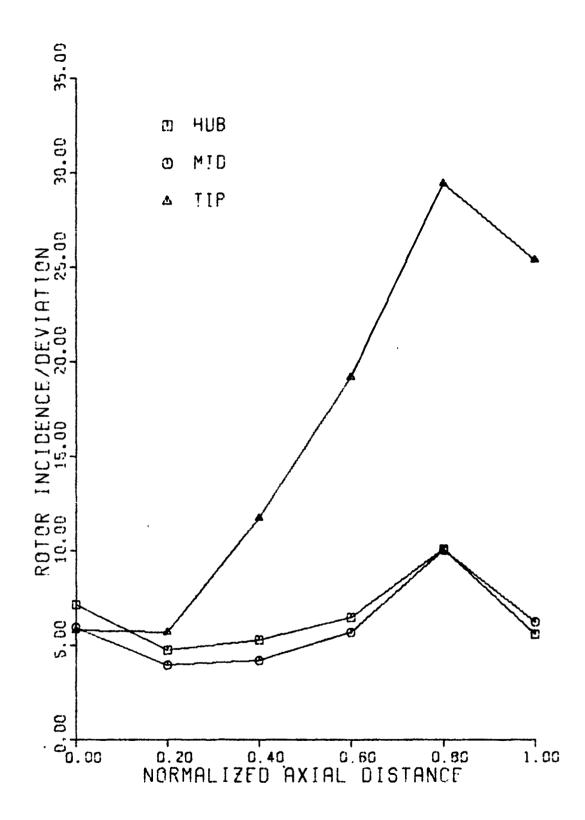


FIGURE 210. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (100% SPEED POINT)

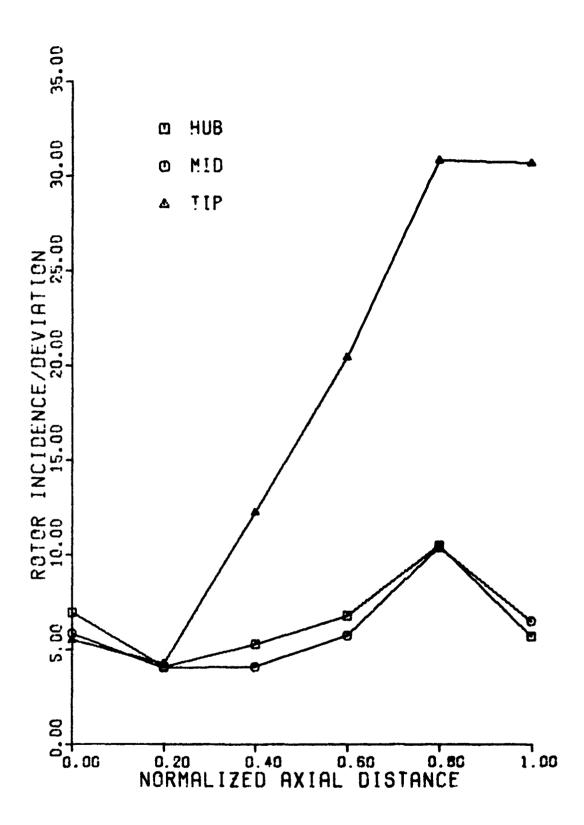


FIGURE 211. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (102% SPEED POINT)

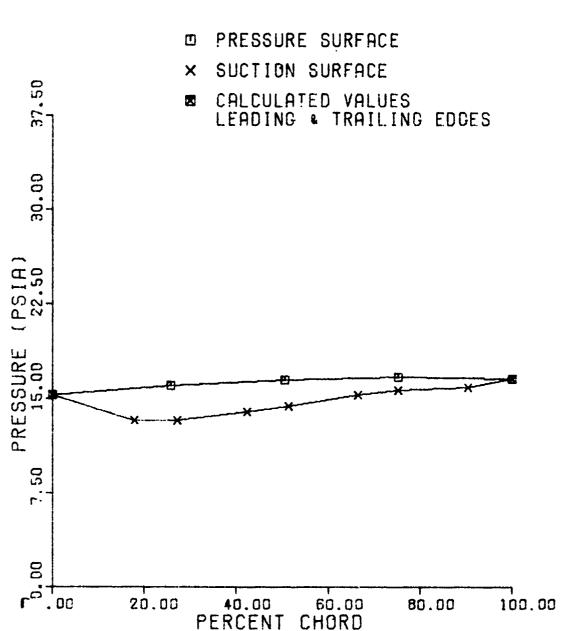


FIGURE 212. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 40% SPEED)



× SUCTION SURFACE

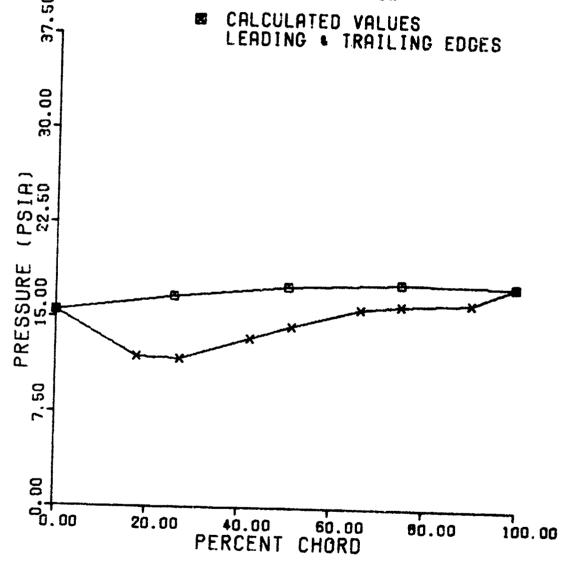


FIGURE 213. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 50% SPEED)

- PRESSURE SURFACE
- SUCTION SURFACE
- CALCULATED VALUES
 LEADING * TRAILING EDGES

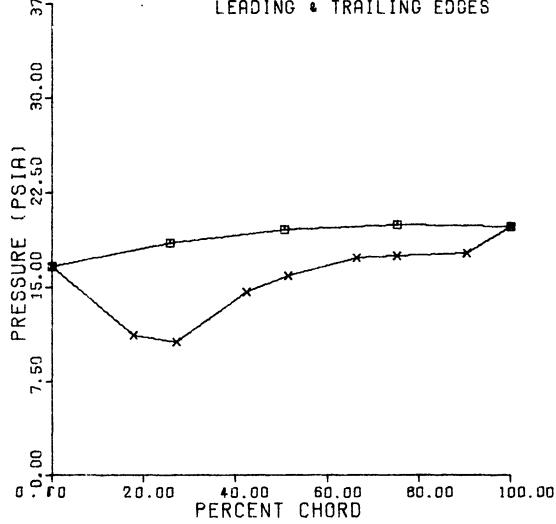


FIGURE 214. STATCR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 60% SPEED)

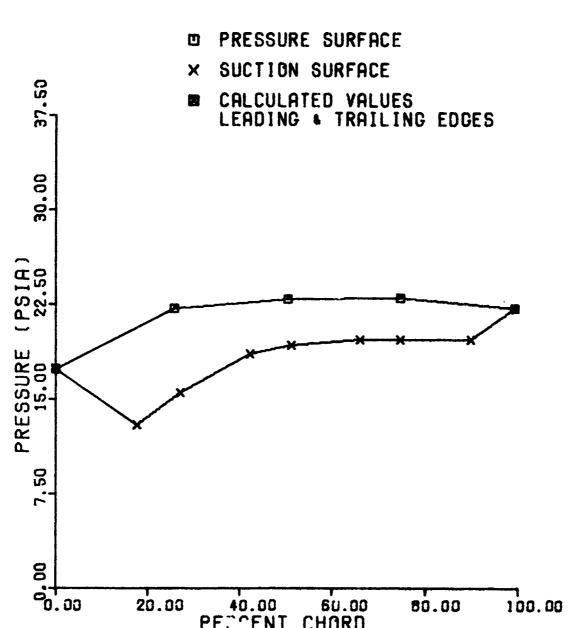


FIGURE 215. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 70% SPEED)

PETCENT CHORD

- D PRESSURE SURFACE
- × SUCTION SURFACE
- M CALCULATED VALUES

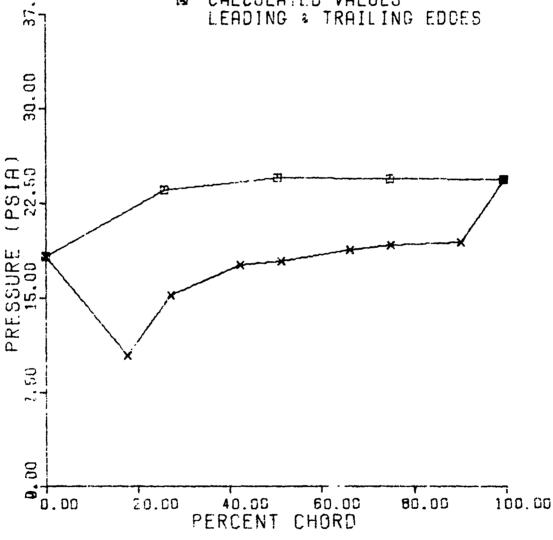


FIGURE 216. STATOR MID-SPAN SUFFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 80% SPEED)

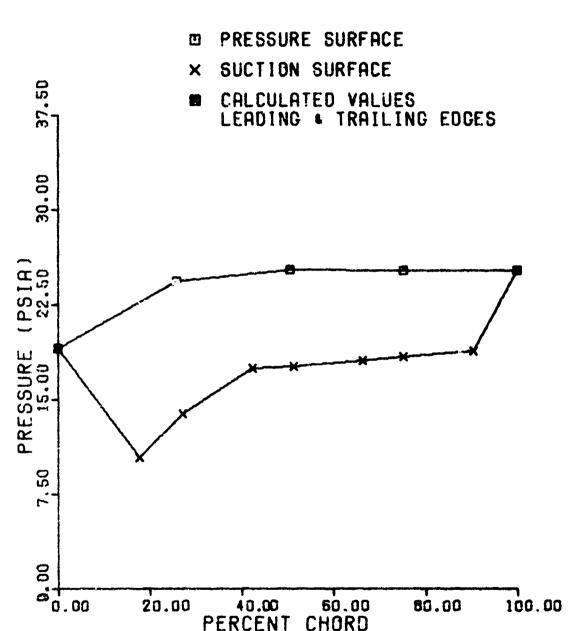


FIGURE 217. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-SLADE ANALYSIS, 85% SPEED)

- PRESSURE SURFACE
- × SUCTION SURFACE
- CALCULATED VALUES
 LEADING & TRAILING EDGES

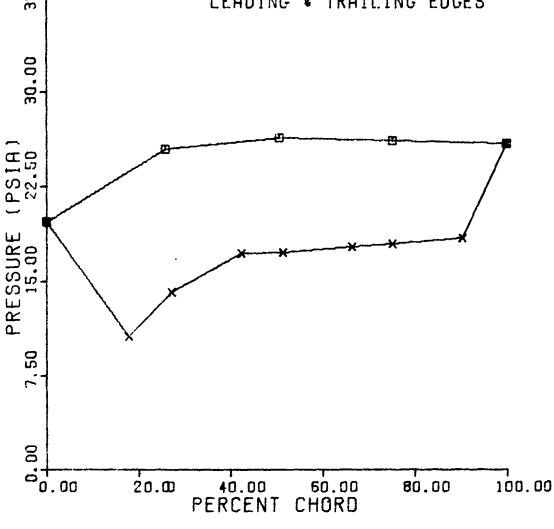


FIGURE 218. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 90% SPEED)

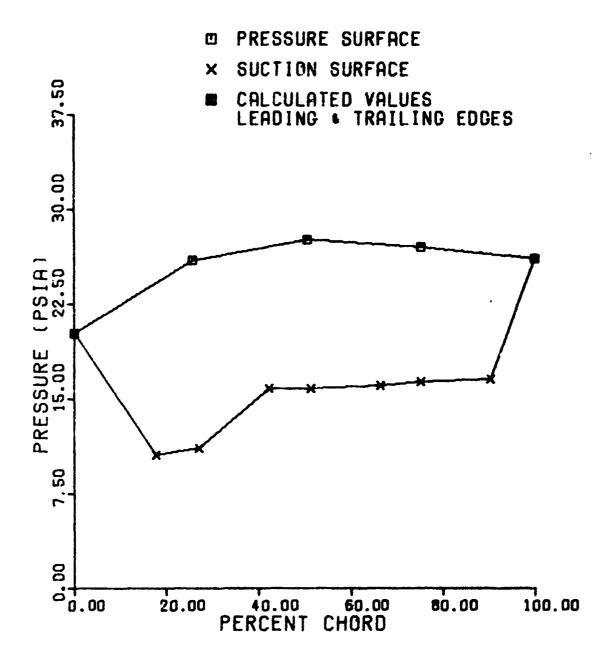


FIGURE 219. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 95% SPEED)

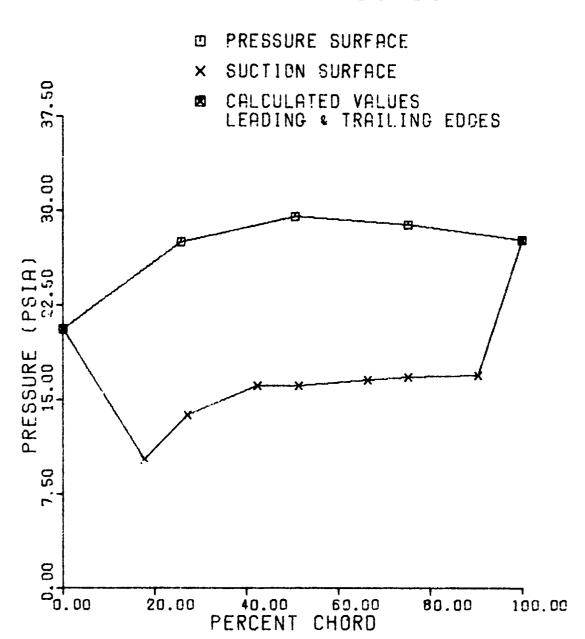


FIGURE 220. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 100% SPEED)

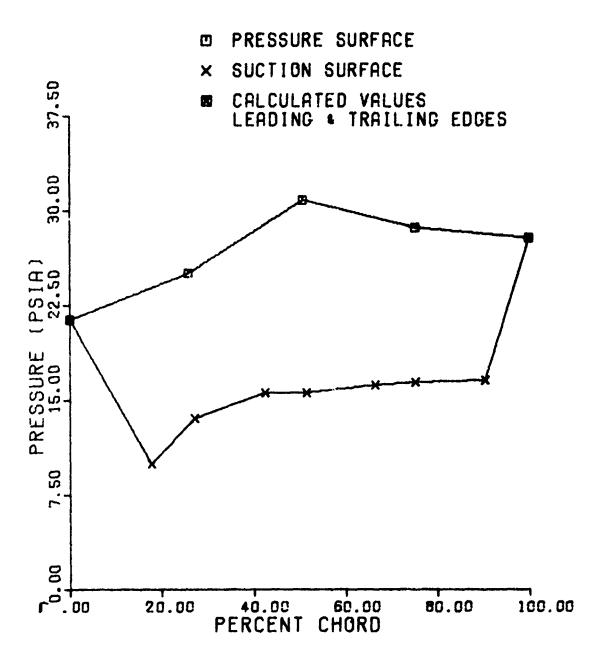


FIGURE 221. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 102% SPEED)

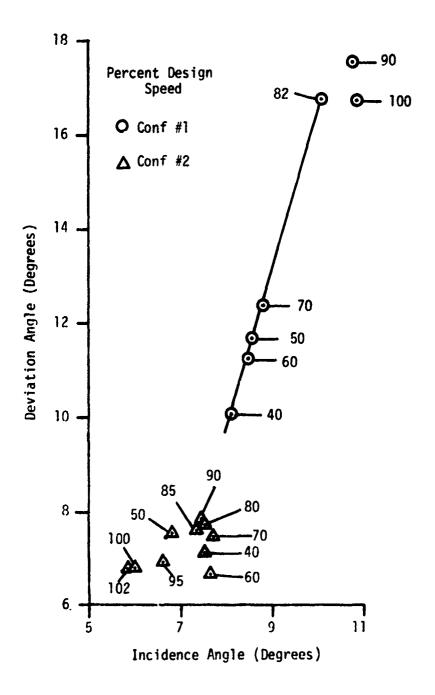


FIGURE 222. ROTOR MID-RADIUS DEVIATION VS INCIDENCE ANGLE

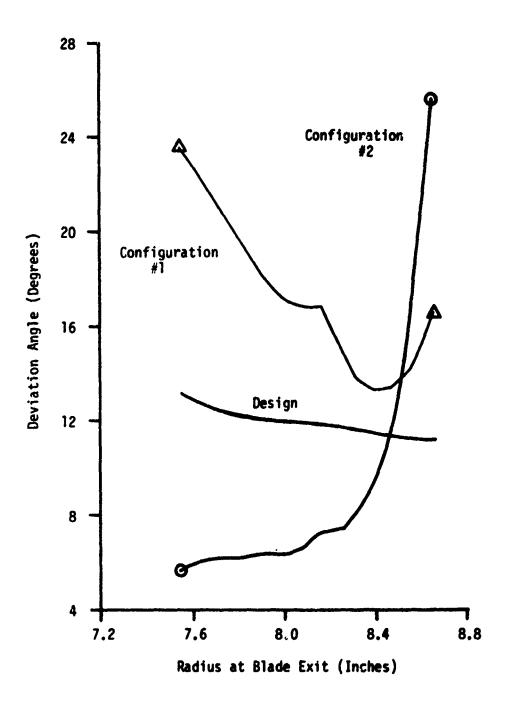
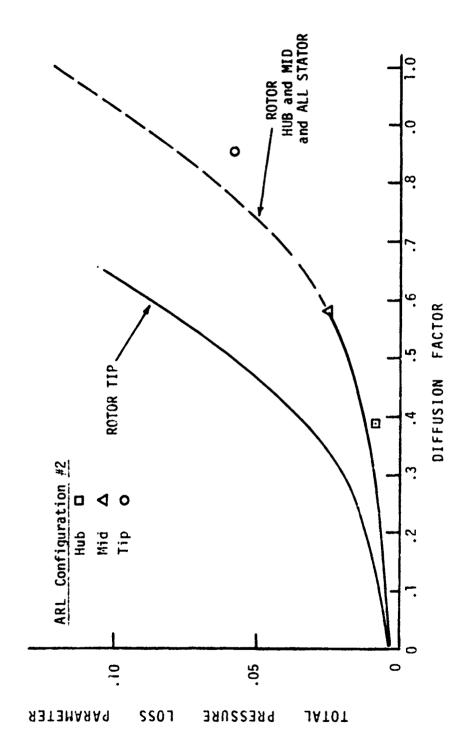


FIGURE 223. ROTOR DEVIATION ANGLE DISTRIBUTION



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FIGURE 224. NACA COMPRESSOR LOSS CORRELATION WITH ARL CONFIGURATION #2 SUPERIMPOSED

APPENDIX A

PHASE II WITHIN-BLADE ANALYSES (COMPUTER PRINTOUTS)

This appendix presents the aerodynamic results (in the form of computer printouts) of the Phase II within-blade analyses for the ten test points selected for that analysis. The printout of input data which preceds the material presented herein has been removed in order to keep the number of pares to a minimum. The input data used in each of these analyses are precented in Appendix B.

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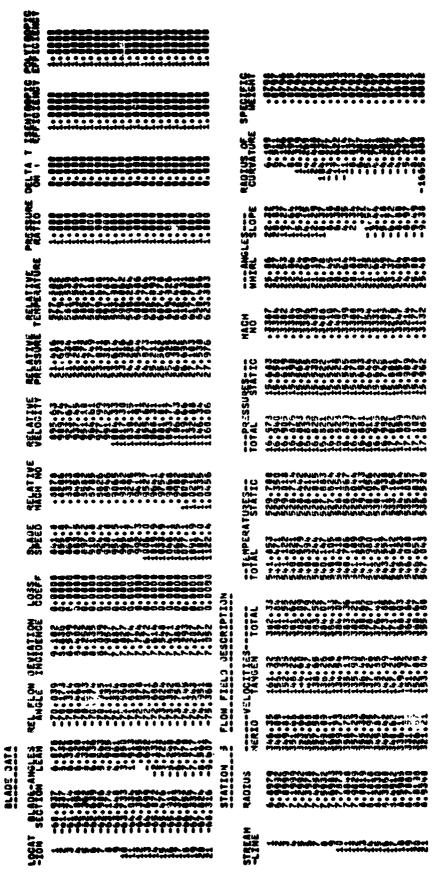
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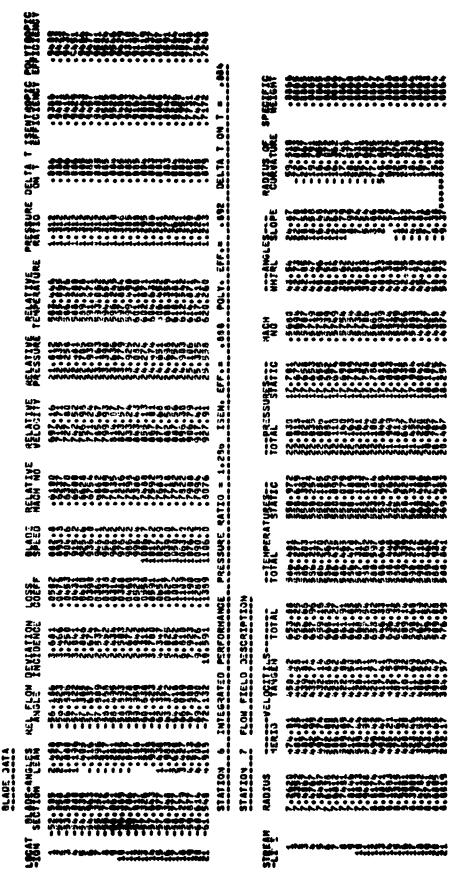
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TUREST	ฅ๛๛๔๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	RELATIV	Z IS	ത്രമ്പ് പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തിലും പുത്തില	AAT10 = 1
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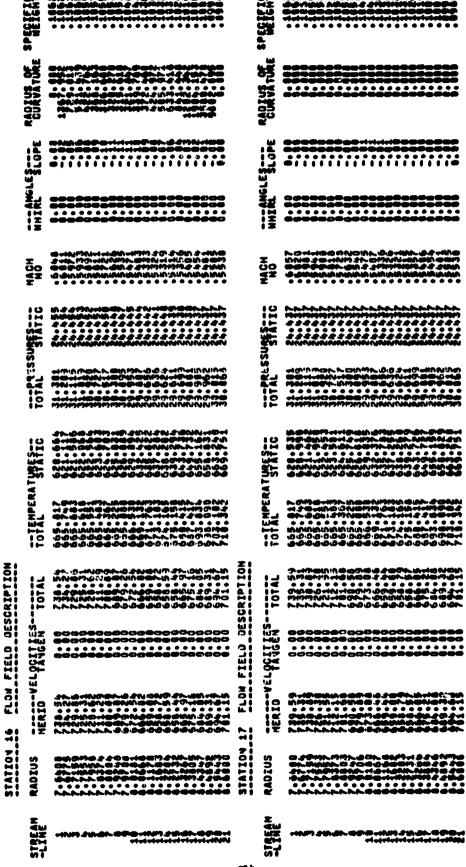
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#### APPENDIX B

### COMPUTER INPUT DATA FOR DATA REDUCTION

### KEY

- SECTION 1. Common Phase I Data
- SECTION 2. Common Phase II Fixed Data (Log 1) Across Plade
- SECTION 3. Common Phase II Input and Test Point Data (Log 3, Log 4) Across Blade
- SECTION 4. Common Phase II Fixed Data (Log 1) Within Blade
- SECTION 5. Common Phase II Input and Test Point Data (Log 3, Log 4) Within Blade
- SECTION 6. Individual Test Input Data
  - a. Exceptions to Section 1 Data (indicated by (1))
  - b. Exceptions to Section 2 Data (indicated by (2) )
  - c. Exceptions to Section 3 Data
     (indicated by (3))
  - d. Exceptions to Section 4, Data (indicated by (4))
  - e. Exceptions to Section 5 Data (indicated by (5))

MASIC.DATA	DECK						
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EDITING DATA DECK

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# SECTION 2. COMMON PHASE II FIXED DATA (LOG 1) ACROSS BLADE

	C CATA PRINTOUT
	OVERALL RUN TITLE
A Branchister was over -	NUMBIR OF STATIONS = 10  NUMBIR OF STPIAGLINES = 21  MAXIMUM NUMBER OF ARBITRARY ITERATIONS = 16  TUTAL PRISSURL SOURCE INCICATOR = 0  TUTAL THERRATURE SOURCE INCICATOR = 0  STATION NUMBER FOR ROTOR EXIT CATA = 7  STATION NUMBER FOR ROTOR EXIT CATA = 7  STATION NUMBER FOR ROTOR EXIT CATA = 7  STATION NUMBER FOR ROTOR EXIT CATA = 60  NUMBIR OF ROTOR BLACES = 49  MAXIMUM NUMBER OF LINES FOR PAGE = 80  NELOS = 3
	MAXIMUM NUMBER OF AFTERATIONS = 46 MAXIMUM NUMBER OF AFTERATIONS = 16 TUTAL PRESSURE SOURCE INCIDENTER = 6
	TUTAL PRESSURE SOURCE INCICATOR = C TOTAL TIMERATURE SOURCE INCICATOR = D STATION NUMBER FOR ROTCH EXIT CATA = 7
	STATION NUMBER FOR ROTOR EXIT CATA = 7 STATION NUMBER FOR STAGE EXIT CATA = 6
	NUMBER OF ROTOR BLADES = 30 NUMBER OF STATOR SLADES = 49
	MAXIMU: NUMBER OF EINES FER PAGE = 3
	ANNULUS SPECIFICATION
	STATION 1 SPECIFIED BY Z. F.CINIS
	RSTN XSTN
	6.0c36 -1.d000 9.0900 -1.30
A	STATION 2 SPECIFIED BY 2 FCINTS
*	RSTA XSTN
	9,0900 -1,0000
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- 164	RSIN XSTN
	7.5193 2.5009 7.7.62 2.6593 7.8/30 2.6592
	7.7.72 2.6593 7.8730 2.6402 5.6949 2.9252
	8.1427 2.9431
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	7.5400	7.0090					
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	STATION CALC	ULATION SPE	CIFICATION A	ND BLACING	CATA		
	STATION 2	NCALC = 0	NDATA = -0	Naf ==0	······································	·	
	STATIUN 3	NCALC = 0		NUE ==0			
2)	STATION 4	NCALC = 1	NCATA = 15	NEL = 0			
	RADIUS	e Para	EPSILCA	BLCCKAGE	THETA		
	5.7,8c 6.9)66	o ~v2•2938	6.0825 6.2938	.01450 .01420	.2192 .2168		
	7.050	-02.3379	<del>-                                </del>	.01410 .01390	<del></del>		· · · · · · · · · · · · · · · · · · ·
	7.3c60 7.5216 7.577	-03.3790	6.2846 5.7616 4.6992	.01390 .01370 .01350	2120 2097		
	7.5776	-c3.7062	3.6317 2.6463	.01330 	2062	_	
	7.9327	-64.5112	-1.785d	.01320	. 2048		
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	8.4791	L -66.1881 2 -66.3700	-5.[474 -7.1213	.01360 .01360	.2078 .2101		
	8.8166 3.930	2 -66.4700 -67.5768 -58.2887	-8.1121 -9.5200	.01420	.2127 .2157		
2)	STATIUA 5	NCALC = 4	NDATA = 15	NBL = 0	····		<del></del>
•	RADIUS	DETA-	EPSILCK	ELCCKAGE	THETA	<del> </del>	
	7.558	-11.0761 -12.5921	10.9221 10.3557 9.3776	194425	1061		
	7.6639	9 -14.1312	9.3776	.04309 .04185	1091		
	7.750t	-17.1350	7.1593	•04100 •04024	1116		
	7.612	5 -18.3596	7.1593 6.6712 6.6211	03556	1127 1138		
	3.0442	2 -28.2566	7.6047	.03806	1151		
	8 <u>123</u>	-21.0485 -21.7990	10.6021	.03752 .03690	1165 1162 1202	<del></del> -	
	5.2047 5.255 5.373	2 -22.4622	12.2000	▲03635	1202		
	8.462	5 -23.4032	13.4357 13.6543 13.7640	.03584 .03545 .03496	- 1252 - 1279		
	8.5549	9 -23.4990	13.7640	.03496 .03437	1279 1387		
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(2)	PLMIAUN D	NCALC = 0			····		
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(2)	STATION 7	NCALC = 1	NDATA = 10	NBL = 0		
	RAUIUS	BETA	EPSILCA	ELUCKAGE	THETA	
		55.1561 53.5860	-37.7735	11614	- 1083	
	7.6595 7.7778	49.8388	-30.1445	.01723 .01536	4952 8847 	
	8.0211		-11.6297 -11.6297	.01392 .01358	0727 0710	
	8.1.54 8.2714	44.6432	9.6089 26.7782	.01338	0722 0770	
	8.3997 8.5330		44.5535	.01333 	<u>8482</u>	
	8.6721	54.4829	48.7546	.01130	1947	
	STATION B					
·····	RADIUS		EPSILCA	ELCCKAGE	THETA	
	7.5000 7.6250 7.7500	-6.7608 -7.1856	•0181 •6202	.00594 .00579	.0001 .0001	
	7.7500 7.8750	-7.6668 -8.1755	.0180 .0121	.00964	.0001	
		-8.5985	.03C	• <b>00936</b> • <b>00923</b>	0.0000	
	8.1250 3.2500 8.3750	-9.0563 -9.0563	002± 0113	• 00919 • 00896	0.0000	
	8.5000 6.5000	-1.1339	•• (255 •• 041£	.00884	.0001	
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	STATION 10	NCALC = 0	ADATA =	) NBL = 1		
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## SECTION 3. COMMON PHASE II INPUT AND TEST POINT DATA (LOG 3, LOG 4) WITHIN BLADE

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	FLOHRAT CTUZ SPEE	) 			= 25.6325 = 20410.0 = 14.6960	
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	8.2513 8.2513 8.3710	43.7000 47.133d				
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(3) STATION.	BLOCKAGE DIS	THIBUTION FACTOR	MID AEG-CENA.	CISTRIBUTION FACTOR	FRACTICH TE PLOCKAGE
1	0.00000	1.CODC	-0.000	-0.0000	-0.0000
3	0.00000	1.000 1.000	-0.006 -0.000 -C.006	-0.0000 -0.0000	-0.0000
<u> </u>	05000	0.000	-0.000	-0.0000 -0.0000	0.0000 0.000 0.000 0.000
	.26000	0.000C 1.000G 1.00G	-0.000	-0.0000 -0.0000	-0.0000 -0.0000 -0.0000
Š	05400 	1.6086	200.00	-0.0000	-0.0000
SOLUTION	TYPE INDICATO		-0000		
(3) STATION		6 7 8 9 10 -C -0 -0 -0 -0	elitar essenti e Tiranomento alla essenti		
(3) NEACH	0-0-0-0	<u>-c-o-o-o-o</u>			
NJUMP= 0					

### SECTION 4. COMMON PHASE II FIXED DATA (LOG 1) WITHIN BLADE

### FIXED DATA PRINTOUT

7.4492

OVERALL RUN TITLE NUMBER OF STATIONS
NUMBER OF STREAMLINES
MAKINUM NUMBER OF ITERATIONS
MAKINUM NUMBER OF ARITRARY ITERATIONS
TOTAL PRESSURE SOURCE INDICATOR
TOTAL TEMPERATURE SOURCE INDICATOR
STATION NUMBER FOR ROTAL EXIT DATA
STATION NUMBER OF LINES
MAKINUM NUMBER OF LINES PER PAGE
NALUM NUMBER OF LINES PER PAGE ANNULUS SPECIFICATION STATION 1 SPECIFIED BY 2 POINTS RSTIL X3TN -1.3033 STATION 2 SPECIFICO BY 2 POINTS RSTN XSTN 9.3746 -1.0000 STATION 3 SPECIFIED BY 2 POINTS ₹3TN XSTN --4000 STATION + SPECIFIED BY 2 POINTS RSTN NTEX 6.7300 9.0000 STATION 5 SPECIFIED BY 2 POINTS RST I XSTI 6+3379 8+33+0 .4338 .4000 STATION & SPLCIFIED BY 2 POINTS PSTN XST4 7.3784 .5000 STATION 7 SPICIFIED BY 2 POINTS RST 4 XST4 1.2000 7.2020 8.1019 STATION & SPECIFIED BY 2 POINTS RSTN XSTN

1.6030

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STATION 3 SPECIFIED BY 2 POINTS
            RSTN
                                                                                                     XSTN
           7.5499
STATION 10 SPECIFIED BY 6 POINTS
             RSTN
                                                                                                     XSTN
            7.57.600
7.8000
6.0000
6.2000
6.4000
8.6339
STATION 11 SPECIFIED BY 8 POINTS
             RSTN
                                                                                                     XSTN
            7.3139
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  STATION 12 SPECIFIED DY 8 POINTS
              RSTN
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8.1746
8.2934
8.4257
8.5730
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3.21119
3.37119
3.37560
3.35560
3.0578
 STATION 13 SPECIFIED BY 8 POINTS
              RSTN
                                                                                                        XSTN
             7.7230
7.3436
7.3336
8.0636
8.1835
8.3126
8.3735
                                                                                                       3.6189
3.7126
3.75256
3.8370
3.8123
3.7433
3.7433
  STATION 14 SPECIFIED BY 3 POINTS
               RSTY
                                                                                                        XSTN
              7.6720
8.1900
8.5900
  STATION 15 SPECIFIED BY 2 POINTS
                RSTN
                                                                                                        XSTN
                                                                                                        4.7250
   STATION 16 SPECIFIED BY 2 POINTS
                 RSTN
                                                                                                          KSTN
                                                                                                         5.4000
5.4000
                7.5400
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### XSTN 7.0900 7.5400 STATION CALCULATION SPECIFICATION AND BLADING DATA NCALC = 0 NDATA = -0 STATION 3 NCALC = 0 NDATA = -0 STATION 4 NCALC = 1 NDATA = 15 NBL = 0 RADIUS BETA EPSILON BLOCKAGE THETA 6.756664 796631 796631 77.3567 77.577 77.643 77.6660 8.477 8.660 8.99 -62.583399 -62.583399 -652.583399 -653.08162 -633.708162 -64.51333 -64.51333 -64.516880 -65.5880 -65.5880 -65.5880 -65.5880 -65.5880 -65.5880 -65.5880 6.083556 6.241846 6.241846 6.241846 6.24184 6.39173 2.241848 7.64743 7.64743 7.64743 7.64743 7.64743 7.64743 7.64743 7.64743 7.64743 7.64743 7.64743 7.64743 • 61450 • 614499 • 613375 • 613375 • 6133223 • 6133223 • 613333 • 61333 • 61333 • 61333 • 6145 • 6145 • 6145 • 6145 (4) STATION 5 NCALC = 2 NDATA = 15 NBL = 3 RADIUS BETA EPSILON BLOCKAGE THETA -60.4847 -60.813467 -60.813467 -61.43133 -61.63133 -61.643133 -62.83362287 -62.83362287 -62.83362287 -65.83362 4.1878 4.1773 3.1246 43.1773 3.1246 43.1773 3.1246 43.1723 43.1724 43.1724 43.1724 43.1724 43.1724 43.1724 43.1724 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•09912345 •09912345 6.9066 7.0443 7.1829 7.3217 1065648226682342 1100432266823342 110043226882342 7.3217 7.4509 7.4509 7.5739 9.2110 8.3364 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 8.467 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STATION 17 SPECIFIED 3Y 2 POINTS

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                                                       STATION 3
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• 106007
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3.4175
5.5971
3.0110
4.7225
(4)
                                             STATION 3
                                                                                                                                                                                WCALS = 4
                                                                                                                                                                                                                                                                                               NDATA = 15
                                                                                                                                                                                                                                                                                                                                                                                                              N3L = 3
                                                                                                             SUIUA
                                                                                                                                                                                                                         BETA
                                                                                                                                                                                                                                                                                                          IPSILON
                                                                                                                                                                                                                                                                                                                                                                                                               BLOCKAGE
                                                                                                   THETA
                                                                                                                                                                                                                                                                                                10.95773
9.35773
9.35773
7.1193
6.652117
6.652117
6.65217
113.495
112.495
113.495
                                                                                                                                                                                                                                                                                                                                                                                                                3.0750
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          -.1307
                                        STATION 13
                                                                                                                                                                          NCA_0 = 0
                                                                                                                                                                                                                                                                                          VDATA = -0
                                                                                                                                                                                                                                                                                                                                                                                                                  N3L = 1
                                        STATION 11
                                                                                                                                                                        NOALS = 1
                                                                                                                                                                                                                                                                                       JOATA = 10
                                                                                                                                                                                                                                                                                                                                                                                                                N-3L =-0
                                                                                                     EUIGAS
                                                                                                                                                                                                                  BETA
                                                                                                                                                                                                                                                                                                  EPSILON
                                                                                                                                                                                                                                                                                                                                                                                                       BLOCKAGE
                                                                                             7.59+95
7.6775
7.6775
7.8121
3.1274
3.1274
3.27197
8.57197
8.57197
8.57197
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             THETA
                                                                                                                                                                                       -43.75335
-37.14357
-37.14357
-21.2239
-11.3239
-11.3239
-26.77535
-41.5554
-48.7554
                                                                                                                                                                                                                                                                                                                                                                                                          J1514

• J1736

• J1736

• J1398

• J1338

• J1338

• J1338

• J1338
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-.0352
-.0847
-.0773
-.0727
-.0727
-.0720
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  -- 00532
                                                                                                                                                                                           34. + 323
                                                                                                                                                                                                                                                                                                                                                                                                               . 01130
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STATION 12 NCALC = 2 NDATA = 10 NBL = 0
                                                            RADIUS
                                                                                                                                              BETA
                                                                                                                                                                                                       EPSILON
                                                                                                                                                                                                                                                                                 BLOCKAGE
                                                                                                                                                                                                                                                                                                                                                                         THETA
                                                          7.513340
7.675956
8.02576
8.02576
8.02576
8.12576
8.35033
8.35033
                                                                                                                           -25.7556
-26.3943
-23.2637
-16.2152
-3.4757
-3.3793
12.2254
23.1232
                                                                                                                                                                                                                                                                                      •118511
•185112
•08062
•06962
•073992
•073992
•07278
                                                                                                                                                                                                                                                                                                                                                                -.0549
-.054947
-.053931
-.05395
-.06285
-.03532
              STATION 13 NGALC = 2 NDATA = 10 N3L = 0
                                                           RADIUS
                                                                                                                                            BETA
                                                                                                                                                                                                     EPSILON
                                                                                                                                                                                                                                                                                BLOCKAGE
                                                                                                                                                                                                                                                                                                                                                                       THETA
                                                        7.5009
7.6256
7.7504
7.8752
                                                                                                                        16.39643
16.39643
15.39643
15.3963
15.3963
15.3963
16.3963
16.7363
16.7363
                                                                                                                                                                                           -9.9376
-10.93947
-9.0205
-3.7730
-3.7738
-1.1768
-3.9553
                                                                                                                                                                                                                                                                                     .12611
.11177
.017799
.07831
.07436
.07368
.07368
                                                                                                                                                                                                                                                                                                                                                              8.001
3.12501
3.2501
3.3751
3.5002
3.5254
                                                                                                                                                                                                   10.0593
                                                                                                                                                                                                                                                                                      .09466
           STATION 1+
                                                                                                         NCALC = 2
                                                                                                                                                                                         NOATA = 10 N3L = 0
                                                       RADIUS
                                                                                                                                         BETA
                                                                                                                                                                                                   EPSILON
                                                                                                                                                                                                                                                                             BLOCKAGE
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4.11830
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4.12837
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-1.1016
-.6527
-.4567
-.3036
-.1369
-.3385
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000334
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000330
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.06672
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05577
053270
05419
05579
                                                     5.1250
5.2501
5.3751
6.5001
5.6251
                                                                                                                                                                                                -1.0923
        STATION 15 NCALC = 3 NOATA = 10 NBL = 1
                                                     RADIUS
                                                                                                                                      3ET4
                                                                                                                                                                                                EPSILON
                                                                                                                                                                                                                                                                          BLOCKAGE
                                                                                                                                                                                                                                                                                                                                                                  THETA
                                                 7.5000
7.67500
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9.0000
8.12500
8.37500
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8.5050
                                                                                                                  6.766655
6.168655
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• 01821
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• 00326
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• 0255
• 0418
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• 00979
• 00950
• 00936
• 00923
• 00910
• 00884
• 00873
                                                                                                                                                                                                                                                                                                                                                         .0001
.0001
.0001
0.0000
0.0000
0.0000
      STATION 15 NCALC =-0 NOATA = -0
                                                                                                                                                                                                                                                                             N3L = 1
     STATION 17
                                                                                                   NCALC =-0 NDATA = -0 NBL = 1
     ROTOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 3 POINTS
                                                                          1-GOORD LOSS COEFF/TOTAL LOSS COEFF
                                                                              0.0000
                                                                                                                                                                                                   0.0000
OUTLET RAJIUS = 7.5499
                                                                       H-COORD
                                                                                                                                               DEVIATION ANGLE (DEGREES)
                                                                                    .2000
.4000
.8000
```

```
(4) OUTLET RADIUS = 7.7343
                H-COORD DEVIATION ANGLE (DEGREES)
                  .2000
.4000
.8000
(4) OUTLET RADIUS = 7.9385
                M-COORD DEVIATION ANGLE (DEGREES)
                  .2000
.4000
.5000
                                  -5.1000
-4.2030
-4.6500
(4) OUTLET RADIUS = 8.1919
                M-COORD DEVIATION ANGLE (DEGREES)
                  •2000
•4000
•8000
                                  -5.3750
-5.7420
-0.5890
(4) OUTLET RADIUS = 8.6599
                Y-COORD DEVIATION ANGLE (DEGREES)
                  .2000
                                 -5.3250
-12.3300
-25.0850
                  .4000
     STATOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 6 POINTS
                H-COORD LOSS COEFF/TOTAL LOSS COEFF
                 0.0000
                                    0.0000
     OUTLET RADIUS = 0.0000
                A-COORD DEVIATION ANGLE (DEGREES)
                 0.0000
-2000
-4000
-6000
                                     .1000
.1100
.1500
.2200
                 1.0000
                                    1.0000
     NUMBER OF TEST POINTS TO BE ANALYSED =
(5) PSCALE= 1.00 PLONER= 14.00 DAMPF= 5.000 NSAVE= 1 NNHAX= +0 MFORGE= +0 NEX= 2
```

## SECTION 5. COMMON PHASE II INPUT AND TEST POINT DATA (LOG 3, LOG 4) WITHIN BLADE

#### IEST_QATA_PSINTQUI_EQR_PQIdT_NQ.__1

```
TEST POINT TITLE
GAS CONSTANT
AIR MASS FRACTION
FLOWRATE PRESSURE
INLET TOTAL PRESSURE
INLET TOTAL PRESSURE
INTERNATIONAL TOTAL
P INTO IN(STD)
P IN/P IN(STD)
 ROTUR OUTLET TOTAL PRESSURE ( 5 POINTS)
    LLIGAS
                         PRISSURE
   7.3710
5.0010
8.1210
6.2510
8.3710
 ROTUR DUTLE. WIAL TEAPERATURE ( 5 POINTS)
                        T: MPERATURE
    RADIUS
   7.8710
8.3010
8.1210
3.2310
5.3710
                         972.227
572.272
573.975
574.431
574.050
STAGI OUTLET TOTAL PRISSURES ( 5 POINTS)
    RAJIUS
                    MEAN PRUS
                                           PLAK PRES
   7.3000
7.9530
8.1200
8.2530
8.4430
                      20.1102
90.0019
70.1487
20.2026
70.1297
                                            20.6143
20.5503
20.7571
20.5903
20.4592
STAGE DUTLET TOTAL TEMPERATURES ( 5 POINTS)
    RADIJS
                       TE MPERATURE
                         973.687
973.153
9775.339
977.637
973.322
    7.3000
STAGE DUTLET FLOW ANGLES ( 1 POINTS)
    RAJIUS
                          AHGLE
    0.0000
                           0.000
CASING STATIC PRISSURES (14 POINTS)
                         PRESSURE
    X-CUJKD
  -2.0000
    0.0000
2530
-5200
```

HUB STATIC PRESSURES ( 5 POINTS)

X-CODRU	PRESSURE
-2.0030 2500 2.2500 4.7250 6.1610	14.4513 14.3257 16.3502 17.6345 17.6346

(5) DISTRIBUTED BLOCKAGE SPECIFICATION

VOITATE	<b>PLOCKAGE</b>	DISTRIBUTION FACTOR	MID ADD.DEVN.	DISTRIBUTION FACTOR	FRACTION TE BLOCKAGE
<u>}</u>	0.00000	1.0000	-0.000	-0.0000	-0.000
3	0.00000	1.0000	-0.000	-0.0000	-0.1601
Ď	0.00000 0.1100	• 6000	• 610 • 610	1.0000	:200
8	.0.300 .01000 .03600	. 20 00 a. 00 00	010	1.0900	
10 11	02000	0.0000	-0:000	-0.000	:1:111
12	11000	1.0000	-0.000	-0.000	-1.1010
1.5 1.5	10000	1.0000	-0.000	-0.0000	3:111
16 17	.10000 .10000	1.0000 1.0000	-0.000 -0.000	-0.000 -0.000	-1:0101

(5) SOLUTION TYPE INDISATORS

## SECTION 6. INDIVIDUAL TEST INPUT DATA

a. EXCEPTIONS TO SECTION 1 DATA (Indicated by (1))

Test Point Number	Exception (1)
212050109840	14-1590
212050213440	##
212050315040	***
212050415940	nn
212050516240	m
212050616440	mm
212050615050	14.1590
212050815750	nn
212050916250	nn
212051015050	1111
212051114250	<b>11 11</b>
212051212250	HH
212051415060	20 27
212051514360	ĦĦ
212051612960	HH
212051715560	##
212051815960	***************************************
212051916360	1911
212070215070	14-5035
212070314770	*****
212070615070	##
212070715670	1111
212070815970	nn 
212070916170	1111
212071015080	14.5035
212071315080	nn
212071415580	11 11
212071515980	n
301180915685	14.2208
301181015885	111
301180615085	1111
301180815385	***
301181515590	14.2208
301181615790	- ""
301181715890	. 1144
301181415290	nn

301230615095 301230415395 301230515695	r 1097 '''	15.0097 ""	15.00	30.00 ""
301231515600 301231615700	5 <b>.</b> 0097	15.0097	15.00	30.00
301231315200	1111	1117	1111	1111
301231415400	****	11 11	****	1111
301340815302	1111	11 11	1111	1111
301240915602	71 71	1117	17.11	10.10

# b. EXCEPTIONS TO SECTION 2 DATA (Indicated by (2))

1000 101110	222070207010		
Station 4 5 6 7	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212050213440		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212050315040		
Station 4 5 6 7 3	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212050415940		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	21205016240		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1

Test Point	212050616440		
Station 4 5	NCALC 1 4	NDATA 15	V

NCALC NDATA NBL
1 15 1
5 4 15 1
6 0 0 1
7 1 10 1
8 3 10 1

Test Point 212050615050

Station 4 5 6 7	NCALC 1 4 0	NDATA 15 15 0 10	NBL 1 1 1
8	3	10	ì

Test Point 212050815750

Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1
.,	3	10	1

Test Point 212050916250

Station	NCALC	NDATA	MBL
٦ ج	÷	15	1
ي ا	4	15	1
. 6	0	Õ	1
7	1	10	ī
Ø	3	10	ī

Station	CICALC	NDATA	NBL
4		15	1
5	4	15	1
6	0	0	
7	1	10	ī
8	3	10	1

Test Point	212051114250		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10 10	NBL 1 1 1 1
Test Point	212051212250		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10 10	NBL 1 1 1 1
Test Point	212051415060		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212051514360		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212051612960		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1

Test Point	212051715560	•	
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212051815960		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212051916360		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212070215070		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212070314770		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1

Test	Point	21207	70615070
------	-------	-------	----------

NCALC	NDATA	NBL
1	15	1
4	15	1
0	Ô	1
1	10	1
3	10	1
	NCALC 1 4 0 1 3	1 15 4 15 0 0 1 10

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

## Test Point 212070815970

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	Ó	1
7	ì	10	1
8	3	10	1

## Test Point 212070916170

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	Ó	1
7	ī	10	1
8	3	10	1

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	Ô	1
7	1	10	1
8	3	10	1

Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212071415580		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	212071515980		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 1 1 1 1
Test Point	301180915685		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDALIA 15 15 0 10 10	NBL 0 1 1 2

rest	Point	301181015885

Station 4 5 6	NCALC 1 4 0	NDATA 15 15	NBL 0 1
7 8	1 3	10 10	1 2 1

Test Point	301180615085		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 0 1 1 2
Test Point	301180815385		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 0 1 2
Test Point	301181515590		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 0 0 0 0 0
Test Point	301181615790		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10 10	NBL 0 0 0 0

21	6
<b>~1</b>	·U

NBL

Test Point	301181415290		
Station 4 5 6 7 0	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 0 0 0 0
Test Point	301230615095		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 0 0 0 0 0
Test Point	301230415395		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 0 0 0 0 0
Test Point	301230515695		
Station 4 5 6 7 8	NCALC  1  4  0  1  3	NDATA 15 15 0 10	NBL 0 0 0 0
Test Point	301231515600		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 0 0 0 0 0

Test Point	301231615700		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10 10	NBL 0 0 0 0 0
Test Point	301231315200		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 0 0 0 0 0
Test Point	301231415400		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10 10	NBL 0 0 0 0 0
Test Point	301240815202		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 0 0 0 0 0
Test Point	301240915602		
Station 4 5 6 7 8	NCALC 1 4 0 1 3	NDATA 15 15 0 10	NBL 0 0 0 0 0

# c. EXCEPTIONS TO SECTION 3 DATA (indicated by (3))

CISTRIBU	TED BLCCKA	GE SPECIFICATION	
STATION	BLCCKAGE	DISTRIBUTION FACTOR	<del></del>
1	C.60066	1.0000	
3	0 - 0 u 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.0000	<del></del>
	i. CCC0	1.0003	
	C-GCCO ú	1.0000	
5	.588Cû	1.0009	
	**************************************	1.0606	and the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of th
7	• 08606	1.0000	
	<del>- 05400</del>	1 6 9 6 9	
ç	.05405	1.0600	
		1+6668	
SCLUTION	TYFL INGI	FATORS	

Test Point 212050213440

STATION	BLCCKAGE	DISTRIBUTION FACTOR	
1	0.00000	1.00C0	
<del></del>	0.06630	1.0850	
3	0.00000	1.0000	
4	0.0000C	1.0000	
5	.08600	1.0000	
<del></del>		1.0000	
7	00380.	1.0000	
		<del></del>	
Ġ	. 054G C	1.3660	
	- 605×00		

PSCALE = .50		PLOMER = 14.0	DAMP $F = 6$ .
CISTRIBU	TED HLCCKA	GE SPECIFICATION	
STATION	BLCCKAGE	DISTRIBUTION FACTOR	
1	0.0000	1.0060	
<del></del>	0.50000	1.000	<del> </del>
3	0.00000	1.00 <b>0</b> 0	
	<b>C.</b> 01103	1.0000	<del></del>
5	.04005	1.0000	
6	- 609800	1:000	<del></del>
7	.0802	1.6368	
8		1,000	·
Ğ	.65430	1.0000	
-16	- 05486	1.0000	
SOLUTION	TYPE INUI	CA TORS	<del></del>
STATION-		+ 5 6 7 t -9 10-	
NHACH	3 U -0 -	· ( -0 -0 -0 -0 -0 -0	

PSCALE = .50

PLOWER = 14.0

DAMP F = 6.0

DISTRIBUTED SLOCKAGE SPECIFICATION

STATION	BLCCKAGE	DISTRIBLTION FACTOR
1	0.00000	1.0000
	0.00000	1.0000
3	1.66605	1.0960
4	C - O U C O O	1.000
5	000000	1.0000
	.09000	1.0000
7	00080.	1.0200
		1.0009
S	.0540G	1.0009
	.05400	1.0003

-SCLUTION TYPL INDICATORS

STATION 1 2 3 4 5 6 7 6 9 16 - - NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

Test Point 212050516240

PSCALE = .50 PLOWER = 14.0 DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATICN	BLOCKAGE	DISTRIBUTION FACTOR
1	0.0000	1.0000
2	- 0.0000 -	1.6800
3	0.00000	1.0000
	G. U 8 8 C	1.0000
5	.08065	1.0000
	- *89000	
7	.08000	1.0000
		1.0000
g	.05480	1.0009
16	<del></del>	

-SOLUTION TYPE INDICATORS

STATICN- 1 - 2 - 3 - 4 5 6 7 8 9 10 - - NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0

PSCALE =	.50	PLOWER = 14.0	DAMP $\dot{\mathbf{F}} = 6.0$
DISTRIBU	TED BLOCKA	GE SPECIFICATION	
STATION	BLCCKAGE	DISTRIBUTION FACTOR	
1	0.00000	1.0000	
<del></del>	0.00C00	1,0000	
3	0.0000	1.0000	
+	0.00000	1.0000	
5	.08000	1.0000	
<del>6</del>	8 <del>9 8 8 -</del>	<del></del>	
7	.08600	1.0000	
8	<del></del>	<del></del>	
9	.05400	1.0000	
10	<del> 35488</del> -		
<del>-SOLUTION</del>	- <del>1 Y P E - 1 N B 1</del>	CATORS	
STATION	-1-2-3-	4 5 6 7 <del>6 9 18</del>	
NMACH	0 0 -0 -	C -0 -0 -0 -0 -0	

### Test Point 212050615050

PSCALE = 1.0	PLOWER = 13.0	DAMP F = 6.0
CISTRIBUTEO	SPECIFICATION	

STATION	BLCCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
<del>2</del>	0 * 0 ÷ 0 C O -	
3	0.00000	1.0000
<del></del>	<del>- 0.06000</del> -	1.6060
5	.08000	.5003
7	•0000 •0000	1.0000
	<del></del>	1.0060
è	.05400	1.0000
-16	<del></del>	1+6080

-SOLUTION-TYFE-INDICATORS-

STATION 1 2 3 4 5 6 7 8 9 10 NMACH 0 0 -0 -C -0 -C -0 -C -C -C

PSCALE = 1.0 PLOWER = 13.0 DAMP F = 6.0

OISTRIBUT : C	BLCCKAGE	SPECIFICAT	ICN
---------------	----------	------------	-----

STATION	BLCCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	C + C C C C C C C C C C C C C C C C	
3	1.00000	1.0000
	<del> €+++++++</del>	
5	10381.	• 50 <b>0</b> 0
<del></del>	<del></del>	<del></del>
7	.08600	1.0600
<del></del>	<del> +05486-</del>	
9	.05460	1.00
<del></del>	<del></del>	<del></del>
<del>-SCLUTIO</del> N	- <del>TYPE-INDI</del>	CA FORS-
STATIEN-	<del></del>	<del>4-5-6-7-8-9-1</del> 6-
NHACH		6- 0- 0- 0- 0- 0

#### Test Point 212050916250

PSCALE = 1.0 PLOWER = 13.0 DAMP F = 6.0

DISTRIBUTED 9	LCCKAGE S	PECIFICATION	1
---------------	-----------	--------------	---

STATION	BLCCKAGE	CISTRIBUTION FACTO
1	0.00036	1.6360
2	0.00000	<del></del>
3	9.00000	1.0000
<del></del>	<del>- 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 </del>	<del>1,6003</del>
5	.38600	.5000
—		
7	0000c	1.0000
<del></del>	<del></del>	
9	.05400	1.000
<del>16</del>		

-SOLUTION -FYPE -INDICATORS----

STATION 1-2-3-4-5-6-7-6-9-10-NMACH 0 0-3-C-0-C-0-C-C

PSCALE =	1.0	PLOWER = 13.0	DAMP F = 6.0
CISTRIBU	TED HLCCKA	GE SPECIFICATION	
STATION	RECCKAGE	DISTRIBLTION FACTOR	
1	0.00000	1.0000	
2	- C. + + + + + + + + + + + + + + + + + +		
ક	1.0.666	1.0000	
ts -	· · 6 • 9 = <del>69 t -</del>		
5	60382.	.5089	
<del>6</del>	<del></del>		
7	.08000	1.0000	
	<del> </del>	<del></del>	
9	00+00	1.9093	
16-	* * * * * * * * * * * * * * * * * * *		
-SOLUTION	- TYFE INGI	CATORS	
STATION NMACH	1 2 3	<del>4 5 6 7 8 9 18</del> • ( -) -) -( -0 -0 -(	

	0	PLOWER = 13.0	DAMP F = 6.0
EISTRIBUTE	ED BLCCKA	GE SPECIFICATION	
STATION '	3LCCKAGE	DISTRIBUTION FACTOR	
1	6.9.800	1.0000	
<del></del>	-6 • 0 6 6 6 ·	1.000	
3	32331.3	1.0000	
4	- <del>6 + 8 C C 0 C -</del>		
5	00000	C • 00 60	
<del></del>	**************************************		
7	.08660	1.0000	
	<del>05400</del> -	1.0000	
ç	. 65466	1.0000	
	- 85 <del>46</del> 8	<del></del>	

STATION	BLCCKAGE	DISTRIBLTION FACTOR	
1	[•6365a	1.0000	
2	0 . 0 <del>0 6 .</del> 0		
3	101111	1.0869	
	- <del>- 6 + 0 f ( f i) -</del>		
		0.0000	
<del></del>		<del></del>	
7	8(3)		
<del></del>		1. <u>0</u> 0-60	
ģ	. (5400	1.000.	
— <u>+</u>	<del></del>		
= :			

#### Test Pooint 212051415060

PLOWER =  $\pm 3.0$  DAMP F = 6.0PSCALE = 1.0 -STATICY - FLCCKAUT -- UISTKIPUTIEW-FACTOR 1.0000 0.26530 3 --- - De Or BO pro---- Peto Ct. . . . . - 10 Chil 1.03.0 • ເວັ້ເ r. u2 89 8 .54) 1.600 9 · ·····•<del>5948</del>········· 1.666······ €19433 1.0003 SCLUTION TYPE INDICATORS STATION 1 2 3 4 5 F 7 8 9 16 ንት የተጠታተው ነው ነው ነው ነው ነው ነው ነው ነው ተመሰብ ተመ

PSCALE = 1	0	PLOWER = 13.0	<b>DAMP F = 6.0</b>
DISTRIBUT	FED BLOCKAGE	SPECIFICATION	-
STATION	SLCCKAGE D	ISTRIBUTION FACTOR	-
	- <del>C. b ú CO O</del>	1.6000	_
2	0.00000	1.000	_
4	0.0000 0.0000	1.0000 1.0000	_
<del></del> 5	<del>0000</del>		-
٤	.08000	9.0099	
8	•0 <del>0000</del> •05400	1.0000	-
<del>-</del>	-05400	1.6060	-
16	.05400	1.0000	-
SOLUTION	TYPE INDICA	TORS	_
STATION	1 2 3 4	5 6 7 8 9 10 -0 -6 -6 -6 -8 -8	-

PSCALE = 1	1.0	PLOWER = 13.0	DAMP $F = 6.0$
- CISTRIBU	TEC RECCKA	E SPECIFICATION	
STATION	BLCCKAGE	DISTRIBUTION FACTOR	
	0.65000	1.6000	
2	0.00000	1.0000	
	- C. CCCCO C	1.0000	•
4	C.00000	1.0009	
<del>5</del>	*00600		•
6	.0000	0.0000	
7		1.0009	-
8	.05406	1.0003	
<del>_</del>		1.5966	•
16	•0540G	1.0600	_
SOLUTION	TYPE INDIC	ATORS	-
STATION	· -	5 6 7 8 9 10	-

PSCALE = 1	.0	PLOWER = 13.0	DAMP F = 6.0
-ÚISTRIMUT	ED PLOCKAGE S	PECIFICATION	-
STATION	HLCCKAGE DIS	TRIBUTION FACTOR	-
	- t - 6 t 9 t	150900	-
2	33333.6	1.G0C0	
	£ 0 € 0 € € €		-
4	0.10000	1.0000	
<del></del>	• <del>0000</del> 0		-
6	. 18063	C• 30 C3	
<del>7</del>	<del></del>	1.6000	-
8	• ū54C E	1.0069	
	<del></del>	1.0960	-
10	.65400	1.0000	_
SCLUTION	TYPE INDICATO	RS	
	1 2 3 4 5	6 7 8 9 10	
-MACH	<del>- 3 - 0 - 0 - 0</del>	<del>····································</del>	-

PSCALE = 1	1.0	PLOWER = 13.0	DAMP F = 6.0
<del>"DISTRIBU</del>	TEB HECCKA	CE SPECIFICATION	
STATION	- 3LCCK#GE	DISTRIBUTION FACTOR	
<u>1</u>		1. 00 00	
4	U.3500U	1.00C0 1.00C0	
£	-00000 -00000 	C • 00 00 C • 00 00	
8	•6549 C	1.5063 1.9660	
18	. 15400	1 • C û O O	
	TYPE INDI		
STATION -		4 5 6 7 8 9 10 f =0 =================================	

PSCALE = 1	L.0		P	LOWE	R =	13.	0		DAMP $F = 6.0$
-CISTRIBU	Tub aud	CKAC	<del>. SP</del>	ECI	FIC	ATI	EN-		_
STATION	<del>el cc</del> k#	i <del>ŭ E</del>	JIST	RIA	<del>ui I</del>	CK-	F <del>A (</del>	TCR	<b>-</b>
2	0.360 0.20				1.0 1.0			<del></del>	_
4	0.000	<del>ឋ ប</del>			1. C	<del>u 00</del>			_
6	160°	0.0			C. 0	000	· · · ·		_
	.:::: 15: 1 <del>0:</del> -	iù C			1.0 1.0	ı Çu			
10	.654			<del></del>	1.0				<del></del>
SCLUTION	TYFE	NLIC	ATCK	\$					
STATION	_	3 4	5	<u> </u>	7	8	9		

PSCALE = 2	2.0	PLOWER = 13.0	DAMP F = 6.0
DEISTRIBU	TED BLOCKA	GE SPECIFICATION	_
STATION	BLOCKAGE	DISTRIBLTION FACTOR	
1	0.00000	1.0000	
2	6.66686	1.0000	•
3	0.00000	1.0000	
	<del>6.0000</del>		-
5	30083.	6.0000	
- <b>6</b>	·· •0000		
7	.08000		
	- 4540-0		-
9	.05400		
16		1.0000	-
_	TYPE INC	ECATORS	-
STATION	1 2 3	.4 5 6 7 8 9-16	<del>-</del>
NMACH	0 0 -0	0 - 0 - 0 - 0 - 0	

PSCALE = 2	2.0	PLOWER = 13.0	DAMP F = 6.0
DISTRIBU	TLD ELCCKA	GE SPECIFICATION	
STATION	PLCCKAGE	DISTRIBUTION FACTOR	
ì	0.00636	1.0000	ı
2	0.00000	1 • ປິບ 6 ປັ	
3	0.0000	1.0000	
		0.0903	
		€ 6 € 6 5	
		1.6900	
		<del></del>	
		1.0000	

STATION	BLCLKAGÉ	DISTRIBUTION FACTOR	
1	0.00000	1.0000	
٤	6.01(66	1 • 3 € <del>6 9</del> ·	
3	0.00000	1.0000	
	<del></del>	<del>1-fif1</del>	
5	.455_6	:• 3u 0 3	
	<del></del>	- 6.666	
7	.08060	1.3683	
<del>6</del>	v ċ <del>5 4 ċ</del> €	- ··4.6669	
Ģ	. ب <b>54</b> ر ر	1.0900	
		1.0002	

Test Point 212070715670

PSCALE = 2.0 CISTRIBUTED BLCCKAGE		PLOWER = 13.0	DAMP F = 6.0
		GE SPECIFICATION	
STATION	BLCCKAGE	DISTRIBLTION FACTOR	
1	0.00000	1.0000	
2	8.0000	1 = 00 00	
3	0.00000	1.0000	
	<del>6.0000</del>		
5		C • 00 G0	
<del></del>	<del>10000</del>		
	.08030		
	<del></del>		
ģ	.05400		
<del>- 1t</del>	<del>05400</del>	<del></del>	
•		EA TORS	
STATION	1 2 3	4 5 6 7 8 9-1G-	
NMACH	g g -g -	0- 6- 8- 3- 0- 6- 3-	

PSCALE = 2.0		PLOWER = 13.0	DAMP F =
DISTRIBU	TEC BLOCKA	GE SPECIFICATION	
STATION	BLCCKAGE	DISTRIBLTION FACTOR	
1	0.01000	1.0000	
2	- u = 0 + 0 0 <del>C</del>		
3	0.03000	1.000C	
	0.2000	1.0000	
5	.08060		
·····	+6866 ·	<del>1-3000</del>	
7	.08630	1.0000	
<b>.</b>	·····65486-		
9	. 05400		
		1.0000	
SCLUTION	TYPE INDI		
STATION .	1 · 2 3	4 5 6 7 - <del>6 -9-1</del> 6	
<b>LMACH</b>	3 3 -3 -	1 -0 -0 -0 -0 -0	

Test Point 212070916170

STATION	BLCCKAGE	DISTRIBUTION FACTOR	
1	0.0000		
Ź	0.60000	- <b>1 : 0:0</b> 0 3	
3	C1696	1.0000	
	<del></del>		
5	.38553	C. 50 65	
7	• 9800 -	1.0900 	
ç	.05460		
	<del></del>		
SOLUTION	TYPE INGI	CATORS	
STATION	1 2 3	5 6 7 8 9 10-	
MMACH	<b>J</b> U -1 -1	2 -0 -0 -0 -0 -0	
Point 2120		PLOWER = 13.0	DAMP F = 6.
PSCALE = 2	2.0	PLOWER = 13.0	DAMP F = 6.
PSCALE = 1	2.0 T_L &LCGKA(	PLOWER = 13.0  E SPECIFICATION  DISTRIBUTION FACTOR	DAMP F = 6.
PSCALE = 1	3LCCKAGL BLCCKAGL	DISTRIBUTION FACTOR	DAMP F = 6.
PSCALE = 1	2.0  T.L. BLCCKAC  BLCCKAGL  (	DISTRIBUTION FACTOR  1.0003	DAMPF=6.
PSCALE = 1 CISTRIBU STATION  1 2 3	2.0  TLL BLCCKA(  BLCCKAGL  (.)	DISTRIBUTION FACTOR  1.0003 1.0003 1.0003	DAMP F = 6.
PSCALE = 1 CISTRIBU STATION  1 2 3 4	2.0  TLU PLCCKAC  BLCCKAGL  COCCCC  COCCCCCCCCCCCCCCCCCCCCCCCCCC	DISTRIBLTION FACTOR  1.0003 1.0003 1.0003 1.0000	DAMP F = 6.
PSCALE = 1 CISTRIBU STATION  1 2 3 4 5	2.0  T_L @LCCKAC	DISTRIBUTION FACTOR  1.0000 1.0000 1.0000 1.0000	DAMP F = 6.
PSCALE = 1 CISTRIAL STATION  1 2 3 4 5	2.0  T_L PLCCKAC	1.0003 1.0003 1.0003 1.0000 1.0000 0.0000	DAMP F = 6.
PSCALE = 1 CISTHIAU STATION  1 2 3 4 5 6 7	2.0  TLU PLCCKAC  BLCCKAGL  C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C	1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	DAMP F = 6.
PSCALE = 1 CISTRIAL STATION  1 2 3 4 5	2.0  T_L PLCCKAC	1.0003 1.0003 1.0003 1.0003 1.0000 0.0000 0.0003 1.0000 1.0000	DAMP F = 6.

PSCALE = 2.0 PLOWE. - 13.0 DAMP F = 6.0

STATION 1 2 7 4 9 E 7 E 9 10 NMACH J 8 +7 +0 +1 +0 +0 +0 +0

SCLUTION TYPE INDICATORS

PSCALE = 2	.0 PLOWER = 13.0	DAMP F = 6.0
<u> </u>	TED BLOCKAGE SPECIFICATION	
STATION	SECONAGE DISTRIBUTION FAC	CTCR
1	£.00000 1.5025	
2 3	6.65669 1.0060 6.0066 1.6060	
4	<u> </u>	
5	.0800 L C. 0000	
6	.08CC. [.CCC	
7	.£8630 1.6063	
6	.05416 1.0000	
ç	.05436 1.0000	
13	.1540. 1.5030	
SCLUTION	TYFF INCICATORS	agraphic deglishman
STATION	1 2 3 4 5 6 7 8 9	10
NMACH	) 6 -2 -2 -3 -2 -1 -6 -0	<u>• [</u>

PSCALE = 2.0		PLOWER = 13.0	DAMP $F = 6.0$
CISTRIBLE	TED BLOCKA	GE SPECIFICATION	
STATION	BLCCKAGE	DISTRIBUTION FACTOR	
1	2622643	1.0000	
2	0.0000	1.000	
3	10000000	1.0000	
4	0.00000	1.0003	
5	0008n.	C.C006	
<del></del> 6	.23800	0.0000	-
7		1.0363	
ò	. 1545 6	1. CC CO	•
S	.09430	1.0002	
16	.[54[3	1.0060	-
SCLUTION	TYPL INCI	CATORS	-
STATION NMACH		4 5 6 7 8 9 1C -C -0 -0 -0 -0 -C	-

PSCALE = 2.0		PLOWER = 13.0	<b>DAMP F = 6.0</b>
CISTRIBUTED BLUCKA		GE SPECIFICATION	
STATION	BLCCKAGE	DISTRIBUTION FACTOR	
1	L. UL GOU	1.0000	
2	9.00000	1.9600	
3	ioultur	1.0000	
4	23356.0	1.0000	
5	.06000	E. C. 3 G. 9	
F	.08603	6.0000	
7	.00000	1. GG CO	
8	.09400	1.0000	
g	. 65460	1.0963	
16	.05496	1. Cù G0	
SCLUTION	TYPE INCI	CATCRS	
STATION	1 2 3	4 5 € 7 8 9 1C	
MACH	<u> </u>	C -0 -C -C -C -G -C	

PSCALE = 4.0 PLOWER = 12.0 DAMP F = 4.0

Test Point 30180615085

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE CISTRIBUTION FACTOR

1 0.00000 1.0000
2 0.00000 1.0000

	1	1.000
*	3	1.0000
	05000 6 • 05000 7 • 05000	0.000 0.000 1.000
	07000 9 .07000	1.0000 1.0000
	807000	11000

SCLUTION TYPE INDICATORS
STATICN 1 2 3 4 5 E 7 8 9 10

PSCALE = 4	1.0	NTOWER = 15	.0	DAME I = 4.0
DISTRIBU	TEC BLOCKA	GE SPECIFICATI	CK	
STATION	BLOCKAGE	CISTRIBUTION	FACTOR_	
1 2	0.00000	1.0000		
3	0.00000 0.00000	1.000G 1.000G		
5 6 7	.05000 .05000	0.0000 0.6060 1.6066	er en sit framen allerina.	
89	.07000 .07000	1.6000 1.0000		
10	10/000	280000		
SCEUTION	TYPE INUI	CATORS		
STATION	1 2 3	4 5 6 7 8	9 10	

PSCALE = 1	4.0	PLOWER = 12.0	DAMP F = 4.0
DISTRIBU	TED BLOCKAGE SE	PECIFICATION	
STATION	JLOCKAG- CIST	FACTOR -	
1	0.00000	1.0000	
5	0.00000	1.0000 1.0000	
6	• 05 00 0 • 05 00 0 • 05 00 0	0.0000 0.000C	
8 9	.07000 .07000	1.0000 1.0000	
SCLUTION	TYPE INDICATOR	3,000	
STATION	1 2 3 4 5 0 -0 -0 -0	6 7 8 9 10 -6 -0 -0 -0 -0	

PSCALE = 4.0

PLOWER = 12.0

DAMP F = 4.0

Test Pcint 301181415290

PSCALE = 2.0

PLOWER = 13.0

DAMP F = 5.0

CISTRIBLTEC BLCCKAGE SPECIFICATION

STATION	BLCCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0030L.a	1.6000
3	0.00000	1.0000
4 .	0.00000_	1.0000
5	.03750	C. 0000
£	.03750	C.0000
7	.07500	1.0000
. &	.27000	1.0000
9	.05400	1.6060
10	05400	1.6000

SCLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 . NMACH 0 0 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0

PSCALE = 2.0 PLOWER = 13.0 DAMP F = 5.0

#### CISTRIBUTED BLOCKAGE SPECIFICATION

STATICN	BLCCKAGE	DISTRIBLTION FACTOR
1	0.00000	1.0000
2	0.0000	
3	6.80600	1.0060
44	9.00000	1.1010
5	.02750	6.6660
<b>£</b>	03750	0.8888
7	.07500	1.6068
8	.26000	1.0066
9	.05480	1.6090
. 16	.05400	1.0000

#### SCLUTICA TYPE INDICATORS

STATION 1 .2. 3 4 5 6 7 .8 .9 18 ... NMACH 5 0 -0 -0 -0 -0 -0 -0 -0 -0

Test Point 301181615790

PSCALE = 2.0 PLOWER = 13.0 DAMP F = 5.0

#### CISTRIBUTED BLCCKAGE SPECIFICATION

STATION	BLCCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2		1.0000
3	0.06000	1.0000
44	0.00000	1.0000
5	.03750	C. 00 GO
6	. £375.£	C. CO CO.
7	.07500	1.0000
. 8	25 CQ G	1,0000
ġ	.05400	1.0000
10	.05400	1.6000

#### SOLLTION TYPE INDICATORS

STATICN 1 2 3 4 5 6 7 8 9 10 AMACH 8 8 -0 -C -0 -0 -0 -0 -8 -8

PSCALE = 2.0

CISTRIBUTED BLCCKAGE SPECIFICATION STATION BLOCKAGE DISTRIBUTION FACTOR 0.0330.0 1.0060 3.00000 1.0000 0.00000 1. 00 60 0.00000 1.0000 .03750 0.0000 .03750 C. 00 CD .07500 1.0000 .24006 1.0000 9 .05400 1.0000 1. CO CO 15 . .05400 SCLUTION TYPE INDICATORS SYATION 1 2 3 4 5 6 7 8 9 10 NMACH L 0 -0 -0 -0 -0 -0 -0 -0 Test Point 301230415395 DAMP F = 5.0PSCALE = 2.5PLOWER = 13.0DISTRIBUTED BLOCKAGE SPECIFICATION STATION BLOCKAGE DISTRIBUTION FACTOR 1.0000 1010101 2 6.00000 1.0663 C.S((b( 1.0000 133330.4 1.0000 C. CGGG .0375 C 1.0060 7 .675.6 22356 C 1. 6866 ċ . U.S.4U.C 1.0000 16 .35400 1.0000 SCLUTION TYPE INDICATORS

PLOWER = 13.0

DAMP F = 5.0

) 0 -0 -( -0 -6 -6 -6 -0 -6

STATICN 1 2 3 4 5 6 7 8 9 10

NMACH

PSCALE = 2.5

PLOWER = 13.0 DAMP F = 5.0

DISTRIBUTED BLCCKAGE SPECIFICATION

STATICN	BLCCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	6.00000	1.0000
3	0.00000	1.0000
4	6.60000	1.0060
5	.05000	C.00G0
6	.05000	C- 00 00
7	.18000	1.0000
8	.25000	1.0000
9	.05430	1.0000
16	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION 1 2 3 4 5 6 7 8 9 10 NMACH C 0 -0 -C -0 -C -0 -0 -0 -0

Test Point 301230615095

PSCALE = 2.5

PLOWER = 13.0 DAMP F = 5.0

CISTRIBUTED BLCCKAGE SPECIFICATION

STATION	BLCCKAGE	DISTRIBLTION FACTOR
1	C.00000	1.0900
2 -	6.80060	1-8080
3	C.00000	1.0000
4	- 0.00000	1.0000
5	.03750	0.0060
	+03750	0.0000
7	.07500	1.0000
8	.26500	1.0000
9	.05400	1.0000
1.0	.05400	1.00CO

- SCLUTION TYPE INCICATORS - - - - -

STATIGN-1-2 3 4 5 € 7 8 9 10 NMACH 0 0 -0 -C -0 -0 -0 -0 -0 -0

PSCALE = 4.0PLOWER = 12.0 DAMP F = 4.0SISTRIBUTED BEBEKAGE SPECIFICATION STATION PLOUKAGE DISTRIBUTION FACTOR. 1 2 3 9.23859 1.0000 1. CJC 39 1. CJC 39 0. 000 C 0. 2756 0. 07500 0. 27500 1.0000 1.000 1.000 0.000 1.000 1.000 1.000 1.000 1.000 • 20000 . 17411 ត្រូវម៉ាងម៉ាហ៊ី 👚 😁 11 SULUTION TYPE INDICATORS 

Test Point 301231415400

1

PSCALE = 4.0

PLOWER = 12.0 DAMP F = 4.0

DISTRIBUTED BLOCKAGE	SPECIFICATION
STATION BLOCKAGE D	STAIBUTION FACTOR
1 0.00000	1.0000
3 0.0000 4 0.0000	1.0000 1.0000 1.0000
5 .05000 6 .05000	0.0000 0.0000
8 • 25000 9 • 05400	1.0000 1.0000 1.0000
10 .05400	1.000
SCLUTION TYPE INUICA	TORS
STATION 1 2 3 4	5 6 7 8 9 10 0 - 6 - 0 - 0 - 0 - 0

Test Point 301231615700

PSCALE = 4.0 PLOWER = 12.0 DAMP F = 4.0

HATICH	BLOCKAGE JIS	TRIBUTION FACTO
1	0.00000	1.0000
3	0.00000	1.0000
	0.00000 .05000	0.000C
é	.05000 10000	Q. CONO 1. CONO
8	. 26000	1.0000
<del>-10</del>	• 05400 • 05400	1.0000
	TYPE INDICATO	

PSCALE = 4.	.0	PLOWER = 12.0	DAMP $F = 4.0$
गडा राउग	ID BLOCKA	GL SPECIFICATION	
ATATION .	JLCUKAGL.	_ BEIDAR MOLLULIFIELD.	
1 2	0.00000	1.000	
7 ty:57 bg	0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	1.000 1.000 1.000 0.000 0.000 1.000 1.000	
SCLUTION	TYP1 1001	CATCES	
PARTICH FURNAL	1 2 3 3 - 0 - 3 -	7 - 2 - C - 7 - C - 9 1 7 C - 0 - 1	

## Test Point 301240915602

# d. EXCEPTIONS TO SECTION 4 DATA (Indicated by (4))

Test Point 212050315040

Station	NCALC	NDATA	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	2	15	3

Station	NCALC	NDATA	NBL
5	2	15	3
6	2	15	ž
7	2	15	จั
8	2	15	<b>4</b>
9	2	15	3

```
OUTLIT RADIUS = 7.3499
            1-COORJ
                         DEVIATION ANGLE (DEGREES)
              .2001
                                 -9.0000
-3.7000
-8.3000
              .4000
              . 5000
                                 -8.0000
DUTLIT KAJIUS = 3.0331
            1-000RJ
                         DEVIATION ANGLE (DEGREES)
              .2000
.4300
.5000
                                 -7.3000
-7.2000
-7.1000
-7.0000
Etco.6 = CUICA, TELTUC
            1-00020
                         OCVIATION ANGL. (DEGREES)
                              -3.0000
-3.1000
-10.2000
-11.2000
              ·2003
              4303
              • 2002
```

Station	NCALC	NDATA	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	2	15	3

```
OUTLIT KAJIUS = 3.6599

4-COCO DIVIATION ANGLE (DEGREES)
.2000 -7.7500
-9.0500
-9.0500
-10.3500
-11.0500
```

Station	NCALC	NDATA	NBL
5	2	15	3
6	2	15	3
7	2	15	ž
8	2	15	3
9	4	15	3

```
OUTLIT RAJIUS = 7.5439
            M-COORJ DEVIATION ANGLE (DEGREES)
               .2300
.4000
                                 -5.1750
-5.4200
-4.7700
               . 8000
DUTLOT RADIUS = 7.73+3
            1-00033
                         JIVIATION ANGLE (DEGREES)
              .2000
.4000
.8000
                                 -5.0750
-4.5420
-4.7060
OUTLIT RAJIUS = 7.3335
            1-00033
                         DEVIATION ANGLE (DEGREES)
                                -5.1000
-4.2030
-4.5500
              .2000
              . +000
OUTLIT RAJIUS = 3.1919
            4-000RD
                         DEVIATION ANGLE (JEGREES)
              .2000
.4000
.8000
                                -5.3750
-5.7420
-6.5890
OUTLET RAJIUS = 3.5599
                         Diviation angle (Digress)
            4-000RD
                               -2.3250
-12.3300
-25.0850
              .2000
              .400C
```

Better The Court of the

45.2

Station	NCALC	NDA'!A	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	4	15	3

OUTLET RAJIUS = 7.5499 4-C00RU DEVIATION ANGLE (DEGREES) .2000 .4000 .8000 -5.1750 -5.4200 -4.7700 OUTLET RADIUS = 7.7343 M-COORD DEVIATION ANGLE (DEGREES) .2000 .4000 .8000 -5.0750 -4.5420 -4.7060 OUTLET RADIUS = 7.9335 GROOD-M DEVIATION ANGLE (DEGREES) .2000 .4000 .8000 -5.1000 -4.2030 -4.6500 OUTLET RAJIUS = 8.1919 H-C00R0 DEVIATION ANGLE (DEGREES) -5.3750 -5.7420 -6.5890 .2000 .4000 .8000 OUTLET RAJIUS = 8.6599 1-C00RD DEVIATION ANGLE (DEGREES)

> .2000 .4000 .8000

-5.3250 -12.3300 -25.0850

Test Point 301181015885

Station	NCALC	NDATA	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	4	15	Ó

```
OUTLET RADIUS = 7.5499
             Y-COORD
                          DEVIATION ANGLE (DEGREES)
               .2000
.4000
.8000
                                  -6.1750
-5.4200
-4.7700
OUTLET RADIUS = 7.7343
            M-COORD
                          DEVIATION ANGLE (DEGREES)
              .2000
                                 -5.4750
-4.5420
-4.7060
              .8000
OUTLET RADIUS = 7.9385
            1-00030
                         DEVIATION ANGLE (DEGREES)
              .2000
.4000
.8000
                                 -5.1000
-4.2030
-4.6500
OUTLET RADIUS = 3.1919
            M-COORD
                          DEVIATION ANGLE (DEGREES)
              .2000
.4000
.6000
                                 -5.3750
-5.7420
-6.5890
OUTLET RADIUS = 6.6699
            H-C00R0
                         DEVIATION ANGLE (DEGREES)
              .2000
.4000
.8000
                                -7.3250
-12.3300
-25.0850
```

**.** 

(4.1) TA

Station	NCALC	NDATA	NBL
5	2	15	0
6	2	15	ž
7	2	15	3
8	2	15	3
9	4	15	ŏ

OUTLET RADIUS = 7.5439 4-C000RD DEVIATION ANGLE (DEGREES) .2000 .4000 .8000 -6.1750 -5.4200 -4.7700 OUTLET KADIUS = 7.7343 M-COORU DEVIATION ANGLE (DEGREES) .2000 .4000 .8000 -5.4750 -4.5420 -4.7060 OUTLET RAJIUS = 7.9385 4-00020 DEVIATION ANGLE (DEGREES) .2000 .4000 .8000 -5.1000 -4.2030 -4.6500 OUTLET RAJIUS = 8.1319 1-C00ku DEVIATION ANGLE (DEGREES) .2000 .4000 .8000 -5.3750 -5.7420 -6.5890 JUTLET RAJIUS = 8.6699 M-COORD DEVIATION ANGLE (DEGREES) .2000 .4000 .8000 -7.3250 -12.3300 -25.0850

Test Point 301230515695

Station	NCALC	NDATA	NBL
5	2	15	0
6	2	15	0
7	2	15	3
8	2	15	3
9	4	15	Ō

```
OUTLET RAJIUS = 7.5493
            4-COORD DEVIATION ANGLE (DEGREES)
              .2000
.4000
.8000
                                -5.3750
-5.4200
-4.7700
OUTLET RADIUS = 7.7343
            1-COORJ
                        DEVIATION ANGLE (DEGREES)
              .2000
.4000
.8000
                                -4.6750
-4.5420
-4.7060
OUTLIT RAJIUS = 7.9385
            1-C00RD
                        DEVIATION ANGLE (DEGREES)
                                -4.5000
-4.2030
-4.6500
              .2000
              .4000
.3000
OUTLET RAJIUS = 8.1919
           4-C00R0
                        DEVIATION ANGLE (DEGREES)
              .2000
                                -4.5750
-5.7420
-6.5890
              4000
PECO.6 = SUICAR TELTUC
           4-000RD
                        DEVIATION ANGLE (DEGREES)
                              -6.5250
-12.3300
-25.0850
              . 2000
              .4000
.8000
```

Station 5	NCALC	NDATA	NBL
7	2	15	0
<b>b</b>	2	15	ñ
7	2	15	3
8	2	15	ž
9	Īi	±)	3
-	7	15	0

```
OUTLET RADIUS = 7.5+99
                          DEVIATION ANGLE (DEGRELS)
             1-000RU
               .2000
.4000
.3000
                                  -4.7640
-5.2750
-4.7700
OUTLET RADIUS = 7.7343
                          DEVIATION ANGLE (DEGREES)
             4-00020
               .2000
.4000
.8000
                                  -4.0730
-4.3750
-4.7060
OUTLET RAJIUS = 7.9385
            H-CUORU
                          DEVIATION ANGLE (DIGREES)
               .2000
                                 -3.9780
-4.1580
-4.6500
               .4600
.8000
OUTLET RADIUS = 8.1919
            M-COURD
                         DEVIATION ANGLE (DEGREES)
              .2000
.4000
.8000
                                 -3:9600
-5:5750
-6:5890
OUTLET RADIUS = 3.6699
            1-CJ0R3
                      DEVIATION ANGLE (DEGREES)
              .2002
                                -5.7160
-11.7500
-24.0850
              . 4500
. 8000
```

Station	NCALC	NDATA	NBL
5	2	15	3
6	2	15	ž
7	2	15	3
8	2	15	3
9	4	15	ŏ

OUTLET RADIUS = 8.1919
M-COORD DEVIATION AMGLE (DEGREES)

.2000 -5.3750 .4000 -5.7420 .8000 -6.5890

OUTLET RADIUS = 8.6599

M-COORD DEVIATION ANGLE (DEGREES)

.2000 -5.3250 .4000 -12.3300 .8000 -25.0850

# e. EXCEPTIONS TO SECTION 5 DATA (indicated by (5))

PSCALE = 1	<b>~</b>	PLOWER = 14.0	DAMP F = 5.0
DISTRIBUTE 1616		AGC SPECIFICATION DISTRIBUTION FACTOR	•NVEG•GGA GIM
12345 27 2901234 767	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	1.0000 1.0000 1.0000 1.0000 0.0000 0.0000 0.0000 1.0000	00000000000000000000000000000000000000
SOLUTIO:	1 2 3 3 0 0		11 12 13 14 15 16 17 -3 -5 J 0 -0 -0 -0

PSCALE = 1	.ə	PLOWER = 14.0	DAMP F = 5.0
DISTRIBUT	ED BLOCKAG	E SPECIFICATION	
STATION	BLOCKAGE	DISTRIBUTION FACTO	R MID ADD.CEVN.
42345078901234557	0.000000000000000000000000000000000000	1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
SOLUTION	TYPE INDIC	SATORS	
POITATE HOANN	1 2 3 -0		1 11 12 13 14 15 16 17 1 -0 -0 0 0 -0 -0 -0

PSCALE =	1.0	PLOWER = 14.0	DAMP F = 5.0
OISTRIBU	TED BLOCKA	GE SPECIFICATION	
STATION	3LOCKAGE	DISTRIBUTION FACTOR	MID ADD. DEVN.
12345678901234567	0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	-0.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000 -0.000
SOLUTION	TYPE INDI	CATORS	
STATION NHACH	1 2 3	+ 5 6 7 8 9 10 -0 0 0 -0 -0 -0 -0	11 12 13 14 15 16 17

5111101 ·

44401

PLOWER =  $\pm 2.5$  DAMP F = 5.0PSCALF = 2.5DISTRUBUTED BEACKAGE SPECIFICATION HID ALD. DEVN. STATE OF SECUNAGE DISTRIBUTION FACIOR 123 -0.000 -0.000 -0.000 .010 .010 .010 .010 -0.000 -0.000 -0.000 5 10 1123 -0.000 3 -1: -0.000 -0.000 SULUTION TYPU TIDIUMIDM3 STATE & West Point 21/0/1-15/50 DOMP F = 5.0 180014 - 35 1LDWE1 = 12.5

BLOTHING BUIKAGE SPECIFICATION STATE OF BEOCKAGE DISTRIBUTION FACTOR .NVIG. GUA CIM 1:3 -0.000 -0.000 -0.000 4 7 .010 010 K 301233 -0.000 -0.000 10000 15 1.0000 17 1.0500 SOLUTION TYPE INDICATORS

-

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```
PSCALE = 3.0
                          PLOWER = 12.0
                                                 DAMP F = 5.0
DISTRIBUTED BLOCKAGE SPECIFICATION
STATION BLOCKAGE
                      DISTRIBUTION FACTOR
                                                         .NVIG.UDA DIP
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           0.00000
                               1.0000
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1.0000
1.0000
                                                            -0.000
  14
  15
             .10000
                                                            -0.000
SOLUTION TYPE INDICATORS
STATION
```

```
PLOWER = 12.0 DAMP F = 5.0
PSCALE = 4.0
SISTRIBUTED CLOCKAGE SPLCIFICATION
STATION BLOCKASI DISTRIBUTION FACTOR
                                                         .NVIC.COA GIM
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            0.00003
                               1.0000
   1
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                               1.3000
   3
                                                             -0.000
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             .00301
            .0389
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  0961123
1123
                                                             -0.000
                                                             -0.000
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                               1.0000
  1+
                                                             -0.000
                                                             -0.000
                               1.0003
             .10000
             .11033
SULUTION TYPE 1 IDICATORS
              POITATE
N'AZA
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```
PLOWER = 12.9
                                                  DAMP F = 5.0
IJCALE = 4.0
JISTRIBUTLD BLOCKAGE SPLOIFICATION
STATILA BLOCKAGE DISTRIBUTION FACTOR
                                                          MIÙ ADU. JEVN.
                                                               -0.000
            0. 1521
9. 1521
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0. 15019
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1.3033
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   23
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                                 . 2000
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                                                               -0.000
   11
                                1.0000
  1.3
                                                               -0.000
                                                               -0.000
                                                               -0.000
                                1.0000
  14
                                1.0000
  12
  10
             . 10000
                                1.3000
              . 10000
                                 1.0101
                                                               -0.000
SULUTION TYPL INDIGATORS
             2 3 4 7 7 9 9 10 11 12 13 14 15 16 17 (-0 -) 1 1 -9 -0 -5 -0 -0 0 0 0 -0 -0 -0
PUTTATE
```

PSCALE = 4	.0		F	LOWER	= 12	.0			DAI	MP F	<b>=</b> 5.	0			
DISTRIBUT	reo ai	LOCK	IGE SP	ECIFI	CAT	ON									
VCITATE	3L00	KAGE	DIST	RIBUT	ION	FAC	TO	ર			MIO	A	0D	.DEI	/N.
12345678901234567		000000 000000 000000 00000 00000 00000 0000		1.	00000000000000000000000000000000000000							111111			
SOLUTION				S											
STATION NMACH	1 2	3 -0	4 5 -) 1	5 7 1 −0	- 8 - 0	-0	10 -0	11 -0	12	13	14 1		16	17 -0	

#### APPENDIX C

# ADDITIONAL CALCOMP PLOTTING ROUTINE LISTINGS

This appendix contains the program listing, for the SEVEL T and STAPLOT plotting routines. Section 11 southing the input format and program listing for DEVILOT. Section 12 contains the input format and program listing for STAPLOT.

#### SECTION C1. DEVPLOT PROGRAM

W. LEVPLY HARRY CANAGE SHARE

SMACE (IF HEROT /16)

In the following mant, the line corresponds to one card except whose meted. Values in parenthese tindicate the input format for the corresponding variable.

27 m. (1)	M 11W.1 (16)
172	) XY (W18) R (W10.8 ) Decurs (MCase Times
* (16)	and fifth frames frames
b. DEFINIT	ION F INPUT DATA LTEM.
ir va va ir m. , ,	Number of Pages (Speed Foliatr) to be flotted
III L A	Hotting option. NFLOT = 1, Hots will be made. NFLOT = 0, No plots will be made.
MEFAFI	Test Point Identification (Percent Design Speed)
	Number of Input Deviation Includes to be illusted for each Molecule. Includes Streamline Computing Station and Corresponding Deviation Angle)
17.77	Im-viation andle
783	Normalized Axial Distance
12	Radial Distance
1:	Computing Station Number Corresponding to Francili Calculations
<i></i>	Stronging Lumber Corresponding to Phase II Calculations

Preceding page blank

^{*} And the stime of previous line.

#### c. PROGRAM LISTING

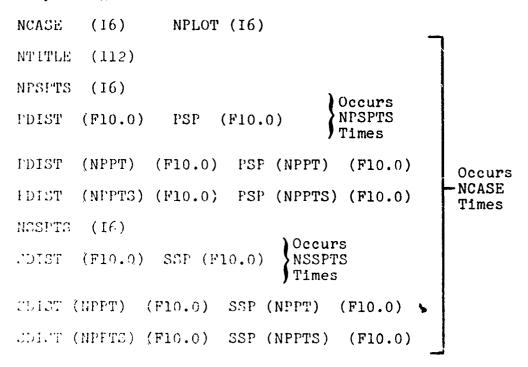
```
PROGRAM DEVPLOT (INPUT. OUTPUT. PLOT)
    UIMENSION D_VSGN(10,3),XX2(10,3),R(10,3),II(10,3),JJ(10,3)
    READ 10, NCASE, NPLOT
10 FORMAT (216)
    PRINT 20, NCASE, NPLOT
20 FORMAT (1H1,10%,25HRLFOR THRU-3LADE DEVIATION,//,10%,17HNUMBER OF
   1CASES =, [3, //, 10x, 7+NPLOT =, [2]
    M=1
 30 REAU 4J, NSPLED, NPOINTS
40 FORMAT (216)
    PRINT 50, NSPEED, NPDINTS
50 FORMAT (1H1,10X,12HTEST SPEED =,I-,1HX,//,10X,23HNUMBER OF JATA PO
   1INTS = , I3, /, 2X)
    READ 60, ((DEVSGN(I,J),XX2(I,J),R(I,J),II(I,J),JJ(I,J),J=1,3),I=1,6
   1)
60 FORMAT (3F12.8,2Io)
    PRINT 70
70 FURMAT(//,22X,10HNOKMALIZED,/,11X,7HSTATION,2X,14HAXIAL DISTANCE,1
   1X, 9HUEVIATION, 2X, 10HSTRLA 4LIN: , 3X, 6HRAJIUS, /, 2X)
    DO 00 J=1.3
    DO 80 I=1,5
 0.2 \times (I, I) = X \times (2(I, J) \times 2.0)
    DO 100 J=1,3
    00 100 I=1,0
    PRINT 30, II(I,J), XX2(I,J), 32VSGN(I,J),JJ(I,J),R(I,J)
 90 FORMAT (10X, 16, 3X, F10.2, +X, F10.4, 3X, Io, 3X, F10.4)
100 CUNTINUL
    IF (NPLOT. EQ. 0) GO TO 150
    CALL PLOT (0.0,-12,0,-3)
    CALL PLUT (3.0, 2.0, -3)
    CALL AXIS(0.,0.,2)HNOKHALIZED AXIAL DISTANCE,-25,5.,0.,0.,0.,.2)
    CALL AXIS(0.,0.,2.)HRUTUR INCIDENCE/DEVIATION,25,7.,90.,0.,5.)
    FPN=NSPLEJ .
    CALL NUMBER (3.0, 0.25, .25, FPN, 0., -1)
    CALL SYMBOL(1.0,6.2,.105,0,0.,-1)
    CALL SYMJUL(1.30,0.+5,.123,3HHU8,0.,3)
    CALL SYMBUL(1.0,6.1,.105,1,0.,-1)
    CALL SYMBOL (1.30,0.30,.125,3HMID,0.,3)
    CALL SYM30L(1.0,5.7,.105,2,0.,-1)
    CALL SYMBOL (1.30,5.05,.125,JHTIP,0.,3)
    DO 110 J=1.3
    XX2(7,J)=0.0
    4 \times 2(8, J) = 0.2
    DL VSGN (7, J) = 0.0
    DEVSGN(0, J) = 5.0
    L=J-1
110 CALL LINE(XX2(1,J), JEVSGN(1,J),6,1,1,L)
    CALL PLOT (8.,0.,-3)
```

150 CONTINUE
IF (M.EQ.NCASE) GO TO 170
M=M+1
GO TO 30
170 CONTINUE
CALL PLOTE
END

#### SECTION C2. STAPLOT PROGRAM

#### a. STAPLOT INPUT DATA FORMAT

In the following chart, one line corresponds to one card. Values in parentheses indicate the input format for the corresponding variable.



#### E. DEFINITION OF INFUT DATA ITEMS

NCASE Number of Test Point Cases to be run (Each requires a separate input data set).

NPLOT : Hotting Option. NPLOT = 1, Plots will be made. NPLOT = 0, No plots will be made.

Mallie 12 Dirit Test Point Identification Number for each NCACE.

NPSPTS Number of Pressure Surface Static Pressure Readings to be Input for each NCASE.

Chord Distance from Leading Edge (On chosen radium) of each Pressure Tap on Pressure surface.

PCP Pressure Surface Static Pressure at each PDIST.

SDIST Same as PDIST, except for Suction Surface Pressure Taps.

Suction Surface Static Pressure at each SDIST.

NSSPTS Same as NPSPTS except for Sustion Surface.

MPFT (NESFTS + 1) array Location for Starting Value of Static Pressure Amic (YAXIS).

MISITS + 1) Array Location Frescure/in value for Pressure Axic (YAXIS).

INSTITUTE (NSCFTS + 1) Same as NPPT.

MOFIG (NOSPTS + 2) Same as NPPTS.

1. 107 (NOTE) Starting Value of Percent Chord Axid (X AXIC).

For Month (TS) Fercent Chord (in value for X Axis.

FIGURE (N. T) Same an PDIST(NPFT).

PTICT(H 102)Came as PDICT(NPPTS)

EVERTURE . Structure Value of Static breakure Axia.

PSF(NPPTS) Pressure/in Value for Static Pressure Axis.

SSP(NPPT) Same as PSP (NPPT)

SSP(NPPTS) Same as PSP(NPPTS)

#### c. PROGRAM LISTING

```
PROGRAM STAPLOT(INPUT, OUTPUT, PLOT)
    DIMENSION PUIST(400), PSP(400), SSP(400), SDIST(400)
    READ 10, NCASE, NPLOT
10 FORMAT(2112)
    PRINT 20, NCASE, NPLOT
20 FORMAT (1H1,10x,31HSTATOR SURFACE STATIC PRESSURES,//, 9x,17HAUMBE
   ir of cases =, 13, //, 9x, 7 HNPLOT =, 13)
    I=1
30 READ 40, NTITLE
40 FORMAT (I12)
    PRINT 50.NTITLE
56 FORMAT (1H1, 1/, 20x, 18HTEST POINT NUMBER, 112)
    READ 60, NPSPTS
60 FORMAT (I12)
    J=NPSPTS+2
    READ 70, (PDIST(K), PSP(K), K=1, J)
 70 FURMAT 'F10.2,F10.3)
    DO 80 L-1, NPSPTS
80 POIST(L)=(((PDIST(L)-2.93)/1.795) *100.0)
    PRINT 30, (PUIST(K), PSP(K), K=1, NPSFTS)
 90 FORMAT (///,24x,22HSTATIC PRESSURE (PSIA),//,27x,16HPRESSURE SURFA
   1CE, //, 18x, 13HPERCENT CHORD, 10x, SHPRESSURE, //, (17x, F10.2, 11x, F10.3)
   2)
    READ 100.NSSPTS
100 FORMAT (112)
    J=NSSPTS+2
    READ 110, (SDIST(K), SSP(K), K=1,J)
110 FORMAT (2F10.3)
    DO 120 L=1, NSSPTS
120 SDIST(L)=(((SDIST(L)-2.93)/1.795)*100.0)
    PRINT 130, (SDIST(K), SSP(K), K=1, MSSPTS)
130 FORMAT(///,28x,15HSUCTION SURFACE,//,18x,13HPERGENT CHORD,10x,8HPR
   1ESSURE,//,(17X,F10.2,11X,F10.3))
    IF(1-NPL OT) 150,140,150
140 CONTINUE
    NPPT=NPS - TS+1
    NPPTS=NP ;PTS+2
    NSPT=NSSOTS+1
    NSPIS=NSSPTS+2
    CALL PLOT (0.0, -12.0, -3)
    CALL PLG((3.0,2.0,-3)
    CALL AXIS(0.,0.,13HPERCENT CHORD,-13,5.,0.,PDIST(NPPT),PDIST(NPPTS
   1))
    CALL AXI3(0.,0.,15HPRESSURE (PSIA),15,5.,90.,PSP(NPPT),PSP(NPPTS))
    CALL LINE (POIST, PSP, NPSPTS, 1, 1, 0)
    CALL LINE(SDIST, SSP, NSSPTS, 1, 1, 4)
    FPN=NTITLE
    CALL NUMBER (1.8,6.25,.2, FPN,0.,-1)
```

```
CALL SYMBOL(1.5,5.8,.105,0,0.,-1)
    CALL SYMBOL(1.8,5.74,.125,16HPRESSURE SURFACE,0.,16)
    CALL SYMBOL(1.5,5.48,.105,4,0.,-1)
    CALL SYMBOL (1.8,5.42,.125,15HSUCTION SURFACE,0.,15)
    CALL SYMBOL (1.5,5.16,.105,0,0.,-1)
    CALL SYMBOL(1.5,5.16, .105,4,0.,-1)
    CALL SYMBOL (1.8,5.18,.125,17HCALCULATED VALUES,0.,17)
    CALL SYMBOL (1.8,4.90,.125,24HLEADING & TRAILING EDGES,0.,24)
    CALL PLOT (6.,0.,-3)
150 CONTINUE
    IF (I-NCASE) 160, 170, 170
160 I=I+1
    GO TO 30
170 CONTINUE
    CALL PLOTE
    END
```

#### APPENDIX D

#### RAW EXPERIMENTAL DATA

This appendix presents a listing of the experimental data after being dumped from magnetic tape onto computer cards. The first two ten-character "words" of each test contain the test identification number.

```
0-0013756
                                                                                                                                                                                                                                                                    0-00E175E
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                                                                                  C+00103cE
                                                                                                  0+00003716
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                                                                                                                                                                                                                                   0-0076576
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0000000	+00209060000000012	+017821600000000022	+015425606000032	-004056
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2000000	+00294260000000013	+01158860000000023	+015756600000000033	-002543
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60000043	+002+6060000000013	+01178060000000023	+01562460000000033	-005263
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-00400	+015E54E0C0000032 +022354ECC0C00032 +022247EEC00032	+613228600000000022 +0190c660000000022 +019568600000000022	+002755c040000012 +00375150000000012	000000000000000000000000000000000000000
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+00209	+00211111100000000000000000000000000000	+0013/15000000000009 +002126e000000000009 +017/137660000000000	+0021 325 40 50 10 65 4 4 4 7 3 8 9 4 5 0 0 0 0 0 0 0 0 0 0 6 5 6 6 6 6 6 6 6	600000000 600000000 600000000
+00221	+002151600000000 +601557660000000	+ CG20%060000000000000000000000000000000000	+002218+00CCCOOCE +0021+7+000CCOOCE	000000000000000000000000000000000000000
+00228	+002208606000000000000000000000000000000	+00156560000000000 +002201600000000000	+002230600000000000000000000000000000000	000000000000000000000000000000000000000
+00204	+00210460C0000007 +6026476000000007	+062131600000000006 +8823460080800000	+0021366000000000000000000000000000000000	000000000000000000000000000000000000000
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+000970 +00140 +002273 +002137 +002332 +002332	+0022446 +0002446 +0002446 +0002469	1 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000000000000000000000000000000000000	0-0023206 0-0022686 0-0022756 0-0041376 0-0045176	1007284 1007284 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10064 10
+0C22696CC0C00006 +0C2266CC00000000 +0C2266CC00000007 +0C2266C000000007 +0023266000000000007	+0025776CC00000008 +0023106CC0C000008 +0023116CC000009 +0023866C00C00099	+01814066C0C0030 +0185726G4C600030 +018116FGGU000030 +0164326CC0000030 +016520600000030	+0156866CGGCGGG31 +0156786CGGCGGG31 +0156CGGCGCGGGG31 +0156116CGGGGG32 +0215516GGGGGG32 +0215516GGGGGGG32	0+0223546600000325 6+0221146CC0C0000327 0+0225186C00000329 0+0221086CC00000331 0+0215066C00C000335	+0223496CCCC000334+014133CCCC000034+014133CCC0000034+0371556CC0C00034+0371556CC0C00034+0553556CC0C00034
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60000005 60000005 600000005 600000005 600000005	00000000000000000000000000000000000000		00000041 00000041 00000041 00000041	06600000423 00000000425 00000000425 0600000429 0606000431	\$10000000 \$10000000 \$10000000 \$100000000

12ST I.L. NUMLER 212070314770

8 0+0009706	0+00230+	0+002171	0+002316	0+002547	0+002257	0+005446	0+003++1	0+002181	6+002354	0-007256	0-007297	0-000+47	0-005881	0-005921	0-002425	0-002444	6-032346	0-002311	C-302238	6-002314	0-002377	0-002335	0-002309	0-002252	D-00+3+3	0-002892	719400-0	0-003130	0-004193	252200-0	0-007251	0-000355	0+0062B3	
0+002300€CUCOSOO05 0-000123cCCOCOSOO5	+0054306 (0000000	+0022526010000000	+0022616660600000	+00536566000000000	+00052206000000	+00533460000000	+3021134600000000	+60246866000000	+0025356000000000	+016143660060003	+016551660060003	+018120606060003	+01641260000003	+015561660000003	+015510 c C J O C D D D D D D D	+61588346546506003	+015556600000003	+015605603000003	+015617664060603	+021538666060003	+0211216030000003	+0216016666600003	+02133560000000003	+021767666066003	+021322600060003	+62042666600003	+CZ1116ECCGCCCCC	+0216356666000003	+021633603060303	+018157 + 00 00003	+01815866000003	+037165663000003	+05526566606003	
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0000000212	00000000	30000000	20000003	5000000	2000000	00000000	00000000	60000000	00000000	60000000	000000000000000000000000000000000000000	0.000000	00000000	0000000	07000000	0000000	000000	00000041	6000003	C0000001	0000000	000000	0000000000	0000000	000000	0000000	2+000000	0000000	0000000	27000000	77000000	77000000	00000044	******

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+006551	+0555726 CC0C00034	+0537c2c0000000000+	+007237603606001+	**000393
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-0072±1	+016154 (00000004	+017305000000000000	+00-112-000000014	000000000000000000000000000000000000000
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# 1 A C C C C	+0215331.00000033	+01+335+00000000000	+00+5210406660013	693983+3
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TEST I.L. NUMBER 212070715670

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+000946	000568660000000000000000000000000000000	+0022-10000033005	,0715-700303C30.	0000000



0-000123E 1-007 296t 0-0025756 3-3072526 0+0025236 C+002533c 3502200+0 0-6047726 -0047256 シーのの2をほどぎ 3-002332E 0-0023306 3-0022c4c 1-0022366 5+003765t -1072016 0+0022576 0+0025046 0+002203E 0-0072564 3-0024364 -0022726 0-0021346 3-0322.16 2005 3-84886-1 1-0023336 1-003203E 0+0062516 -005 104£ 3-002 3+0+5 E-0001301 CCUC030052 6+00256360160040066 0+0155312000000315 0+025217cCS0C060323 0+0244674606030333 0+0247544660000335 0+02>127<ft>05000339 0+0022036C30u000007+ 0+66261166600000000 0+00000000001×622000+0 0+062258656650000098 8+5213476 [ 5 0 5 0 0 0 0 3 1 1 0+02127~6€€0€0000323 0+6276301030103010352 0+054650+C1546000357 0+0242616698000331 0+0023434060000034 0+01614466660000301 0+0216581 01666008321 0+079788661060003+7 0+69337866866000347 0+02511266.00000337 0+0787:766?066303+3 0+06227355500007 0+0159366000100031 C+015EE7tCC0C0631 0+017031460000030 0+01 8122 cc c c c c 3 10 3 3 0+0154486640000030 0+0211994666000030 0+61536 FL 606105031 0+03715860000004 C+0<1137<00000000023 £+00530000+52500+3 C+3822364888688888 C+C17308006000000215 C+617376600000000217 4+0174466 406000000219 L+61-739F 0000u60223 0-000125-000000000051 .+002533600000000000000 -+ 0021:1:7:0:000000000 [+017235f9u000c0201 C+01c217 L W00 U0 0 0 2 0 3 C+012530c600000000007 C+015277+000000000213 C+615024600000000821 6+621359c0000000227 C+013932403000000233 C+0182+2c00000000023> C+015507600000000037 C+013339c 06000000233 0+0173116000000000241 [+017311£0400000244 C+60226960300000000000077 C+362+0966969696861 C+005411-000000000000 C+C17278F.0000160265 C+01>114E000000000211 C+C11131E00000060231 :+02035cc0000nn035; 0+653765600000000024 0+600010-0906600660 0+002-5% cd000000000 0+00372269965600163 0+063070000000000000 4-397777467066666664 0+002327 c00 300000063 0+0025:349366639656 0+9030 11690 36600107 0+00477563006100103 8+86597450066600113 0+40523479896638348 0+uŭ> >+1r300Cd00117 0+00443344966669114 0+00534769986698435 0+000015500560015F 0+00021253400533145 0+667237+9066600147 070015276333333350000 2736033066777777 9+002235500000000000 3+372-+250006603684 0+500:21313000000010 0+u6+5+:+300Cf00111 0+00-+03-63600000551 **]+U**C+><1rd][CCull2 0+00+5c3e00000€00131 6+19036908411-19049 3530939366728475946 UF9615 13 5 3 5 3 9 9 9 0 C 9 9 1 0 1 0+844+10c00CCC001E7 0+39-81+63366630141 0+80.0 + 100030000121 0+403775+40966140457 0+0140J2c 0000160413 45.000.0042.4 0000000000 F ? + 0000990 2+700000000 5406000000 1.100JuS3c3 0000000000 3000000000 5 60 60 00 00 n n 00000000 30-000000 60-000000000 0606969413 3506308415 6206003076 34000000 4500000000 0.0000437 24+0000707 4 + 40 0 0 0 5 0 0 0 4 6 6 6 6 6 9 4 6 7 3600303-11 1440000000 1000000000 0600000000 00000000 3660360-17 3.00003.421 3.6000016 **3**₹00000*5% 85683333431

TEST I.U. NUMBER 212070916170

+ + + + + + + + + + + + + + + + + + +
+0025/76000000000000000000000000000000000000
. 4 11 11 11 11 11 11 11 11 11 11 11 11 1

TEST 1.0. NUPBER 212071015080

+000952 -000126 +0031c6 +002922 +005127	+003455 +003036 +003272 +002446 +0025446	-007297 -007297 -005697 -006974		0-001776 0-0012316 0-0012316 0-0039136 0-0034166 0-0072926 0-0072926
+0036476CC00000006 +0001296CC0000006 +0034276C00000006 +003626CC00000000000000000000000000000000	+0031666CJCO00007 +0034656DJCJDJDGA +6031436CBGJDDO3 +0026296CJQDQQQG +0032846CCQCQQQQG	+0181456000000000000000000000000000000000000	+615476ccggcbggg +015373c66000031 +01526+66600031 +015256cc600031 +02305260000032 +023469600000032 +02346960000032	0+023690600000331 0+02339540000003331 0+02233940000003331 0+022317400000003331 0+02234566000000337 0+018199600000341 0+037179600000343
+003058e0000000006 +00012560000000000 +0035560000000000 +00307150000000006 -00195860000000000	+00235060000000000 +0313660000000000 +0028586000000000 +0033276000000000 +0028016000000000	+01723760000000000 +015904600000000000 +01726860000000000 +014154C0000000000 +01449160000000000	+01454050000000001 +01495760000000021 +01752560000000021 +019817 -0000000022 +020317 -0000000022 +0202416000000022	C+02241960000000234 0+01504600000000234 0+0140662600000000235 C+01458060000000235 C+01731160000000241 0+017311600000000241 0+03591460000000245
71015330006600000066 +00003960000000066 -0330350000000006 +03031600000006	+003331600000000007 +00365060000000008 +0034306000000008 +002977600000000 +003259600000000	F001-773000000000000000000000000000000000	+0034966000660011 +0057206030000011 +002857600060011 +0058516000600011 +0034546000600012 +0057316000600012	0+00-94160000000139 0+00-94160000000131 0+004-95-0000000133 0+005-9360000000135 0+005-05-0000000135 0+004711600000000141 0+00029160000000143 0+0072906000000143
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TaST 1.4. NUPRER 212071315080

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**********	+0072326303060014	+053733600000000004	+6554056660600034	^006259
******	+01+013			

C+303216E 0-0072596 0-03u8c2c C+0032766 0+003029¢ にゅこの このよかり 0-00-611c 3624000-0 1-000177E 0-0003576 6+0033E& 0-0372336 0-03-6416 0-0000-1 **0-000615**6 6-1000:28E 0-0003+26 U-0013+2c C- 1100 35 36 0-0002,26 -0027206 6-0414036 J-003377t 0-0027:3t 0-0072546 0-0011636 9+62/00-0 J+00625è6 2+8400+0 3+005 0+003C3+6CC0C0C000034 0-00016546806000002 0+0034cffc000000066 0~00367446386930070 0+C031634CC0C0000086 0+0025076 6366030033 0+16528tt 6606000034 0+0031176600000000000 0+0162596 0000003030 0+01=3146666000319 0+02+775€6000000335 0+02525866060000339 0+00053446600000040 3+003131c6560010078 0+01914666660000301 0+01-06666390030307 0+61555666666000313 0+02253146600000323 0+02:271eCCC6000537 0+03717446000000345 0+6554016666300347 0+0035+0+01000000082 0+618597£ CC000000311 0+01525160000000317 0+012+35<600000333 0+016157cc6666430343 0+624559466660603331 C+01316660060003+1 0+0167356660000030 0+6141176.660666030 0+0256 > 6 & 6 & 6 & 6 & 30 32 3 0+0251384666606032 0+02453656566000032 0+01537260000001 0+8234+640000032 L+01533560698660203 3+01-174E 00000000003 [+014546600000000233 0+62332860660668223 C+61833500000000335 C+ C17051c0000000033 £+603030466000060357 L-0001996000000000000 1+603030e06000660000 C+CO313+c000000C00C0063 C+00293J÷000000000077 C+6632255e0600006041 C+003 31 95000000000000 L+6032+1c060000000 [+61/257e06000cu201 C+0172,766000000000000 C+015251c000000CC207 C+01++33600000000011 C+01+973c006003021J 1+01-875-0000000000221 0+5252314000000000553 +6223756000000303227 1+01051860006066231 :+C11+3UL00000000233 0+617310-00000000241 C+353791600000000000C+7 10+8173056010001106243 :+61c5>1e608e38353 [+03591260000000024 . **90000000000000** = 6200+3 C+C1/830600CU0000Z1 C+017525600000000021 C+025+3+c600000022 U71415>4000CCc00Cc 0+000311600065030c J-831550e033000000 6+16312169308630664 65106313000+6+00+0 0+16233caaaacaac3 0+0633>+00006606675 u+00s71st006oC00tc86 +500300 C -+ /5000+0 3+003111e3986C006e3 0+063314500C3C3C300C5 9+65>01363030566656 0F001J743000CC001C1 +30+21553336500153 0+60+27203366603163 0+0037>160006690167 9+30 >1 >50 2003 8 9 9 9 9 9 9 9 9 9 9 0+00+72/6000600111 0+5039-3-0069650113 u+u601_+: 330960911= U+9055766936668117 0+00+7+264164630181 0+00-0-3603506015-0+465 4576346569333 7+03>6:6c306CC00135 +8(: 02367354643141 1+6012 33600 666001143 0+00023260060600148 +06,72,55006660001+7 +00+612c000CC06137 0+00.312-00000000012. 3146360664172600+6 0+00371000000000 1+002+7-0-03636301 0+01+015c 360c 13935 3 £0+0n(nn3 1000000000 7+4010330 500000000000 6000000413 6600000000 504000000 3600000-13 22-001000 190303433 000000-33 ********** 2604969072 ยือบูชิธ์อยู่คง .60300687 00000011 0000000 60015042 000000000000 16000000000 **/**0+0000110 9 C 0 9 3 0 0 0 c 7 1000000 500000000 0-0000000 0.00000000 5-06.000 00000000000 54636343 366639942

TEST 1.3. 10*40x 21207191940

3234800+0 6-0001116 0-0003326 0+003226E 0-0072986 3-007298t 3-000+12¢ 0-0003226 0-0002646 3-006156c 6-0023376 3-002841t 0-0072546 1-0003506 C+0034316 99110040 0+0030786 C+0328686 3-0044636 3-00+066**t** 0-00409-0 2-000920E 0-000836E 3-000£13£ **)-0000116** 0-0003426 0-0006706 0-0021486 0-0072546 3526000-9 0+0062386 0-60069746606000062 420000000033225C0040 0+1052546 60660400090 +60000000533252E00+8 0+10364166600000088 0+0265526000000335 0+0276346600000339 0+03717460000000345 0+00046366000000000 0+605659603060306076 0+603151660000000076 0+00256766300000082 0+00515666600000086 0+02253260000000323 0+0255446000000325 0+0260234 C00C000333 U+026540£Ci00000337 0+055401600000347 U+6167+468JD60J03D3 0+01416060606000343 0+018166666000000341 0+62122346600000011 0+02e7556CC0C00**00327** 0+0267/35(606000331 0+6131166 C00000030 0+0161626660604030 0+021054466000030 0+0154154000001 0+015324600000331 0+015254666000031 0+0271756600000032 C-0000326600000000001 (+0031216000000000000 [+00313363000065043 :+003315c000000000055 T+00291466000000000000 +01593550000000000000 .+01-5-2-0000J60211 (+01-j-ce00000000111 0+6223144 666 000 0225 C+0137486000000000239 :+017313000000000243 (+035310600000005<del>4</del>5 (+005334c600000000000 C+302972504603000677 .+C1723960000000000001 C+617270603000000863 [+61-1:1=000000000000 +620838600000000223 1+6228+30600000000227 +01>911c000000000233 1+01347760000000000233 .+663253606066066697 1+01/03840666006217 +0174726000000000217 .+017>3>6000000000213 1+01+3556000000000221 :+6**2**2474€00000030223 0+0106586000000000031 :+017313c0000000002+1 (+60321366600006001 +61525360000000000000 [+[1:3909e00000000002**3**] +30.21150990500103 0715155533000000055 0+903019690000000000 0-08J379cJJ0cCu0fc4 0+0031-269969696 +402931-90000000072 0+06332+10103630-76 +003m32e0303C33C3 0+667352513996600064 0+00523460300000088 1+602-1163700636111 1+00-+6960106690113 1+86×6+c630000000119 **]+80**7756930860**01**23 3+004710600 CCC00133 +00575763060630135 +000233600000000143 3+0062±3630066600145 +007290=00000147 0+05; 0:063300003000 Fu012 > 230666000161 0+10+00+01010101001105 1+00. 7 54600 CCC13165 0+00554869106650115 u+904.37760306:00117 1+06/130600000000001+1 **)+00>3**,3c0à00C0ù652 +06-+30-00606001167 0+00>>3653304600121 + 100>7 326 136 6 600 131 +88,110,886,60,000,35 1+10+5/363066600127 +60+3+3c0366660137 +00+>1360000000015 +0010193001151115 3+01-011 0600000-15 000000425 00000000423 F 5000C0000 62000000000 0600000000 66000000000 20-00000000 20+0000000 0.600.300-07 **でつりつつつつりつ** 000000111 00000013 0600000-13 000000423 25-6000000 000000000000 0096999433 00000000000 0000000000 000000000 160000000 0000000421 2000000000 /++ G000000 9.90360057 000000000 000000000 00000000000 90000000 ัชถาดถาดจะ 7000000. 10000010 ** NO00000

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0+00e795 0+0036334 0+0028720 2+1139436 0+0326,36 3+00+80+0 3+03-5056 C+034721E 325720041 1+6020+36 0+008 3-36 0+0038+2c 3++8503+16 0+00,9516 0+1003116 1+39<u>80</u>3+1 2+83+800+ 3+03cc1+c 0+0137tof C+0355736 0+497979+26 0+005-055 0+0327 **JFU017** 2+5+0 0+00+340+CCCC00003× £6+06600077775700+0 0-000002600000000000 1+10148166766380419 0-0004-0-0-07000033 U+06473+6660c030037 0+0070360360300035 0+30+6556666030039 0-00727066366636+31 1-005-57-60000000431 0-000074600000437 U-067271+5365090441 0+000-0-10000000+1 1+000a0010100a00a0 0+0000-4-6036-030+21 |2+000030||13||14||15||00000 6+60%16+666688888 0+0045+846?6603040 6+6661° + < C66606041 0+1666314671600942 0-6035436666600043 0+6044251135600007 0+00447260130000007 0+60-5246500000 0-005111 C. C. C. 000-1 0+66313866030633041 0+1007354706633042 0+0001775555003045 0-06/271cEJBC030++ **00033307023000+0 (+00-5--601000-608-6 54613334400000000362 C+63333466600086847 236000000031120001+0 C+++02>2>25.69000 . Euro 6+03+4124000000000073 L+36-734E608030E074 0+10-1705000000000000 #\$80°090071/2×*00+3 0+00-477+000066634 1+11+47340000000000000 -0-3000000 FZ + 310+3 C+010547600000000011 1+113022C000codo21s 0+010033+600010+315 1+*12 1380 660 60 6517 C+021215-000C00339 C+037032000000000000000 0+16+57 or 888883607+ 0+5620-3-7-066000003-5 2+3157.6+6809940307 r+112 /255000000000000011 [+6215256000066354 565550000000-4-655140 7+6240,74600000333 1+82150550000300337 C+01-11900000000000001 1+31-013-6666030301 +021+33660000066321 _+6253571856000003277 C+62132>+8u660696331 [+3212-1-660035632 ñ+5211.cc9učí603724 1504153559396600657 794763763736666666 +01%5 + 36 00 00 000 35 + 34 10+ 0+61+37+.00000000253 J+31, 550,000 CCC 35643 u+3000230634060300c1 0+30m++1540mc630673 カチンひこうシャピ フリひじらごりょうち 1446-1245138CC0665 2+41,0+1,43,36193261 0+61744450366636665 512000001846 3+TC+0 +0220,4403005000664 54512134609665000456 8437 -1 4.33766690arv にくつかいりゅうのついろく さらじょう 0+90-712c330CC00.31 0+61431264336434677 +5155 - 16 0 16 6 6 0 6 2 6 5 0+0100136000000011 +41-51-51-00 35 60 65 15 0+61, 2<1 013F033c1. 0+010-0-0-00-0-0-0-0 3+42272-1336669625 0+01s1 .>ru7CcC03231 -01761616 8+6135 .4cJ966600237 3+617051-900000000 U+03.730f190f68974s 0+7232726Ju0660066 4 0 C + 0 Jududy Joe 0486336134 6515111111 0.0000000 300000000000 3000000000 9606469133 0000010111 ปียีปียีปียีปี 115 0640333113 5676673336 1210000000 100000100 1660390151 000600134 JC JC JC JC JC 3 CC063630c~ 3006938--2-062230 0609301161 000000113 3.0000331. 3667703145 36003001-7 9966000117 3001333121 0000100131 3000000000 Tottone of 9604079 563030011

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3662500+0 DF 0017393 0+00+8836 0+0047256 0+00+7656 1+0061356 0+0006646 0+0049116 3+0071116 3+0043666 0+0005526 3658 400+3 **1+0063256** 0+002 404E 3559400+0 3+0044366 0+0061756 0+002 4276 359**00+0 **3+00+3**516 0+00000000 0+00635+E 0+00+033 0+024511 3+006817 0+00+189( 0+0071+3 9+00+0 0+00124246000000099 0+0006636000000000 0+00472460000000000 0-0000746000000413 0-0016666000000439 0+004442460060000071 C+0045036000000000000 0+00%66246606000003 0-0000240600000411 0+0006526660000425 0-000250660000000437 0-00121465000000000 0+0003736C00C000**0**421 0+00073540000000**0**427 0-001629660000**0043**1 0+0049766000000007 0-003510603000000040 0+000564466060000+0 0+0002006000000000000 0+000052500000000045 0-005256650000043 6+004500€000000000053 C+01293660000000119 0+604333£0000000007+ C+00+3136060000000094 1+01393260000000315 0+000652-00000000000000 0+00510+000000000000 C+00~62~60000000000073 C+00>1+3c00000000062 C+6044116000600000090 0+61-02060000000301 0+01+449666000066303 C+015970c00000000305 C+0137906000000000000  $0 + 01 \times 230 \times 0000000000311$ 0+01301960000000013 [+61292660600000317 [+020516600000000323 C+0251-360000000325 [+025035600000000331 C+02408~£000000000333 [+02+735E000000000335 [+025305~00000000033** 0+0252916000000000333 0+0219+96000000000321 0+02>011600000000327 C+025514600000000032; C+0177756000000000000 101010045906969657 u+01+37-60366630213 0+017353500000000219 0+6211-1164966600883 0+00>222500000000c +60++60e0306500073 +3043~~~00666666 0+015>7060000000000 0+01456360000090607 0+01350360033600500 0+0139+660000C00211 0+622537530606000255 +02275960066600283 0+0184+05000500000000 **3+8000540090000000000** 0+06474060060000661 1+00451960003148665 0+0170~56000uc00201 0+01/0020000000000000 +01726360000000017 0+013325=00600000221 +023235=0000000000257 +0103546000000000331 0+01+00+00+00000000000 0+61795560006600637 0+60+37 +6000u0000077 /5168818688842<del>+</del>868884 0+00+5,0cn000c00ce 0+0178216306660023 0+0143476300668021 +900000000 0.00000000 + 60000000 3000000033 260000000 000000123 FE10600000 10000000000 00000000000 6000000000 666663372 000000000000000 ~50060000 000000103 000000107 01000000 000000113 000000115 000000113 000000123 3000333133 0600000135 000000 00000111 0000000000 00000117 000000121 000000123 600000127 00000000 0000000

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W. 4.70 0+0057486 0+0051226 **نه** ده 1+0379636 0+0338506 0+0054976 0+0058976 0+0332846 3+0327746 1+0346516 1+0385236 1+0350276 0+00515+E 0+0385036 0+034279E 0+0373446 C.+037 5826 C+6338656 0+0343566 C+037500E 1+0327036 0+0380356 3+3341786 1+0355636 3+0380946 0+042703c 0+006027 1+05020+0 3405×30+0 3+028865 0F1015 1+0347 0+0000000325450000003 0+00557766360000067 0+00;3476660000000 C+COC352EC0000000+0 32436660000433 9+610178ECCCC000433 0+6112336 [ 000000437 0+0023766 CC0C000031 0+012215EC00C060411 0+00825 66 [ 0000000431 0+66511866600000000000 0+01345060000000000 0-00365766606000441 0+0025546 [60600003. 0+00033586500500040 0+0025616[[0000000] 0+6102046660600041 0+0066610000043 0+074468660000044 0+006625600000000 6060000033473613+0 0+000+00030313922400+0 0+011126666000041 0+0125356 CC 0 C 0 0 0 0 4 1 617666600042 0+00032160300000044 0+0005454660000044 0+0052646600000007 0+0120534060C000+1 0+011140€000000042 2+00010334277000+3 540+0 0+012 +00c072r9000000000 +60,3,46,660000000000 + CO.732 c 0000 J C 00 B 2 +6043376000000000000 +605-13600000000009+ +61+331+6000000030+ :+012378£0600060313 +0240036000000333 +002395400000000000 + 6051:760000000003: C+01c230c00000000001 +61432160060000383 +01622560000006303 [+013417E0000000307 +6145254060066311 +001647c0000000315 [+0063596000000000313 1+02,443600000000325 [+12c+386000000000324 (+ UZ = 3 : Z = 000000000333 +00:27360000000030341 +635235600000000345 1+69322760000000347 +01213060000000017 C+62: 3286 66000000321 [+C2306v60000006323 1+32:333600000000327 .+C2::9226.00006C0331 +0247%+660000666337 .+(2{501606006C337 C+00:2-160000000000 0+0123,3693000000203 0+0130-5-0700000013 0+111-014-00000000015 3+317771c00c0cc021g 0+100007440006600001 0+00.111E09CCC40673 0+00-1-56000000000077 0+16-16-72-4609646000199 0+0010046466666666 0+00-1,3600000000000 0+01/33500000000000000 0+51:4.86000000000000 532003330C 14. 8LFC+0 0+11+43340062600267 0+0133"7630GCC30211 0+023553639900005253 0+32-19163000000255 0+02-038500CCC00256 0+U11+/je306CE0623 3270011300546241040 0+01>2500000005240+0 0+03c03cc000CC002+5 0+00:1 12:030003000 0+36,5775000000000 U+00+32430 CCC00Ccc 1+420+17-000CC09221 8+42+444440966600654 0+31>+14>136600643 0+36,621+3066606241 7+300333600055E856+6 0+0102+7c0ufff60023 0+01+73>60066606655 0+30.231c360000000 3+6165+56000CC0021 100010000 22000000000 ~ 200nn 003v 0000100083 00000n0 0010000000 9546050034 ************ 5 P J D D D D D D D D 3699863163 000000113 3663060123 **3600360101** 3003000107 000000111 00000153 000000152 7000000127 3000000135 0600000133 3669659121 3000000133 0000000137 000000141 00000011 00000011 00000000 060000014 30000011 CC0000014

TEST I.C. NUPBER 3(1231615700

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+038029 +035535	+011C21EGG0000043 +006520EGCGC00043	+02725560000000033 +027317600000000033	+01> > > 2600 CO CO CO CO CO CO CO CO CO CO CO CO CO	00000013 Cu000013
+033266	+00664560000043	+02555360000000033	#2000000000000000000000000000000000000	21000000
+034789 +038638	+6031926660000043 +0183676600000043	+0269:760000000033 +0244:860000000033	+010+>2600000000023 +6137545000000000	0000013
+034656	+012256660000000	+027 3036 600 00 6032	+0261126000CC0022	C000000
+038058	+01345060000045	+0259196000000032	+02493060000000025	60000012
+0330%	+0123246000000042	+0266356000000032	+02+2+76000600022	00000012
+037703	+015676466666645	+023025E00000000032	+02351960060600025	0000012
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+034577	+00+672600000000	+015446600000000000	+01302960000000020	00000000
+038438	+004624650000000000	+013443600000000000	+01+6236000000000	0.000000
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+021030	+00000303366000000000000000000000000000	+005608600000000000+	+000000000000000+	60000000
+005245	+0000000000000000+	+004901600000000000+	+0026360000000000	00000000
+002134	+00536260100000000	+0024216000000000000000000000000000000000	+0043+260000000000	80000000
PPD 9DD+	+6C55E3E(60C03007	+ CC5338	+00511560000000000	
+005732	+00000000122500+	+002027600000000007	+102303000000000000+	00000000
550 COO+	+CC51C56CC000007	+005353600000000000	+0072246000000000	000000000000000000000000000000000000000
+002485	+0000000000455500+	+00607360000000000	+006.1736000000000	60000000
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0+0381216 **3+006171E** +0385316 0+0326986 +0336566 0+0376996 0+0322396 0+0331186 +03+00% F0020241 +006356 304400+0 +033169 +036268 +032169 005500+3 +037221 0+038740 1+033246 403204 1 336232 +032363 0+042288 1+002346 +0000345 +034018 +017780 0+0000016 CC 00000063 0+005624600000000067 0+005370€0000000071 0+0051766660000000000 0+007044600000400 0+01071566600000413 0+0130756 6006000425 0+01447560000000447 0+00555660000000000 0+002230600000000000 0+0026016660000000000 0+0752866000000472 0+61186669000000417 0+013618666900000418 0+01584066666666666888 0+00632060000000000 0+0026286600000000000 0+0126026660000411 0+014218666060000427 0+000663606060000437 0+07866666000000000000 0+0044446600000448 7-003511660000000441 0+0115666000000000421 0+011623600000000437 0+0046176000000040 0+07724260000000045 0+0055106000000000 0+00211360000000000 ***************** 0+0000795000000000000 0+0033576600000000058 [+005271E0000000007+ 0+005697600000000078 C+006a776000000000082 0+00496060000000000000 C+006297€00000000066 C+00563360000000000066 0+014322660000000000 [+016361600000000305 C+0127636000000000000 [+01236160000000313 6+023580600000000335 E+C3543563000000345 C+0024286000000000000 C+016407600000000000 C+013417600000000307 C+012979600000000311 C+612394600000000315 C+012105600000000317 C+012233600000000013 C+02549264000000000321 C+023474600000000323 0+02474060000000325 C+023883£0000000327 0+0223796000000000329 6+022814600000000333 C+021/4/600000000033/ C+0248+4600**0**000000339 :+017318600000000043 C+05366160000000347 [+024485600**000**00331 0+0025436000000000347 0+0064266000000000065 0+002+63600000000068 0+0053166000000000003 0+00511760000000000 0+01745160006000205 0+01291750006600269 0+014309600000000215 0+017924500001000219 0+023551600000000223 0+0246326000000000255 24081530200000000057 0+000001600000000061 0+0003396000000000 0+00575460006600061 0+0,0>25360000000000 +8052066000000000057 1+017502600000000201 +01245166466666666 0+0145666000000000000 0+01329460006600611 0+013622600000000213 0+016537600000000217 0+02061460006600621 0+0254266000000000237 0+02603460000000223 12200111009296600+0 0+01307360006600235 0+0136526000000000 0+00657460000000000241 0+018398600000000243 0+0361536000000000 0+0129616000000000237 00000000 00000000 090000000 49000000 00000000 2600000000 9600000000 601000000 0 90 0 0 0 0 0 0 **1900000000** 600000000 0000000000 0000000113 000000115 000000125 00000000000000 0000000117 000000123 00000135 000000000 000000000 00000101 000000000 0000000121 000000158 000000000 000000000 000000143 000000121 000000131 000000137 040000044

NUMBER 301240015302

TEST 1.0.

SEPTION MOMERT OFFEROMENCE

3+01c355E F0020303 0+035002E 0+0330c06 6+9347±5E 0+03+4656 C+0457276 0+00+1636 3334.00+3 0+03×132E 1+0325336 0+0367676 C+03+14+6 0+0346756 0+037e376 0+630213c 0+03+0+36 0+0330716 1+038241 0+036821E 0+0332156 G+038222c 0+03535BE 3+0241326 0+0425716 360+3 +00% 000+0 753+0 0+6066746660000063 0+005597663000000075 0+60621760000000079 0+00245666606000093 0+00523666000000000 560000000003338350040 0+00000001600000+03 0+0031+166.06000405 0+00033746.0000000407 60400010333655400+0 0+0107226 6 6 6 6 6 0 0 0 4 1 3 0+0126644666000423 0+6166276656000433 0+0053846 (00000000) 0+6003316 (000030401 0+0127154 600000011 0+00655466601000433 0+00535916506000071 0+61176366666000417 0+61157056666000421 0+00000678660000000000000 0-0025136630000000++1 0+N142+7EGGGCGJG427 0+008645<6000000431 0+811667660000000437 0+[1266760000041 0+015554666000045 0+013732109999941 0+C13435+C160000+2 0+6067626660600043 1+06.23760000600060 C+00>50+6000000000073 C+005573500000CGG7. +905944606000000000 +007635600000000356 +C02334 0060060094 +600000000011100+ C+61c+04c00000000301 C+014316600000000303 +615034663000000309 +61527560000000311 [+612351£0000000313 C+01215360000000010317 0+012232500000000013 [+6234+0000000000323 C+C2. 9:56 C+00000632 [+62753260300000032× +02505960000000333 +62231460000666335 +027557600000000353 0+03542560000000345 C+65565760000000347 C+0134+><0000000000307 L+E2.935600000000321 1+02c1 > 56038008 0327 +0275 18 00000000337 +0652416000000000341 +01635560000000030. C+612+316060006031, [+027030€00000000331 24491333665635169945 0+41733363366600219 0+3669.3000000000000000 6+345+1463936634645 0+00: ~ . ~ 6906 C 69669 3+90> 310+0066600653 6+3053346996609677 3+60.1170006300cs 0+0173016006600661 0+012 +00000000000000 0+017+:3600000000265 0+31+61464006600207 0+012 3>303306100263 0+01335569066600213 0+01+36060000000015 0+31c+7c600CCC00217 J+0247306010000001 0+023031600000000323 3+72-55503066630625 0+62.1.38-000F1036239 0+013>1460000000233 U+v10053cd00CC00235 0+06*~* >04~006C00Ce1 U+025357t0JCC6U6227 0+01003760006600631 8+111-4J46J0CCC0J23E 0+00057363006600641 3+8371+361100600245 **0+05+0356000000000** 3+30>++7.9039639063 0+00×329e0900C0066 0+3452935906660065 0+61,3356390660024 0+0133548 0306000 2600000000 0010010000 9956010969 ~~0(.6668) 8506300030 4.10000000 0.00169123 000001133 3.06300132 64336308+ 2F(10000000 000000000 100000000 0.00000103 000000111 6660333113 000001117 000000121 060000137 1600303147 0.600000131 1300000141 0.0003312 01000012 10033037 1666600007 116000000 36043442 0000011+

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